

Article

A Separated Receptor/**Transducer Scheme as Strategy to Enhance the Gas Sensing Performance Using Hematite–Carbon Nanotube Composite**

Nguyen Minh Hieu, Cao Van Phuoc [,](https://orcid.org/0000-0002-2662-7077) Truong Thi Hien, Nguyen Duc Chinh, Nguyen Duc Quang, Chunjoong Kim *, Jong-Ryul Jeon[g](https://orcid.org/0000-0002-0295-4030) and Dojin Kim [*](https://orcid.org/0000-0003-0964-8527)

Department of Materials Science and Engineering, Chungnam National University, Daejeon 34134, Korea; cockyhieu@gmail.com (N.M.H.); caovanphuoc91@gmail.com (C.V.P.); anhientruong@gmail.com (T.T.H.); nguyenducchinh0605@gmail.com (N.D.C.); nguyenducquang0903@gmail.com (N.D.Q.); jrjeong@cnu.ac.kr (J.-R.J.)

***** Correspondence: ckim0218@cnu.ac.kr (C.K.); dojin@cnu.ac.kr (D.K.); Tel.: +82-42-821-6639 (D.K.)

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Abstract: Nanocomposite structures, where the Fe, Fe₂O₃, or Ni₂O₃ nanoparticles with thin carbon layers are distributed among a single-wall carbon nanotube (SWCNT) network, are architectured using the co-arc discharge method. A synergistic effect between the nanoparticles and SWCNT is achieved with the composite structures, leading to the enhanced sensing response in ammonia detection. Thorough studies about the correlation between the electric properties and sensing performance confirm the independent operation of the receptor and transducer in the sensor structure by nanoparticles and SWCNT, respectively. Nanoparticles with a large specific surface area provide adsorption sites for the $NH₃$ gas molecules, whereas hole carriers are supplied by the SWCNT to complete the chemisorption process. A new chemo-resistive sensor concept and its operating mechanism is proposed in our work. Furthermore, the separated receptor and transducer sensor scheme allows us more freedom in the design of sensor materials and structures, thereby enabling the design of high-performance gas sensors.

Keywords: separated receptor and transducer; hematite–carbon nanotube composite; gas sensor

1. Introduction

Metal oxides have been extensively studied for chemoresistive gas sensors because of their high reactivity with various gas molecules as well as their adoptability to modern microfabrication technologies [\[1\]](#page-12-0). It is well known that the molecular adsorption of gas phases followed by the chemical reaction with the oxide occurs by the charge exchange between the gas molecule and oxide, and the consequent change of conductance change in the oxide is translated to the sensing signal through the metal electrodes underneath [\[2–](#page-12-1)[4\]](#page-12-2). In such oxide gas sensors, the surface plays the role of the sensory receptor by the supply of gas molecular ionosorption sites while the bulk structure donates charges for the ionosorption reaction on the surface. At the same time, the bulk structure also works as a transducer, which reveals the change of conductance (or resistance) as an electric signal. A typical geometry for the operation of metal oxide gas sensors is configured by the receptor and transducer integrated into the single metal oxide body.

Since the sensor operating principle is strongly affected by the structure of the sensor, both 'nanosize effect' and 'nanosize limit effect' have been reported in conduction-type gas sensors. The nanosize effect is a well-known observation in chemoresistive gas sensors, which describes the increase in the sensing response as the dimension of the sensor structure decreases to a nanosize [\[4–](#page-12-2)[10\]](#page-12-3). However,

when the size decreases smaller than the depletion depth scale, the total depletion of carriers leads to the insulating nature in the sensor structure followed by the decrease of the sensor signal. Such declining response at the dimension below the depletion depth scale has been introduced as the nanosize limit [\[10](#page-12-3)[,11\]](#page-12-4). Therefore, the highest response level can be achieved at the size comparable with that of the depletion depth for a given doping concentration of the oxide.

CNTs have been repeatedly reported to show the sensing capability toward $NH₃$ at room temperature (RT, ~25 °C) [\[12](#page-12-5)[–17\]](#page-12-6). The interaction of NH₃ with the Fe and Fe₂O₃ at RT also was reported to occur via the dissociative molecular adsorption of $NH₃$ on the Fe and Fe₂O₃ clusters [\[18](#page-12-7)[–27\]](#page-13-0), respectively. Hematite exhibited higher ammonia sensing performance at the elevated temperature (150 °C) than that at RT [\[26\]](#page-13-1). Meanwhile, the composite sensors, tin oxide-based carbon, showed a sensing capability toward NH₃ [\[28](#page-13-2)[–30\]](#page-13-3) and NO₂ [\[31\]](#page-13-4). Hieu et al. [\[28\]](#page-13-2) showed that the SnO₂/multi-wall CNT composite detected NH₃ at RT. Lee et al. [\[29\]](#page-13-5) reported about the SnO₂/carbon nanoflake composite for the detection of NH₃ at 400 °C. The different operating temperatures were possibly originated from the different mixing ratios between the carbon (a p-type conducting sensor operating at RT) and $SnO₂$ (an n-type conducting sensor operating at high temperature). Rigoni et al. [\[30\]](#page-13-3) also detected NH³ using the indium tin oxide (ITO) and SWCNT composite at RT. Interestingly, the conducting type of the composite sensor changed from the p-type semiconductor to the n-type with high NH₃ adsorption due to the injection of many electrons into the structure.

