



# *Article* **Broadband Solar Absorber and Thermal Emitter Based on Single-Layer Molybdenum Disulfide**

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**Abstract:** In recent years, solar energy has become popular because of its clean and renewable properties. Meanwhile, two-dimensional materials have become a new favorite in scientific research due to their unique physicochemical properties. Among them, monolayer molybdenum disulfide (MoS<sup>2</sup> ), as an outstanding representative of transition metal sulfides, is a hot research topic after graphene. Therefore, we have conducted an in-depth theoretical study and design simulation using the finite-difference method in time domain (FDTD) for a solar absorber based on the two-dimensional material MoS<sup>2</sup> . In this paper, a broadband solar absorber and thermal emitter based on a single layer of molybdenum disulfide is designed. It is shown that the broadband absorption of the absorber is mainly due to the propagating plasma resonance on the metal surface of the patterned layer and the localized surface plasma resonance excited in the adjacent patterned air cavity. The research results show that the designed structure boasts an exceptional broadband performance, achieving an ultrawide spectral range spanning 2040 nm, with an overall absorption efficiency exceeding 90%. Notably, it maintains an average absorption rate of 94.61% across its spectrum, and in a narrow bandwidth centered at 303 nm, it demonstrates a near-unity absorption rate, surpassing 99%, underscoring its remarkable absorptive capabilities. The weighted average absorption rate of the whole wavelength range (280 nm–2500 nm) at AM1.5 is above 95.03%, and even at the extreme temperature of up to 1500 K, its heat radiation efficiency is high. Furthermore, the solar absorber in question exhibits polarization insensitivity, ensuring its performance is not influenced by the orientation of incident light. These advantages can enable our absorber to be widely used in solar thermal photovoltaics and other fields and provide new ideas for broadband absorbers based on two-dimensional materials.

**Keywords:** ultra-wideband absorption; two-dimensional materials; molybdenum disulfide; thermal emission

## **1. Introduction**

In contemporary society, with the sharp increase in energy demand, the supply of traditional fossil energy has been struggling to meet the needs of sustainable development, prompting people to focus on a wider range of renewable energy fields [\[1](#page-11-0)[–3\]](#page-11-1). Among them, solar energy, as an emerging and clean form of renewable energy, has attracted much attention. In order to cope with the challenge of energy shortage, researchers have carried out in-depth and extensive research on various types of clean energy, including solar energy [\[4](#page-11-2)[–6\]](#page-11-3). However, despite extensive research on solar absorbers, there are still many drawbacks. For example, the narrow width of the absorption band, the low absorption



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intensity, and the complex structure limit the application of absorbers in solar photovoltaic and other fields. Therefore, it is important to explore a broadband absorber with good oblique incidence characteristics and polarization angle independence as well as high thermal radiation efficiency [\[7–](#page-11-4)[9\]](#page-11-5).

In addition, ultra-wideband absorbers constructed from refractory materials show significant promise for applications where thermophotovoltaic devices are frequently subjected to high-temperature extremes. These absorbers not only operate stably at high temperatures, but also maintain excellent absorption stability, which lays a solid technical foundation for efficient energy conversion in high-temperature environments. Therefore, an in-depth exploration and optimization of the design strategy and preparation technology of such absorbers is of great significance to accelerate the innovation and development of solar energy and wider clean energy technologies. Titanium metal is known for its unique physical properties, including core advantages such as high strength, excellent heat and corrosion resistance, superior ductility, and relatively low density [\[10\]](#page-11-6). As a member of the refractory metals, titanium has a high melting point of 1668  $°C$ , displays excellent thermal stability, and exhibits good antimagnetization properties in strong magnetic field environments [\[11\]](#page-11-7). In absorber applications, titanium stands out not only for its excellent stability, but also for its cost-effectiveness compared to precious metals such as gold (Au) and silver (Ag). Of particular interest is the ability of titanium as a resonant material to excite a broader bandwidth response in the infrared spectral region, a property that offers the possibility of realizing highly efficient absorption in an ultra-broad band, thus greatly broadening its potential for a wide range of practical applications.