In this study, we prepared composite sensors composed of iron or hematite (Fe₂O₃) and single-wall carbon nanotubes (SWCNTs), Fe:SWCNTs, and Fe₂O₃:SWCNTs, respectively, for the NH₃ detection at RT, and scrutinized their sensing behaviours with pure hematite and SWCNT sensors. Fe:SWCNTs and $Fe₂O₃$:SWCNTs nanocomposite structures showed the enhanced NH₃ sensing response at RT owing to the synergistic effect. In addition, based on the comparative study with single-body gas sensors, hematite or SWCNTs sensors, we explored the underlying sensing mechanism of the composite structure. The semiconductor depletion model for the nanosize effect and the nanosize limit effect was thoroughly revisited, thus we could overcome the nanosize limit via the new concept of separated receptors and transducers for the high-response chemoresistive gas sensors. While the large surface area of hematite nanoparticles with a thin carbon layer provides adsorption sites for ammonia gas molecules, the charges necessary for the ionosorption are supplied from the SWCNTs. The net result is the appearance of far more extended depletion in SWCNTs, enabling an enhanced sensor signal. We elaborate the origin of the synergy effect and the principle of the new sensor scheme. Furthermore, we showed that such a sensor scheme can be a general route to overcome the nanosize limit regardless of the junction types by comparison with the p-p junction composite of $Ni₂O₃$:SWCNT.

2. Experiment

2.1. Synthesis of the Fe2O3:CNT Structures

The Fe:CNT composites were fabricated on alumina substrates of 2.5 mm \times 2.5 mm \times 0.23 mm patterned with bar-type gold electrodes by a co-arc discharge method [\[11,](#page-12-4)[32–](#page-13-6)[35\]](#page-13-7), which is commonly used to prepare nanocrystalline metal (or metal oxide)-CNT composites at a high temperature during the arc-discharge process. The distance between the Au electrodes was kept at 1 mm. In general, a co-arc discharge method produces the morphology of finely dispersed metal (or metal oxide) nanoparticles among the SWCNTs [\[32](#page-13-6)[,34](#page-13-8)[,35\]](#page-13-7). Firstly, the gold electrode-patterned Al_2O_3 substrates were ultrasonically cleaned sequentially with acetone, methanol, and deionized water for 15 min each, followed by N_2 blow drying. The substrates were mounted on the inside wall of the arc-discharge chamber, as schematically shown in Figure S1a,b (Supporting Information). A hollow graphite tube with a length, outer diameter, and inner diameter of 160, 6.4, and 3 mm, respectively, was used as a carbon source (Figure S1c). The hollow carbon tube was filled with different numbers of Fe wires. The arc-discharge process of the graphite tube filled with iron feedstock was performed for 20 min at an arc-discharge current density of 40 A cm−² in a hydrogen atmosphere with a H² partial pressure

of 5.3×10^3 Pa. The *as-de[pos](#page-2-0)ited* sample is labelled by AD in Figure 1a that presents the flowchart of sample fabrication.

Figure 1. Experimental procedure of fabricating the (a) as-deposited (AD) and methanol-treated (MT) iron:carbon nanotubes (Fe:CNT) and heat-treated (HT) hematite (Fe $_2$ O $_3$):CNT composite structures, (b) pure CNT, and (c) pure Fe₂O₃.

The AD sample, the Fe:CNTs composite, shows a highly porous structure, in which the Fe nanoparticles are uniformly dispersed in the entangled CNTs. It was observed that the iron particles nanoparticles are uniformly dispersed in the entangled CNTs. It was observed that the iron particles are deposited by carbon during the arc-discharge process. Therefore, the Fe nanoparticles in the \overline{a} Fe:CNTs composite are actually the carbon-encapsulated Fe as can be seen in the TEM observation. Fe:CNTs composite are actually the carbon-encapsulated Fe as can be seen in the TEM observation. When the AD sample was dipped into the methanol solution, the hydrophobicity of the CNTs When the AD sample was dipped into the methanol solution, the hydrophobicity of the CNTs rendered the porous Fe:CNT composite structure to be collapsed. Therefore, the *methanol-treated* (MT) sample sample with less porosity could be obtained as shown in Figure 1a [16]. Finally, the MT sample was *heat-*with less porosity could be obtained as shown in Figure [1a](#page-2-0) [\[16\]](#page-12-8). Finally, the MT sample was *heat-treated* at 400 [◦]C in air for 2 h to oxidize iron to iron oxide, thereby the Fe₂O₃:CNT composite was formed (sample HT). The carbon layer was still preserved on the surface of Fe₂O₃ even after heat treatment.

In addition, pure CNT and pure iron oxide structures were prepared for the comparative study.

In addition, pure CNT and pure iron oxide structures were prepared for the comparative study. The pure CNT (CNT-p) structures were prepared via the same arc-discharge method. However, the pure CNT (CNT-p) the catalytic metals in CNTs were thoroughly removed by following the acid treatment as shown in Figure 1, CNTs were thoroughly removed by following the acid treatment as shown in Figure [1b](#page-2-0). CNT-p showed a mat-like structure of the closely stacked SWCNTs morphology.
The pure hematities in the pure hematite structure in the pure of the closely stacked SWCNTs morphology. The pure hematite structure (H-p) was fabricated through a chemical method using an iron solution in $\frac{1}{2}$ dimethylformamide (DMF, $(CH_3)_2NC(O)H$), followed by the heat treatment at 500 °C (Figure [1c](#page-2-0)).

2.2. Morphology and Structure Characterization

Most characterizations and measurements were performed from the samples with 20 min of the arc-discharge process, which showed the highest sensing performance. The morphologies of the fabricated structures were investigated by field-emission scanning electron microscopy (FE-SEM, JSM 700F, JEOL, Tokyo, Japan) and transmission electron microscopy (TEM, JEM-ARM200F, JEOL, Tokyo, Japan). The crystalline structures and chemical binding natures were examined by X-ray diffraction (XRD, X'pert PROMPD, PANalytical, Amelo, The Netherlands) with Cu Kα radiation and Raman spectrometry (Horiba Jobin Yvon, LabRAM HF-800, Horiba, Paris, France), respectively.

2.3. Sensing Property Measurements

The gas sensing properties were measured using a Picoammeter/Voltage source (Keithley 6487, Keithley Instruments, Solon, Ohio, USA) in the homemade measurement system [\[34\]](#page-13-8). Figure S2 displays the schematic of the sensor measurement system equipped with the gas flow vacuum chamber, mass flow control (MFC) system, substrate heater, and computer. Sensor structures were degassed in the vacuum chamber at 300 ◦C before the sensing measurement to remove any preadsorbed water molecules. The target gases such as $NH₃$, $H₂S$, $H₂$, CH₄, etc. were supplied by gas cylinders and diluted up to 1000 ppm by nitrogen. The gases were further diluted in dry air by varying the gas concentration at a constant dry air flow rate of 100 sccm when fed into the test chamber. The gas concentrations were determined by $C(ppm) = C_{std}(ppm) \times f/(f+F)$ [\[36,](#page-13-9)[37\]](#page-13-10), where f and F are the flow rates of the analyte gas and the carrier gas, respectively, and C_{std} (ppm) is the concentration of the analyte gas in the gas cylinder. $C_{std}(ppm)$ was 1000 ppm balanced with nitrogen for all of the gases. Dry air was used as a carrier gas, and the gas flow rate was controlled by a mass flow controller. The resistances were measured by applying 1 V bias between the two electrodes with flowing air (R_0) or the target gas (R_g) into the chamber.

3. Results and Discussion

The sample AD (the Fe:CNT composite) showed a highly porous morphology with large volume among the SWCNTs as shown in the SEM image (Figure [2a](#page-4-0)). The methanol treatment led the porous composite structure to collapse and form a compact mat-like structure (sample MT) due to the hydrophobicity of the SWCNTs (Figure [2b](#page-4-0)) [\[38](#page-13-11)[,39\]](#page-13-12). The sample HT (the Fe₂O₃:CNT composite) was obtained by thermal oxidation of the MT sample, in which Fe nanoparticles were oxidized to $Fe₂O₃$ nanoparticles while preserving the porosity of the MT sample as well as the thin carbon layer on the surface (Figure [2c](#page-4-0)). Transmission electron microscopy (TEM) images clearly presents the dispersed hematite particles on the SWCNT network in the HT sample (Figure [2d](#page-4-0)). The entangled SWCNT bundles with the diameter of \sim 10 nm supported Fe₂O₃ nanoparticles, of which the size range is large from several to ~30 nm. The high-resolution TEM image with the electron diffraction pattern of the inset (Figure [2e](#page-4-0)) confirms the crystalline Fe₂O₃ nanoparticles in the Fe₂O₃:CNT composite structure. The hematite particles were encapsulated by amorphous or graphitic carbon layers as shown by Figure [2e](#page-4-0),f. The carbon layers encapsulating the Fe and $Fe₂O₃$ nanoparticles were preserved during the oxidation process at 400 $^{\circ}$ C.

Figure 2. Top-view SEM images of the (a) AD, (b) MT, and (c) HT samples. (d) The TEM image of HT showing hematite nanoparticles entangled with the single-wall carbon nanotube (SWCNT) network. High-resolution (HR)TEM images confirms the existence of (e) amorphous and (f) graphitic carbon layers on the surface of hematite particles. layers on the surface of hematite particles. layers on the surface of hematite particles.