Over the past few years, two-dimensional materials have garnered significant attention within the scientific community, primarily due to their unparalleled physical and chemical characteristics, such as high electron mobility, excellent heat resistance, and chemical stability. Graphene [\[12](#page-11-8)[,13\]](#page-11-9), as a leader in the field of two-dimensional materials [\[14–](#page-11-10)[17\]](#page-12-0), has attracted extensive research interest for its unique physical properties. Its ultra-thin characteristics are particularly remarkable, with a thickness of only 0.34 nm, which is almost equal to the diameter of a single carbon atom. As an allotrope composed of carbon elements, in its monolayer state, the carbon atoms of graphene are closely combined with three adjacent carbon atoms by SP hybridization, forming a unique planar hexagonal honeycomb structure [\[18\]](#page-12-1). This structure endows graphene with excellent mechanical, electrical, and thermal properties, which makes it show great potential in scientific research and industrial applications. Many studies have confirmed that these excellent properties of graphene provide a broad prospect for its application in many fields [\[19](#page-12-2)[–22\]](#page-12-3). Graphene is unique in its zero-band gap property, which enables electrons to transition from valence band to conduction band at a very low energy state. However, it is the energy band structure of graphene that has zero bandgap [\[23\]](#page-12-4), so it has no adjustable semiconductor conductivity at all, which limits the possibility of its further development [\[24\]](#page-12-5).

Therefore, in contrast to pristine graphene, transition metal dichalcogenides (TMDCs) are generally regarded as superior absorbing materials. This is due to the fact that graphene possesses a zero bandgap, necessitating thermal excitation of electrons for conductivity, a characteristic that significantly constrains its practical applicability. TMDCs exhibit a tunable bandgap spanning from 1 to 2 eV, offering significant advantages in the fabrication of absorbers. Key attributes that render TMDCs particularly suitable for the production of solar absorbers include their remarkable stability, controllable thickness, and high absorption efficiency. Their ultrathin (monolayer) nature endows them with a direct bandgap within the visible spectrum, resulting in exceptional absorption capabilities. Among two-dimensional materials,  $MoS<sub>2</sub>$  stands out as a highly promising candidate for functional photonic devices due to its notable current cutoff ratio and tunable optoelectronic properties, as reported in  $[25,26]$  $[25,26]$ . Consequently, this study focuses on single-layer MoS<sub>2</sub> as a representative example for our investigation into two-dimensional materials.

Molybdenum disulfide  $(MoS<sub>2</sub>)$ , a transition metal sulfide, has received a lot of attention in recent years for its potential applications in optoelectronics. The unique properties

of MoS2, especially its broadband light absorption capability in the visible to near-infrared region, make it an ideal material for solar absorbers [\[27\]](#page-12-8). Compared with other twodimensional materials,  $MoS<sub>2</sub>$  has a direct bandgap, which gives it a significant advantage in light absorption efficiency. In addition, the high electron mobility of  $MoS<sub>2</sub>$  facilitates the rapid transport of electrons under light excitation, which improves the response speed and efficiency of optoelectronic devices. In terms of chemical stability,  $MoS<sub>2</sub>$  is able to maintain its performance under a wide range of environmental conditions, which is essential for the fabrication of durable optoelectronic devices [\[28\]](#page-12-9). With the development of solution processing techniques, the preparation of  $MoS<sub>2</sub>$  thin films has become more economical and scalable. Spin-coating techniques have been used to prepare homogeneous  $MoS<sub>2</sub>$  films and characterize them by variable angle spectroscopic ellipsometry. In addition, by using the dimethylformamide/n-butylamine/2-aminoethanol solvent system, researchers have been able to synthesize wafer-scale  $MoS<sub>2</sub>$  thin films with controllable thickness using the solution method. These advances not only improve the quality of  $MoS<sub>2</sub>$  films, but also pave the way for their integration in solar cells, photodetectors, and other optoelectronic devices  $[29,30]$  $[29,30]$ . The bandgap of MoS<sub>2</sub> can be tuned by chemical doping or strain engineering, enabling precise control of the absorption spectrum. This tunability provides great flexibility in designing optoelectronic devices with specific spectral responses. With the further understanding of  $MoS<sub>2</sub>$  material properties and the continuous advancement of processing technologies, MoS2-based optoelectronic devices are expected to play an important role in the future of sustainable energy and advanced electronics.

Currently, the state of absorbers in this domain is marred by numerous limitations: some absorbers are too complicated to design and too bulky for actual manufacturing [\[31\]](#page-12-12). The working range of the absorber is too narrow, the absorption capacity is limited, and numerous state-of-the-art absorbers utilize costly precious metals, particularly gold and silver, resulting in significant production expenses. Additionally, there is ample scope for enhancing their thermal endurance to ensure optimal performance under various conditions. Thus, in this paper, we propose a cost-effective solar absorber featuring straightforward manufacturing processes, a broad absorption spectrum, and superior absorption efficiency within the solar radiation spectrum. The solar energy absorber demonstrates remarkable absorption capabilities across a broad spectral domain, particularly within the wavelength interval spanning from 280 to 2320 nanometers (2040 nm in total), and its absorption efficiency keeps above 90%, with an average absorption efficiency as high as 94.61%, which fully proves its high-efficiency light energy absorption capacity. Therefore, our absorber will provide some references for similar structures of other solar absorbers and has potential for a wide range of applications such as solar thermal photovoltaic systems. Our work also opens up new avenues for the application of two-dimensional materials in the field of optoelectronics and energy conversion.