[Th](#page-4-1)e XRD patterns of the AD and HT samples are shown in Figure 3a. Those of pure $Fe₂O₃$ (H-p) and SWCNT (CNT-p) are displayed together for the comparison. The diffraction peak at \sim 44° matches (400) of Fe in the AD sample, indicating the distribution of Fe nanoparticles on SWCNTs. Meanwhile, diffraction peaks corresponding to the polycrystalline hematite ($Fe₂O₃$; JCPDS 00-024-0072) and graphite (JCPDS 98-002-0123) were identified in the HT sample. The Raman spectra of the composites are shown in Figure 3b. The [G-](#page-4-1) and D-mode peaks at \sim 1600 cm⁻¹ and \sim 1400 cm⁻¹ represent the graphitic lattice and the defective graphite structure, respectively, therefore the intensity ratio of G to D peaks can be considered a measure of the crystalline characteristic of the single-wall CNT $[40,41]$ $[40,41]$ $[40,41]$. All composites revealed the similar intensity ratio of G to D peaks indicating the preserved graphitic character in SWCNT during the process. This indicates that the crystallinity of the CNT in the composites was not noticeably degraded after the methanol or heat treatment, as exhibited by the sharp G-mode peak with respect to the D-mode peak. sharp G-mode peak with respect to the D-mode peak. sharp G-mode peak with respect to the D-mode peak.

Figure 3. (a) XRD patterns of the HT and AD samples along with the pure CNT and $Fe₂O₃$ samples. The peaks confirmed Fe, polycrystalline hematite, and graphite. (b) Raman spectra of the AD, MT, and HT samples. (c) Current versus voltage curves of the AD, MT, and HT composite structures.

The electrical properties of the composite structures are measured as shown in Figure 3c. All composite samples exhibited excellent ohmic contacts with the Au electrodes at RT in air as indicative by the linearity in the current versus voltage curves. The high resistance of \sim 3.1 \times 10⁵ Ohm of the as-deposited Fe:CNT composite (AD) originates from the high porosity of the structure. The high porosity in the entangled nanowires comprises relatively a small number of contacts among the CNTs, which leads to the high resistance by a small cross-section area for the current path. The other Fe:CNT composite after the methanol treatment, the MT sample, shows two orders of magnitude lowered resistance of $~6.8 \times 10^3$ Ohm. The methanol treatment led to the collapse of the porous structure followed by formation of the compact mat-like structure [38,39], in which the cross-section area for the current path is large due to the great increase in the number of contacts among the CNTs. HT reveals the same compact structure with MT, however, Fe nanoparticles were oxidized to semiconducting oxide particles, $Fe₂O₃$. Despite similar compact structures between MT and HT, the much higher resistance of Fe₂O₃ than Fe caused a far increase in the resistance, ~1.3 \times 10⁴ Ohm. A partial burn-out of the SWCNTs could contribute to the increase of the resistance in the HT structure [38].

The resistance changes of the HT composite toward 500 ppm $NH₃$ gas diluted in dry air were measured at differen[t t](#page-5-0)emperatures, as shown in Figure 4a. The increase of the resistance upon exposure to the reducing gas like NH_3 indicates that the HT composite is a p-type sensor, in which the positive charge carrier hole (h^+) is supplied to the adsorbed NH₃ molecules, thereby enabling ionosorption (e.g., NH₃ + h⁺ \rightarrow NH₃⁺ ad). The change of the resistance was highest at RT, however it decreased by the increase of the temperature. The similar p-type semiconducting sensing behaviours and the temperature dependence were observed in the Fe:SWCNT composite (AD and MT samples) as shown in Figure 4 b. The RT s[en](#page-5-0)sing response was attributed to the molecular adsorption of NH₃ on the sensor (not combustion of NH_3). Furthermore, the p-type behaviours in the sensing mechanism indicates that p-type SWCNTs are the main contributor for the charge exchange during NH₃ adsorption.

Figure 4. (**a**) The response-recovery curves of the HT structure measured for 500 ppm NH3 with **Figure 4.** (**a**) The response-recovery curves of the HT structure measured for 500 ppm NH³ with varying temperatures. (**b**) The temperature dependence of the response levels of the AD, MT, and HT varying temperatures. (**b**) The temperature dependence of the response levels of the AD, MT, and HT $(500$ ppm $NH₃)$ structures.

The RT response-recovery curves of the composite structures (AD, MT, and HT) are presented The RT response-recovery curves of the composite structures (AD, MT, and HT) are presented in Fi[gu](#page-6-0)re 5a. The response and recovery times of the HT structure were \sim 1.2 and \sim 1.8 min, respectively, as estimated in previous studies [\[8,](#page-12-9)[9\]](#page-12-10). The measurements from pure SWCNT (CNT-p) and pure hematite (H-p) structures with 500 ppm NH₃ are also plotted for comparison. The corresponding resistance changes of the sensor stru[ctu](#page-6-0)res are presented in Figure 5b. It can be immediately noted that the H-p sensor with very high resistance showed negligible response and the CNT-p sensor with very low resistance also showed a small response to NH₃ at RT. However, the composite-type sensors revealed the enhanced chemoresistive response level. The observed sensing response with the composites is elucidated by the synergistic interplay between the hole carrier concentration in the transducer and the adsorption sites density of the receptor. Holes are supplied by p-type SWCNTs, of which concentration is directly translated to the sensor resistance. The density of adsorption sites depends on the physical and chemical nature of the nanoparticles distributed on SWCNTs. We thoroughly investigate the synergetic effect in the sensing response by examination of the electronic and morphological properties of the structures.

Figure 5. (**a**) Sensor response-recovery characteristics of AD, MT, and HT structures to 500 ppm **Figure 5.** (**a**) Sensor response-recovery characteristics of AD, MT, and HT structures to 500 ppm ammonia at room temperature (RT). The responses of the composites showed a synergetic effect ammonia at room temperature (RT). The responses of the composites showed a synergetic effect compared with pure hematite (H-p) and pure SWCNT (CNT-p). (**b**) The same presented by the change compared with pure hematite (H-p) and pure SWCNT (CNT-p). (**b**) The same presented by the change in resistances. in resistances.

Ionosorption is chemical adsorption (chemisorption) of the gas molecule on the material surface Ionosorption is chemical adsorption (chemisorption) of the gas molecule on the material surface as an ionic state, which can be completed by either capture or release of electrons by or from the material, respectively. Therefore, a molecule impinging on the receptor can end up with adsorption followed by the charge exchange with the transducer. The charge supplied to or extracted from the transducer leads to a resistance change of the transducer. The ratio of resistances before and after gas adsorption (R_o and R_g, respectively) is taken as the sensor response signal, which is defined by Equation (1),

$$
S = \frac{R_g}{R_o},\tag{1}
$$

for sensing of $\overline{S} = D / D$ has beed for \overline{S} and \overline{S} reducing \overline{S} and $\overline{S$ reverse (S = R_o/R_g) can be defined for sensing oxidizing gases on p-type doped materials or reducing ϵ for sensing of oxidizing gases on n-type doped materials or reducing gases on p-type materials. The gases on n-type materials.

The simple condition, the uniform thin film oxide sensor with a thickness (t), is illustrated in Figure [6a](#page-7-0). The resistance is inversely proportional to the thickness, $R_0 = At^{-1}$ (A is arbitrary). If a Figure 6a. The resistance is inversely proportional to the thickness, $R_0 = At$ (A is arbitrary). If a reducing gas adsorbs by the hole supply from the p-type film (such as the NH₃ adsorption on SWCNT), the surface region becomes depleted of holes with the depletion depth (d) from the each side, leading the surface region becomes depleted of holes with the depletion depth (d) from the each side, leading \mathbf{S}_{S} the shapes of the film position becomes $\mathbf{S}_{\text{S}} = \lambda(t - 2\lambda)^{-1}$. Folynthese the spanned of the thin film to the change of the film resistance, $R_g = A(t - 2d)^{-1}$ [\[36\]](#page-13-9). Therefore, the response of the thin film the thin film sensor is given by Equation (2), sensor is given by Equation (2),

$$
S = \frac{t}{t - 2d}.\tag{2}
$$

Figure 6. The schematic showing nanostructured sensor conditions with different performance. (**a**) **Figure 6.** The schematic showing nanostructured sensor conditions with different performance. (**a**) The structural dimension of the sensor material is far greater than the depletion depth. The response is small due to too high conductance by the great conduction region. (b) The dimension of the structure approaches the depletion depth, which is the condition of the maximum nano-size effect in sensing. sensing. (**c**) The dimension of the structure is smaller than the depletion depth. Too high resistance (**c**) The dimension of the structure is smaller than the depletion depth. Too high resistance leads to the negligible modulation of the resistance followed by the small response during chemisorption on the sensor. Note the surface adsorption sites are all occupied in the condition of (a) and (b), but are partially occupied in (c) due to the limited charge carriers in the structure. (d) The increase in both charge carriers and adsorption site density in optimized composite structures can reveal the high sensing capability like the condition of (b).

 (cm^{-3}) and the areal density of molecular adsorption on the receptor (cm^{-2}) , respectively, in the steady S approaches the unity (= 1) or negligible response in the condition of $t \gg d$ (Figure 6a) [\[10\]](#page-12-3). The nano-size effect in gas sensing is observed by the enhancement of response as thickness (t) approaches twice of the depletion depth, i.e., $t = \sim 2d$, of which the condition is illustrated in Figure 6b. The nano-size effect is highest when $t = \sim 2d$ or the film thickness is comparable with the depletion depth in the given doping concentration. Since the depletion in the transducer occurs by the molecular adsorption of the gas phase on the receptor surface and consequent charge extraction, the total depletion condition is given by $n_d t = \sim N_{ad}$, where n_d and N_{ad} are the carrier concentration of the transducer state for a given gas concentration. Considering the resistance and the adsorption site intensity in the structure, the difference in the sensing response among AD, MT, and HT (see room temperature data in Figure [4b](#page-5-0)) can be elucidated by the sensor structural conditions between Figure [6a](#page-7-0),b.