#### **2. Results and Discussion**

Figure [1](#page-3-0) meticulously portrays the absorption characteristics of the structure through a comprehensive chart. Specifically, the red trace delineates the absorption efficiency, whereas the black trace signifies reflectivity, and the blue trace is indicative of transmittance. In view of the sufficient thickness of the substrate Ti, we observed that the transmittance was almost zero. Obviously, the solar energy absorber shows excellent absorption performance in a wide spectral range, particularly within the spectral range spanning from 280 to 2320 nanometers (a total of 2040 nm), within which the absorber maintains an absorption efficiency exceeding 90% with an average efficiency of 94.61%. Notably, it achieves a nearperfect absorption rate of 99% specifically at a wavelength of 303 nm, which fully proves its high-efficiency light energy absorption ability. Compared with other recent absorbents based on molybdenum disulfide, our absorbent has obvious advantages in bandwidth and average absorption rate, as shown in Table [1](#page-3-1) [\[12](#page-11-8)[,32](#page-12-13)[–37\]](#page-12-14).

<span id="page-3-0"></span>

mechanisms to achieve efficient absorption.

**Figure 1.** Depicts the spectral characteristics of absorption, reflectance, and transmittance, under **Figure 1.** Depicts the spectral characteristics of absorption, reflectance, and transmittance, under plane incident light. plane incident light.

<span id="page-3-1"></span>**Table 1.** Comparison with other literature.

Essay	Spectral Region Exhibiting an <b>Absorption Rate Exceeding 90%</b>	<b>Average Absorption</b> Efficiency	Maximum <b>Absorption Rate</b>
$[32]$	$712 \text{ nm}$	97%	99.80%
$[12]$	<1000 nm	85%	97.00%
[38]	$1110 \,\mathrm{nm}$	$<90\%$	99.80%
$[34]$	475 nm	$94\%$	97%
$[35]$	1547 nm	90%	98%
[36]	$1200 \text{ nm}$	$91\%$	
[37]	$1100 \text{ nm}$	99.6%	98.5%
This text	$2040$ nm	94.61%	99.87%

In order to probe into the rationale behind the ultra-broadband and near-perfect **Efficiency**  absorption achieved in this paper, we chose three representative bands for the follow-up study of electric field distribution. These three bands are  $\lambda$ 1 = 456 nm (in the visible region),  $\lambda$ 2 = 916 nm (in the vicinity of the infrared spectral region) and  $\lambda$ 3 = 1720 nm (also in the near-infrared region). Through this analysis, we expect to reveal the key factors and mechanisms to achieve efficient absorption.

A comprehensive comparison of the performance metrics of the absorber introduced in this study with those reported in prior research is presented in Table 1. The analysis shows that the perfect absorber designed by us has remarkable ultra-wide bandwidth characteristics, which obviously exceed other comparative absorbers, and its highest ab-*2.1. The Influence of Different Structures on the Results*  highest in terms of average absorption efficiency, it still shows significant advantages in comprehensive performance of bandwidth and efficiency, which provides us with an ideal<br>and practical choice  $\frac{1}{\sqrt{2}}$ sorption rate is also better. In addition, although our solar energy absorber is not the and practical choice.

#### *2.1. The Influence of Different Structures on the Results*

Initially, we delve into the consequences of integrating a single-layer molybdenum disulfide within the architecture. For illustrative purposes, we have modeled the structure with and without a single layer of molybdenum disulphide and with the transformed 2D material being graphene. For example, the absorption of light by monolayer graphene is inherently low, about 2.3 per cent, due to its energy band structure [\[39\]](#page-12-19). Graphene is a zero-bandgap material with an electronic structure similar to a Dirac cone, which makes it less responsive to light in the visible and near-infrared bands, as shown in Figure [2a](#page-4-0). As evident from Figure [2a](#page-4-0), the incorporation of this monolayer yields two notable benefits: a significant broadening of the operational bandwidth and an enhancement in the beficiency within the shorter wavelength region. Within Region I, the analysis absorption efficiency within the shorter wavelength region. Within Region I, the analysis that the absorption rate of the nanostructures falls below 90% across a relatively reveals that the absorption rate of the nanostructures falls below 90% across a relatively extensive bandwidth, in the absence of a single layer of molybdenum disulfide. After the introduction of single-layer molybdenum disulfide, it can be seen that due to its high the introduction of single-layer molybdenum disulfide, it can be seen that due to its high absorption rate in the near-ultraviolet band, the absorption efficiency within the shorter wavelength spectrum undergoes a substantial augmentation, surpassing the 90% threshold. Furthermore, Figure [2b](#page-4-0), depicting a magnified section of Region II, evidences a marked expansion in the bandwidth where the absorption rate surpasses 90%. Specifically, the introduction of a single layer of  $MoS<sub>2</sub>$  results in a broadening of this high-absorption region by approximately 310 nanometers. In a word, the introduction of single-layer molybdenum disulfide makes the Ti-SiO<sub>2</sub> cuboid structure designed for superior absorption address the challenge of insufficient absorption in the short-wavelength region, thereby effectively broadening the operational bandwidth.