However, in the case of t < 2d, the total charges in the transducer structure are smaller than the steady-state adsorption molecules ($n_{\rm d}t < N_{\rm ad}$). Only part of the steady-state adsorption sites can be occupied. The completely depleted state in the transducer before and after the gas adsorption is depicted in Figure [6c](#page-7-0), where the absence of the sensing response, i.e., $S = \sim 1$, is detected. It should be noted that Equation (2) cannot be applied to this condition. The maximum response as proposed in Figure [6b](#page-7-0) begins to decline as the thickness decreases like the schematic in Figure [6c](#page-7-0). We already called this the declining response with the decrease in the sensor dimension below the depletion depth scale as 'nanosize effect limit'. We had repeatedly observed the nanosize effect limit in several oxide gas sensors [\[9–](#page-12-10)[11,](#page-12-4)[42\]](#page-13-15). We have to note that both of the nanosize effect (increase in the sensing response with decreasing the sensor size towards the depletion depth scale) and the nanosize limit (decrease in the sensing response with further decreasing the sensor size below the critical limit of the depletion depth) are conceived from the independence between the receptor and transducer action in the single-body

scheme of the gas sensor. Therefore, simultaneous control of the dimensions of the oxide element, carrier concentration, and adsorption site density is required to achieve the maximum response signal in the conventional single-body oxide sensors.

To discuss the synergetic effect of the composite sensors, we need to understand the origin of zero and negligible response levels from the H-p and CNT-p sensors, respectively, as shown in Figure [5a](#page-6-0). Detection of NH₃ in CNT-based sensors at RT has been reported [\[12](#page-12-5)[–17\]](#page-12-6), and the relatively good recovery at RT was available due to the weak adsorption binding between CNT and NH₃ [\[43\]](#page-13-16). However, the CNT-p exhibited a small response level (S = ~1.02 or $R_g = \sim R_o$ in Equation (1)), indicating that the resistance modulation in the SWCNT by the $NH₃$ adsorption is very small. The small response is attributed to the relatively high hole carrier concentration (i.e., high conductance in SWCNTs) compared with the small adsorption site density of the SWCNTs ($n_d t >> N_{ad}$). This case corresponds to the condition schemed in Figure [6a](#page-7-0), where the adsorption sites are occupied at the steady state, however, the consequent surface deletion depth is relatively small.

Meanwhile, the origin of the no response $(S = \sim 0)$ in the H-p sensor (Figure [5a](#page-6-0)) is different with that in the CNT-p sensor. It is reported that an n-type hematite sensor responded to ammonia at a high temperature like other oxide gas sensors [\[26\]](#page-13-1). However, the hematite film exhibited an agglomeration among nanometric hematite particles, thereby revealing a very high resistance ($>\mathsf{G}\Omega$) due to fully depleted electron carriers as shown in Figure [5b](#page-6-0). The semi-insulating hematite film corresponds the condition of $n_{ox}t << N_{ad}$ as presented in Figure [6c](#page-7-0). Ionosorption of 500 ppm NH₃ molecules followed by the release of electrons into the hematite could not lead to any detectable resistance change in the H-p sensor, as manifested by the nearly zero response.

Contrary to the poor sensing responses of the SWCNT and hematite, the enhanced response in their composite structures can be understood by investigation about their electronic and morphological structures. Namely, the resistance of the Fe:SWCNT composite is comprised by competition between the high-resistance Schottky contact between the Fe and SWCNT and low-resistance ohmic contact among the SWCNTs. Therefore, the resistances of the composites are located in between that of CNT-p and H-p (Figure [5b](#page-6-0)), which is directly reflected to the operating condition. The sensor operating conditions of the composites lie between the conditions presented in Figure [6a](#page-7-0),c. Meanwhile, the proposed morphology of the composite sensors with the enhanced sensing response is depicted in Figure [6d](#page-7-0). The high-performance composite structure can be designed by consideration about two aspects. (1) The carbon-encapsulated Fe (or $Fe₂O₃$) nanoparticles with great surface area work as receptors for the NH₃ adsorption, and (2) the nanoparticle/SWCNT heterojunctions decrease the conductance of the SWCNT transducer. Both effects cooperatively push to the condition of Figure [6b](#page-7-0) of higher response.

The effect of concentration and distribution of $Fe₂O₃$ nanoparticles on the sensor response of composites were examined as well. The $Fe₂O₃$ concentration in the $Fe₂O₃$:SWCNT composites could be increased by adding more Fe wires into the graphite rod during the co-arc-discharge process. The synthesis using the more Fe wires produced the composite with the higher carbon-encapsulated $Fe₂O₃$ concentration. The response to 500 ppm $NH₃$ of the structures are shown in Figure [7a](#page-9-0). The higher responses were obtained with the more Fe wires due to higher receptor concentration in the composites. Since the NH³ adsorb on SWCNT as shown by the response of the CNT-p sensor, the high distribution of carbon-encapsulated hematite particles will increase the specific adsorption sites for NH3.