<span id="page-4-0"></span>

**Figure 2.** (a) Illustrative sketch outlining the enhancement in absorption for a monolayer  $MoS<sub>2</sub>$ structure; (**b**) Magnified section of Region I for closer inspection.

In the following research, we deeply discuss the influence of different geometric patterns on the performance of the absorber. We replaced the original cuboid structure with a cylindrical structure  $(B)$  and a circular column structure  $(C)$ , respectively, and calculated their absorption efficiency under the same lighting conditions. Through careful analysis of the absorption spectrum in Figure [3a](#page-5-0), our analysis indicates that the rectangular paralparallelepiped configuration exhibits a marginally reduced absorption efficiency compared to both cylindrical and circular cylindrical structures, within the spectral range spanning from 400 nm in the visible light region to 1600 nm in the near-infrared, but it shows it is shown in the near-infrared, but it shows it is also in the near-infrared, but it shows it is also in the near-infrared, but it is significant advantages in the band over 1600 nm. Its wider bandwidth and higher overall states with and higher overall absorption rate of solar full spectrum grant the cuboid structure greater potential in wide-absorption rate of solar full spectrum grant the cuboid structure greater potential in wideband light absorption applications. Based on the above analysis, we finally chose the cu-structure as the micro-nano-structure of the absorber in order to achieve better performance. boid structure as the micro-nano-structure of the absorber in order to achieve better per-This selection not only considers the evaluation of the absorber's efficacy within the for the second the constant of the evaluation of the evaluation of the evaluation  $\frac{1}{2}$  is the constant of the absorber of the absorber  $\frac{1}{2}$  is a constant of the absorber of the absorber of the absorber of the ab visible light and near-infrared spectral bands, but also fully considers its comprehensive<br>near-infrared spectral bands, but also fully considers its comprehensive band light absorption applications. Based on the above analysis, we finally chose the cuboid performance in a wider band.

In addition, from the electric field distribution diagram shown in Figure [3b](#page-5-0)–d, we can observe that the electric field is mainly concentrated on the geometric surface. This phenomenon is mainly attributed to the excitation of PSPs (surface plasmon) on the surface of the pattern layer [\[38](#page-12-15)[,40](#page-12-20)[,41\]](#page-13-0). PSPs are electromagnetic oscillations generated at the metal-medium interface; this capability allows for the conversion of light energy into thermal energy or alternative energy forms, thus achieving efficient light absorption [\[42](#page-13-1)[–44\]](#page-13-2). Therefore, the intensified electric field distribution along the geometric surface underscores the pivotal role played by PSPs in facilitating the light absorption process.

<span id="page-5-0"></span>

**Figure 3.** (a) is an absorption spectrum diagram of different micro-nano structures;  $(b-d)$  are the electric field intensities of different micro-nano structures in the XOY plane within a period. electric field intensities of different micro-nano structures in the XOY plane within a period.

### *2.2. Physical Mechanism Analysis of High Absorption and Wide Bandwidth of Structure*

In addition, from the electric field distribution diagram shown in Figure 3b–d, we can To gain deeper insight into the underlying physical mechanisms that contribute to the high absorption efficiency and extended bandwidth of the absorber, spanning from<br>the surface plast the high association of a surface per homogened at the dealer little spanning from the visible light to the hear inflated region, we have conducted carealations pertaining<br>to the electric field distributions at specific wavelengths:  $λ1 = 456$  nm,  $λ2 = 916$  nm, and  $\lambda$ 3 = 1720 nm, and compared them by drawing. Among them, Figure [4a](#page-6-0)–c shows the electric field distribution in the XOY direction in the next period from  $\lambda$ 1 to  $\lambda$ 3, and The vector that is the intensity intensity in the intensity  $\frac{1}{2}$  is  $\frac{1}{2}$  in  $\frac{1}{2}$  in  $\frac{1}{2}$  is  $\frac{1}{2}$  in  $\frac{1}{2}$  in  $\frac{1}{2}$  is  $\frac{1}{2}$  in  $\frac{1}{2}$  is  $\frac{1}{2}$  is  $\frac{1}{2}$  if  $\frac{1}{2}$  is  $\frac{1$ Figure [4d](#page-6-0)–f shows the electric field distribution in the XOZ direction in the two periods from  $31$  to  $33$ the visible light to the near-infrared region, we have conducted calculations pertaining from λ1 to λ3.

*2.2. Physical Mechanism Analysis of High Absorption and Wide Bandwidth of Structure*  planes, as shown in Figure [4a](#page-6-0)–f, with the increase in resonance wavelength, optical coupling goes from the edge of the metal cuboid of the pattern layer to the air cavity formed by the adjacent pattern layers, and it is obvious that excitation of surface plasmon resonance occurs within the absorber [\[45](#page-13-3)[,46\]](#page-13-4). When the wavelength is  $\lambda$ 1 = 456 nm, observation of Figure [4a](#page-6-0) reveals that the electric field is predominantly concentrated on the metallic upper segment of the patterned layer. Therefore, the primary factor contributing to the perfect absorption observed at wavelength  $\lambda 1$  is the excitation of surface plasmon polaritons (PSPs) on the surface of the patterned layer.  $\frac{1}{2}$  to  $\frac{1}{2}$  to Integrating the analysis of the electric field distribution within both the X-Y and X-Z pattern layer.<br>Pattern layer

<span id="page-6-0"></span>

**Figure 4.** (a–c) are the electric field distributions of the XOY plane in one period at  $\lambda$ 1,  $\lambda$ 2, and  $\lambda$ 3 wavelengths, respectively;  $(d-f)$  are the electric field distributions of two periodic XOZ planes at  $\lambda$ 1, λ2, and λ3 wavelengths, respectively. λ2, and λ3 wavelengths, respectively.

Different from the excitation mechanism of PSPs, the excitation of LSPs does not need specific momentum-matching conditions  $[47–49]$ . The underlying reason for this is [tha](#page-13-5)t the incident light's wavelength far exceeds the characteristic dimensions of the metallic structures, and these nanostructures can be regarded as a kind of focused source point, which can produce diverse wave vector components, and then provide the necessary momentum matching for LSPs in the excitation structure. More specifically, the excitation intensity of local surface plasmon resonance (LSPs) is determined by the wavelength of the incoming light, the size of nanoparticles or nanostructures and the inherent characteristics of the materials [\[50\]](#page-13-7). Since the wavelength of incident light,  $\lambda$ 2 = 916 nm, is much longer than the period of the absorber, 400 nm, LSPs can be generated in the metal of the pattern layer.

*2.3. Weighted Average Absorption Rate and Radiation Performance Analysis*  region. The electric field distribution shows that PSPs and LSPs are excited on the metal surface of the pattern layer and in the adjacent pattern air cavity, respectively; concurrently,  $\lambda$ 3 = 1720 nm, the electric field distribution in the XOY direction is similar to that when Illustrated in Figure [4b](#page-6-0),e, a strong electric field appears in the adjacent pattern layer the resonant wavelength of  $\lambda$ 2 = 916 nm attains perfect absorption. At a wavelength of  $\lambda$ 2 = 916 nm, as shown in Figure [4c](#page-6-0), but different from 916 nm. An intense electric field accumulates within the dielectric spacer, localized at the interface between the cuboid structure and the MoS<sub>2</sub> layer, and the electric field intensity of the top anti-reflection layer silicon dioxide is weakened. Therefore, the perfect absorption observed in the 1720 nm band stems from the excitation of localized surface plasmons (LSPs).

#### *2.3. Weighted Average Absorption Rate and Radiation Performance Analysis*

This paper delves into the absorption and radiation properties of the proposed structure, with the objective of evaluating its performance efficiency as both a solar absorber and a thermal emitter. In this process, we use the global spectral equation under the condition of AM 1.5 incident solar energy, which is specifically expressed as [\[51](#page-13-8)[,52\]](#page-13-9):

$$
\eta_A = \frac{\int_{\lambda_{Min}}^{\lambda_{Max}} A(\omega) I_{AM1.5}(\omega) d\omega}{\int_{\lambda_{Min}}^{\lambda_{Max}} I_{AM1.5}(\omega) d\omega}
$$
(1)

The equation of thermal emission efficiency  $(\eta_E)$  is [\[53\]](#page-13-10):

$$
\eta_E = \frac{\int_{\lambda_{min}}^{\lambda_{max}} \varepsilon(\omega) \cdot I_{BE}(\omega, T) d\omega}{\int_{\lambda_{min}}^{\lambda_{max}} I_{BE}(\omega, T) d\omega}
$$
(2)

Herein,  $I_{BE}(\omega, T)$  signifies the intensity of radiation emitted by an ideal blackbody at a given frequency  $\omega$  and temperature *T*.