Whereas, when Fe was sputter deposited on the mat-like SWCNTs thin film, a thin film of Fe seats on the SWCNT mat. The following oxidation process converts Fe to $Fe₂O₃$ nanoparticles agglomeration without the carbon shell layer. The sputter-based composite will show a morphology of thin film $Fe₂O₃$ nanoparticle receptor piled up on the mat-like SWCNT transducer. The cross-section views of the structures are shown in Figure S3 that signifies increase in the thickness with the sputtering time. The sputter-based composite also revealed higher response with the $Fe₂O₃$ thickness (Figure [7b](#page-9-0)). It was already repeatedly shown that the $NH₃$ molecules can adsorb on Fe or Fe₂O₃ nanoparticles at RT via the molecular adsorption reaction $NH_3 \rightarrow NH_3^+$ ad $+e^-$ or the dissociative adsorption

reaction $NH_3 \rightarrow NH_{2ad} + H^+_{ad} + e^-$, etc. [\[19–](#page-12-11)[21\]](#page-12-12). In this way, either the ammonia adsorption on carbon-encapsulated Fe₂O₃ or the direct adsorption on Fe₂O₃ observed in Figure 7 can be supported.

Figure 7. The response to 500 ppm NH₃ of the Fe₂O₃:SWCNT composite structures (a) fabricated by the arc-discharge method with varying number of iron wires inserted to the graphite rod from five to 50 wires, and (b) fabricated by sputter deposition of Fe for 30 and 60 min on the SWCNT mat structures.

The microscopic view about the ammonia adsorption on the carbon-encapsulated hematite nanoparticle is presented in Fig[ure](#page-9-1) 8. The $Fe₂O₃/SWCNT$ heterojunction results in the formation of the hole depletion region in the SWCNT. When the NH_3 molecules adsorb on the carbon-encapsulated Fe₂O₃ receptor at RT, electrons released via the adsorption reaction are transferred to the SWCNTs to recombine with holes. The electron transfer can be achieved by either surface conduction or tunneling through the hematite particles. The resultant increase in the hole depletion depth in the SWCNT transducer is translated to the sensor signal following Equation (2). From this perspective, an enhanced sensor response, i.e., far increased resistance modulation of the SWCNT transducer, is available by increase in the adsorption site density for the NH₃ molecules. The higher adsorption can be achieved by the higher concentration of nanoparticle receptors.

molecules on the carbon-encapsulated $Fe₂O₃$ transport to SWCNTs by surface conduction or tunneling. The electrons recombine with holes in SWCNTs, which expands the depletion region at the Fe₂O₃/SWCNT heterojunction. Figure 3. **CEREMATIC OF THE CARBON-ENGAPTER CARBON-ENGAPTER CONTACT THE CONTACT OF STATE** \overline{a} \overline{b} **Figure 8.** Schematic of the carbon-encapsulated $Fe₂O₃$ nanoparticle in contact with the SWCNTs

We also fabricated the Ni₂O₃:SWCNT as the p-type-oxide:SWCNT composite structure by the dependence of sensing responses to 100 ppm NH_3 is presented in Figure S4. All results follow those same method used for the preparation of the $Fe₂O₃$:SWCNT composite sensor. The temperature dependence of sensing responses to 100 ppm NH3 is presented in Figure S4. All results follow those sensing follow from the Fe₂O₃:SWCNT composite. This indicates that the enhanced SWCNT sensor performance can be achieved by adding any type of receptor if it can provide adsorption sites for NH3.

The various ammonia sensing properties of the HT sensor ($Fe₂O₃$:CNT composite) at RT are summarized in Figure 9. In the test of the repeatability of sensing, the baseline resistance after recovery continued to increase by the repetition of the sensing cycles as shown [in](#page-10-0) Figure 9a. The chemical forms of ammonia adsorption can be variable in [rea](#page-12-11)[lity](#page-12-12) [19–21], and a finite amount of H^+ and/or H_2^+ ${\rm H_2^+}$, which binds more strongly with the adsorption sites than ${\rm NH_3^+}$, remains adsorbed during the recovery cy[cle \[](#page-12-11)19]. The remnant adsorption can be accumulating as the response-recovery cycles are repeated. The linearity of the HT sensor at RT for ammonia detection was measured at the various are repeated. The linearity of the HT sensor at RT for ammonia detection was measured at the various concentrations in the range from 50 to 500 ppm as shown in Figure 9b. The responses of the HT sample concentrations in the range from 50 to 500 ppm as shown in Fi[gu](#page-10-0)re 8b. The responses of the HT to other reducing and oxidizing gases were also examined, which shows high selectivity of the sensor to ammonia a[t R](#page-10-0)T (Figure 9c). The preliminary examination shows that the composite structure can be further developed to commercial sensor structures. It is also interesting to not[e i](#page-10-0)n Figure 9c that the composite structure can be used as a H_2S sensor at high temperatures with good selectivity.