The equation of thermal emission efficiency (*η*E) is [53]:

Under AM 1.5 illumination conditions, as exemplified in Figure [5a](#page-7-0), the blue curve portrays the theoretical ideal absorption spectrum, whereas the red curve represents the actual energy absorption achieved by the structure. The black area in the figure represents the main area of energy loss, mainly concentrated in the visible light band. Nevertheless, on the whole, the band absorption rate is maintained at a high level of 95.03%, while the loss rate is controlled below 5%. Further, Figure 5b divulges the thermal emission properties exhibited by the structure when subjected to a high temperature of 1500 Kelvin. The black line in the figure represents the theoretical blackbody radiation curve and serves as a benchmark, whereas the red area represents the actual thermal radiation emitted by the structure. It can be observed from the figure that within the spectral range below 1800 nanometers, the observed thermal radiation closely aligns with the theoretical blackbody radiation curve, and only slight thermal radiation loss occurs in the band above 1800 nm. However, in the whole band, the thermal radiation efficiency remains at a high level, reaching 95.96%.

<span id="page-7-0"></span>

Figure 5. (a) Depicts the distribution of energy absorption and loss for solar radiation spanning 280 nm to 2500 nm, under an atmospheric mass (AM) of 1.5; (**b**) Illustrates the energy emission from 280 nm to 2500 nm, under an atmospheric mass (AM) of 1.5; (**b**) Illustrates the energy emission spectrum emanating from a solar absorber operating at an elevated temperature of 1500 K. spectrum emanating from a solar absorber operating at an elevated temperature of 1500 K.

# *2.4. Effect of Varying Parameters on Absorption Outcomes 2.4. Effect of Varying Parameters on Absorption Outcomes*

To validate the optimally chosen structural parameters within this design framework, we conducted a methodical evaluation of the influence that various structural attributes exert on absorption efficiency under the premise of ensuring that other parameters remain unchanged  $[54,55]$  $[54,55]$ . Specifically, we discussed in detail the thickness H1 of top silicon dioxide  $(SiO<sub>2</sub>)$ , the thickness H2 of rectangular titanium (Ti) and its side length D, and the and the period P of the whole structure. In this process, we did not take into account the period P of the whole structure. In this process, we did not take into account the parameter changes in Ti and SiO<sub>2</sub>, because according to the previous analysis, the adjustment of these parameters has no significant influence on absorption efficiency.

In Figure [6a](#page-8-0)–d, firstly, we deeply studied how the thickness H1 of the top  $SiO<sub>2</sub>$  affects the absorption spectrum. Especially in the ultraviolet and visible light bands, the  $SiO<sub>2</sub>$  layer plays a vital role [\[56,](#page-13-13)[57\]](#page-13-14). Through careful observation, we found that with the side length d gradually increasing from 20 nm to 60 nm, the absorption efficiency first showed an upward trend, but then showed a downward trend. This discovery provides an important clue for us to further understand the role of the  $SiO<sub>2</sub>$  layer in light absorption. Based on this discovery, we infer that the optimal side length of a rectangle should be close to 40 nm. Then, we delved deeper into examining the effect of varying the thickness (H2) of the rectangular titanium (Ti) layer on the absorption spectrum. As H2 was incremented from 100 nm to 300 nm, we discerned a trend in the evolution of the absorption efficiency. It is particularly noteworthy that when the period p is set to 200 nm, we get the best absorption

result, which not only has high absorption efficiency, but also has excellent absorption bandwidth. This discovery provides an important reference for our subsequent experiments and applications. As shown in Figure [6c](#page-8-0), when the side length of a cuboid is increased from 180 nm to 260 nm, we can observe that the shorter the side length of the cuboid is, an enhanced absorption efficiency is observed within the short wavelength region spanning from 280 to 1500 nanometers. However, with the increase in wavelength, the absorption efficiency of the rectangular parallelepiped with longer side length is significantly enhanced and the bandwidth is wider. On the whole, when  $\overrightarrow{D} = 220$  nm, the overall absorption rate and bandwidth are better. Therefore, upon thorough analysis, we propose that a side length of  $D = 220$  nm offers optimal performance. Figure [6d](#page-8-0) illustrates the absorption spectrum across the entire periodic variation, where it becomes evident that an increase in the periodicity corresponds to an augmentation in the absorption rate within the spectral range of 1000-1500 nanometers, but considering the overall absorption efficiency of short wave and long wave, the absorber can only exert its maximum absorption potential when  $P = 400$  nm.

<span id="page-8-0"></span>

**Figure 6. (a)** Thickness change absorption spectrogram of top silicon dioxide; ( $\mathbf{b}$ , $\mathbf{c}$ ) are absorption spectrograms of thickness and side length change in rectangular titanium, respectively; (d) The absorption spectrum of structural period change.

# *2.5. Angle Sensitivity Analysis 2.5. Angle Sensitivity Analysis*

Finally, in order to study the application potential of the structure, we studied the Finally, in order to study the application potential of the structure, we studied the angular sensitivity of the structure [58–60]. It is acknowledged that in practical scenarios, angular sensitivity of the structure [\[58–](#page-13-15)[60\]](#page-13-16). It is acknowledged that in practical scenarios, natural light seldom strikes the solar absorber vertically, contrasting with the idealized natural light seldom strikes the solar absorber vertically, contrasting with the idealized conditions. Consequently, it is crucial to investigate the influence of varying polarization and incident angles on the performance of solar absorbers. As depicted in Figure [7,](#page-9-0) we have conducted simulations to analyze the absorption spectrum, encompassing incident angles and polarization angles ranging from  $0^{\circ}$  to  $60^{\circ}$ , respectively. As evident from Figure [7a](#page-9-0), the designed absorber demonstrates remarkable performance within an incident angle span of  $0^{\circ}$  to  $60^{\circ}$ , exhibiting exceptional overall absorption efficiency. As the polarization angle of the incident light progresses from  $0^{\circ}$  to  $60^{\circ}$ , a marginal enhancement in visible light absorption is observed, while the near-infrared region undergoes a slight attenuation, particularly from 50%. Notably, the absorber sustains an absorption rate exceeding 90%

across a broad wavelength spectrum extending up to 2040 nm. The results of this study clearly show that the absorber we designed shows excellent insensitivity to incident angle. As shown in Figure [7b](#page-9-0), the spectral response remains stable even when the polarization angle increases; this underscores the exceptional insensitivity of the structure towards polarization variations, thereby reinforcing its robustness. The inherent high geometric symmetry of the structure contributes to a consistently high absorption rate across the entire wavelength spectrum, exhibiting minimal variation with alterations in polarization a[ng](#page-13-17)le  $[61,62]$ . This robustness to both oblique incidence and polarization insensitivity significantly enhances the absorber's performance, presenting substantial advantages for practical applications.

<span id="page-9-0"></span>

 $\frac{1}{2}$  **Figure 7.** (**b**) Manipulating the absorption spectrum through alterations in the polarization angle 0 $\degree$  to 60 $\degree$ ; (**b**) Manipulating the absorption spectrum through alterations in the polarization angle, spanning from 0 $\degree$  to 60 $\degree$ . spanning from  $0°$  to  $60°$ . **Figure 7.** (**a**) Modifying the absorption spectrum by varying the incident angle within a range of

# **3. Modelling and Structural Parameters of the Micro-Nano Optical Devices**

In this paper, we introduce a periodically arranged rectangular configuration consisting of Ti-SiO<sub>2</sub> layered structures, as shown in Figure 8a. The thickness of local structure is denoted as H1, H2, H3, and H4 from top to bottom. The overall width of the absorber is  $P = 400$  nm, the bottom is made of titanium, and its thickness H4 = 300 nm. In this architecture, Ti functions as a reflective element, with its thickness (H4) set at 300 nanometers, significantly exceeding the penetration depth of electromagnetic radiation. Consequently, the transmission through this structure is effectively nullified, that is,  $T(\omega) = 0$  [63,64]. In this work, the spectral absorption efficiency is defined as:

$$
A(\omega) = 1 - R(\omega) - T(\omega)
$$
\n(3)