Figure 9. (a) Sensing reproducibility of the HT sample showing good repeatability but with increasing baseline resistance for 500 ppm NH₃ concentration at RT or ~25 °C. (**b**) Linearity of HT measured in the concentration range between 50 and 500 ppm NH₃ at RT. (**c**) Gas selectivity of HT tested at various temperatures for each of the 500 ppm concentrations. (**d**) Humidity dependent resistance of HT measured at RT under varying $NH₃$ concentration and RH.

sensor at RT. The H₂O molecules strongly affect the sensing signals via adsorption on the surface of the sensor. At low temperatures below 400 K, preferentially dissociated water molecules form the sensor. At low temperatures below 400 K, preferentially dissociated water molecules form the the sensor. At low temperatures below 400 K, preferentially dissociated water molecules form the chemisorption layer of hydroxyl ions on the very surface, and further water molecular impingement forms multilayers of physisorbed water molecules [\[44](#page-13-17)[–47\]](#page-14-0). The water molecular adsorption provides the ionic conduction path, thereby increasing the conductance of the oxide. In addition, electrons are released via the water molecular adsorption [\[3\]](#page-12-13), which also contributes to the further increase of the conductance in the case of n-type semiconducting oxides. We found that the n-type ZnO thin conductance in the case of n-type semiconduction \mathbf{r}_1 and \mathbf{r}_2 the case of \mathbf{r}_2 this case of \mathbf{r}_1 and \mathbf{r}_2 the n-type \mathbf{r}_1 and \mathbf{r}_2 this case of \mathbf{r}_2 the n-type \mathbf{r}_1 and $\mathbf{r$ film can be used as a selective humidity sensor because it shows the conductance increase by relative The humidity in the air is considered one of the most critical issues to operate the oxide gas

humidity (RH) (Figure S5). Rapid decrease of the sensing response above ~60% RH may account for an enhanced conduction due to several layers of the physisorbed water molecules. The conductivity change resulting from the physisorbed water molecules as well as the simultaneous electron injection into the oxide can manifest the humidity sensing of the ZnO.

Whereas, the behaviour of the p-type $Fe₂O₃:CNT$ composite sensor is opposite with ZnO as shown in Figure [9d](#page-10-0), in which the conductance of the sensor was decreased by the humidity (see the curve with the zero NH_3 flow). Since SWCNTs also respond to water molecules [\[48\]](#page-14-1), the opposite humidity effect on the sensor conductance indicates that a part of the holes in the SWCNTs are compensated by the released electrons from the chemisorbed water molecule. Figure [9d](#page-10-0) shows that the NH₃ gas in a ppm concentration range competitively adsorb on the surface in the humidity as indicative by sensing signals. Note that the ionic conduction by the adsorption of water molecules is not significant. Therefore, the ammonia sensing signal of HT in the humid condition still can result from the hole conduction mechanism in the SWCNT transducer. As observed, the ammonia gas concentration cannot be precisely determined in humidity unless the humidity is measured separately. The simplest solution is the monitoring of the humidity at the same location. Many semiconductor type humidity sensors have been developed to be mounted together with the chemoresistive sensor [\[45\]](#page-14-2). In this case, a microprocessor to calibrate the signals based on the humidity is required as well.

4. Conclusions

An ammonia sensing response was thoroughly studied in the Fe:SWCNT, $Fe₂O₃$:SWCNT, and $Ni₂O₃$:SWCNT nanocomposite structures, in which carbon-encapsulated metals or metal oxide nanoparticles are finely distributed among the SWCNT bundles. The much higher sensing response of the composites than that of the pure hematite and SWCNT structures could be obtained by the greater charge modulation in the sensor structure. Such condition could be motivated by the increase in the number of molecules adsorbed on nanoparticles that formed the intimate contact with SWCNTs. The distribution of fine nanoparticles of Fe, $Fe₂O₃$, and Ni₂O₃ in the composites increases the specific adsorption sites for NH3. In turn, the more adsorption of NH³ molecules accordingly leads to the wider depletion depth in the SWCNT structure. The synergetic effect that enhanced the sensing performance was elaborated by our new sensor scheme, in which the physically separated but electrically connected nanoparticles and SWCNTs function simultaneously as receptors and transducers, respectively, during the sensor operation. This understanding allows us to propose the new concept of a separated receptor and transducer scheme in the conduction-type gas sensors, which enable the optimization of the receptor and the transducer as independent materials and structures. Our study provides the guidance to choose the best receptor and transducer materials toward the development of the high-performance sensor that cannot be achieved in the existing design scheme.

Supplementary Materials: The following are available online at http://[www.mdpi.com](http://www.mdpi.com/1424-8220/19/18/3915/s1)/1424-8220/19/18/3915/s1, Figure S1: The arc-discharge synthesis system, Figure S2: The sensor measurement system and the sensor structure, Figure S3: The Fe₂O₃:CNT composite structures fabricated by sputter deposition, Figure S4: Sensing property of $\rm Ni_2O_3$:CNT composite structure, Figure S5: ZnO thin film humidity sensor property.

Author Contributions: N.M.H. conceived the sensor structures, performed most of the experiments, measurement, and analyses. He also wrote the manuscript. C.V.P. and J.R.J. drew some of the plots with the discussion, T.T.H., N.D.C., and N.D.Q. carried out XRD and SEM examinations with help in materials preparation. D.K. supervised the project. C.K. and D.K. revised the manuscript with the discussion.

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