Therefore, the absorption rate can be simplified as  $A(\omega) = 1 - R(\omega)$  [\[65](#page-13-21)[,66\]](#page-13-22), where R ( $\Omega$ ) and  $T(\Omega)$  respectively represent the spectral reflection and transmission under the illumination of plane light. The second layer is dielectric silicon dioxide  $(SiO<sub>2</sub>)$  with a dividend  $(SiO<sub>2</sub>)$ the  $\frac{1}{2}$   $\frac{1}{2}$   $\frac{1}{2}$   $\frac{1}{2}$  for the substrate the supporting substrate  $\frac{1}{2}$   $\frac{$ of MoS<sub>2</sub>, aiming at solving the challenge of depositing MoS<sub>2</sub> directly on the titanium<br>layer. This concentration the layer has been deposited at the tital state meterial on the term it is the two-dimensional metamaterial  $MoS<sub>2</sub>$ . We set the thickness of  $MoS<sub>2</sub>$  as 0.625 nm, which is mensional metamaterial MoS2. We set the thickness of MoS2 as 0.625 nm, which is based based on the standard thickness grown under most laboratory conditions, thus ensuring the accuracy and repeatability of the research. This configuration not only optimizes the example and repeatability of the research. This comiguration for only optimizes the growth environment of MoS<sub>2</sub>, but also lays a foundation for its performance in subsequent thickness of  $H3 = 40$  nm. In this paper, we propose a material as the supporting substrate layer. This support material is located under the dielectric material and above it is the applications. The microstructure of the surface layer is stacked by  $Ti-SiO<sub>2</sub>$ , and its height is set to  $H1 = 40$  nm and  $H2 = 200$  nm. Non-precious metal (Ti) is chosen as the metal material here, because Ti has high loss in visible light and near-infrared, which can effectively broaden the absorption bandwidth, and the price is relatively cheap, which can reduce the manufacturing cost. Among them, the dielectric constant data of Ti and  $SiO<sub>2</sub>$  are cited and applied based on the experimental results of Palik [\[67\]](#page-13-23). In numerical calculations and simulations, the dielectric constant of molybdenum disulphide  $(MoS<sub>2</sub>)$  is a key parameter that determines the material's response properties to light. For the monolayer  $MoS<sub>2</sub>$  in the paper, we cite the data of Ermolaev et al. [\[68\]](#page-14-0). Its dielectric constant is usually expressed in complex form, including real and imaginary parts, and can be expressed as  $n = n' + ik$ , where n' is the real part of the dielectric function, which represents the material's polarization capacity, while k is the imaginary part, which is related to the material's absorption capacity.

<span id="page-10-0"></span>

Figure 8. (a) Shows the three-dimensional structure of the model; (b) Structure diagram of XOZ plane.

**4. Conclusions**  as an analysis tool. In this simulation, the setting of the light source is very important. We selected the plane light source from 280 nm to 2500 nm and ensured the polarization of light aligned along the X-axis by configuring the incident light to propagate vertically in the negative Z-axis direction. To uphold the rigor and fidelity of our simulation, we applied periodic boundary conditions in the x and y dimensions to simulate the infinite extended  $\overline{a}$ periodic structure. Along the Z-axis, we choose the perfectly matched layer (PML) as the boundary condition to effectively absorb and eliminate the possible reflected waves during the simulation, thus ensuring the accuracy of the simulation results  $[69]$ . In the numerical simulation calculation, we use FDTD version 2020 solutions software

# sional materials in improving absorption performance. In addition, MoS2 not only has ex-**4. Conclusions**

In this paper, we have achieved the successful design of an efficient broadband solar the condition effect, we have achieved the successful design of an emergin producture solar absorber, leveraging the unique properties of  $MoS<sub>2</sub>$  two-dimensional materials. Through numerical calculation, our findings indicate that the absorption efficiency of the structure surpasses 90% within a wavelength spectrum exceeding 2040 nm, and the absorption rate can reach 99% or more in the wavelength range of 303 nm. It is noteworthy that an optimal thickness of  $0.625$  nm for the  $MoS<sub>2</sub>$  layer has been identified, and its absorption bandwidth is significantly extended to 310 nm, which fully verifies the superiority of two-dimensional materials in improving absorption performance. In addition, MoS<sub>2</sub> not only has excellent thermal stability, but also helps to reduce device size and improve overall absorption efficiency. Under the condition of AM 1.5 spectrum, our structure shows excellent weighted average absorption efficiency, reaching a high level of 95.03%. Even at an extreme temperature as high as 1500 K, its thermal radiation efficiency can be maintained at an excellent level of 95.96%. The structure demonstrates remarkable independence and resilience towards variations in both the polarization angle and the incident angle of the incoming light, and its performance remains stable even in the polarization angle range of 0 to 60. In summary, the high absorption efficiency and stability at extreme temperatures of this MoS<sub>2</sub>-based broadband solar absorber we have designed make it ideal for solar thermal photovoltaic systems that can convert solar energy directly into electricity, thereby reducing dependence on fossil fuels and lowering greenhouse gas emissions. Additionally, by using cost-effective titanium (Ti) in place of expensive precious metals, our technology helps lower the economic barrier to solar technology, advancing its use in a wider range of

applications. Our design also demonstrates insensitivity to the direction of polarization of incident light, which increases its reliability in variable environments and opens up the possibility of applying solar absorbing technologies in different geographical locations and climates.

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