

## Article

# Microwave Heating Improvement: Permittivity Characterization of Water–Ethanol and Water–NaCl Binary Mixtures <sup>†</sup>

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Abstract: Microwave heating offers a lot of advantages compared to conventional heating methods in the chemical reactions field due to its positive effects on reaction time and selectivity. Dielectric properties, and in particular permittivity, of substances and mixtures, are important for the optimization of microwave heating processes; notwithstanding this, specific databases are poor and far from being complete, and in the scientific literature very little data regarding these properties can be found. In this work, impedance measurements were carried out using a specially designed system to get the real and imaginary parts of the dielectric constant. The apparatus was tested in the estimation of permittivity of water–ethanol and water–NaCl mixtures, varying their composition to obtain a wide range of permittivity values. The results were compared to literature data and fitted with available literature models to verify the correspondence between them, finding that permittivity dependence on mixture composition can be effectively described by the models.

**Keywords:** Acree model; dielectric constant; ethanol; impedance; King and Queen model; microwave heating; binary mixtures; NaCl; permittivity; water

## 1. Introduction

Microwaves (MWs) refer to electromagnetic radiation in the frequency range of 300 MHz–300 GHz with a wavelength between 1 mm and 1 m [1]. MWs can be generated by high-power sources including magnetrons (used in microwave ovens and available at lower costs than other sources), klystrons, traveling wave tubes, and gyrotrons [2]. Electromagnetic energy propagates through space using time-varying electric and magnetic fields [3].

MW heating is a characteristic phenomenon that cannot be imitated by other heating methods: it can lead to internal heating, selective heating, the formation of hotspots, local heating, superheating, and non-uniform heating [4]. There are two main mechanisms of MW heating: dipolar reorientation and ionic conduction [5]. Dipolar reorientation is mainly connected with the presence of water, dipoles, or charged materials in general. Water molecules are dipolar and they try to follow the electric field which alternates at very high frequency. For a commonly used microwave frequency of 2450 MHz, the electric field changes directions  $2.45 \times 10^9$  times per second, making the dipoles move with it [6]. Such rotation of molecules means heat generation inside the material; therefore, MWs can generate significant volumetric heat in materials containing high amounts of water [7]. The second major



mechanism is ionic conduction linked to the ability of ions to migrate under the influence of the electric field and to generate heat [5].

The heating efficiency of this process can reach values of about 80–85%, which are higher than the efficiencies of the conventional heating methods [8]. MWs can be more efficient and economic than conventional heating methods, as the heat transferred through this technique is generated directly in the material through molecular interactions, instead of originating from external surfaces (as happens in the case of conventional methods) and not conducted from the surface of the heating source into the sample [9]. So, the core of the material gets heated up quickly and the heat flows outwards from the core to the surface. Thus, in microwave heating, there is an inverse heating profile due to convective and radiative heat loss from the surface of the material to the surroundings [10].

In reacting systems, this selective volumetric heating mechanism allows several advantages [4]: (i) it brings an important reduction of reaction times [11]; (ii) it mitigates the reaction conditions [12]; (iii) it provides selective heating with an increase of product yields and purities [13]. In addition, using this way of heating makes the process easier to control and safer, also reducing the complexity of the exchange units and is more environmentally friendly [14].

After the second world war, due to the discovery of the potential of this technique, a slow increment of interest around it was registered [1], which allowed researchers to gradually move from a laboratory-scale approach to an established method that is now also heavily used in industrial applications. Currently, microwave heating under the commercial frequency of 915 or 2450 MHz has been increasingly applied in several fields, including organic and pharmaceutical chemistry, solid-phase peptide and polymer synthesis, material science, nanomaterials research [15], and a variety of chemical [16] and biochemical processes, like enzyme reactions [17], soil treatment [18], disinfection [19], biomass pyrolysis [20], and metallurgy [21].

Microwave heating is based on the dielectric properties of the material and can occur both inside and in the boundaries, where the latter phenomenon is explained by the Maxwell–Wagner polarization [22]. Dielectric properties influence the reflection of electromagnetic waves at the interfaces and the attenuation of the wave energy within materials, which determines the amount of energy that can be absorbed and converted into heat [23]. The dielectric properties of materials that are related to the interactions with microwaves are permeability, permittivity, and electrical conductivity [24]. It is generally accepted that, for most dielectric materials, the permeability presents no or very small contribution to dielectric heating, and so it is usually not considered [25]. Knowing the value of permittivity, on the contrary, is useful to estimate the reaction temperature [15] and to optimize the heating process in order to minimize the energy consumption. The penetration depth of the material is an important parameter for the heating processes efficiency improvement, and it depends on the dielectric properties of the substance [26]. Microwave heating also depends on other elements, i.e., the applicator characteristics, the geometry of the object to be irradiated, the mode of wave propagation, and the radiation frequency and to the temperature, but the dielectric properties of the material have a central role.

In addition to chemistry, the knowledge of material dielectric properties is fundamental to improve MW heating in other interesting fields like, for example, food technology [27], pyrolysis [28], hyperthermia cancer treatments [29], and sterilization of agricultural lands [30].

Despite the important role that permittivity data play in the knowledge of the microwave heating properties, there is still a lack of fundamental data on the dielectric properties of substances and materials, which generates several difficulties with the scaling up from laboratory units to industrial equipment. So, the goal of this work is to provide some useful information about the dielectric properties of a water–ethanol system, which can be representative of many typical solvents of industrial interest, due to the common use of the alcohols in the organic chemistry. In addition to this, also the dielectric properties of water–NaCl mixtures were investigated to extend the applicability of the measurement technique. The measurement method and the collected information suggest how the dielectric characterization of pure substances and binary mixtures can be done with the purposes of the reaction process optimization and the minimization of its energy consumption.

#### Elements of Dielectric Theory

As already introduced in the previous main section, permittivity is a very important parameter in the characterization of the behavior of a material when exposed to an electromagnetic field. Permittivity is defined as the ability to store electrical energy of a non-conductive material subjected to an electrical field [31]. In the frequency (f) domain, this parameter ( $\varepsilon$ ) is expressed as:

$$\varepsilon = \varepsilon' - j\varepsilon'',\tag{1}$$

where  $\varepsilon'$  and  $\varepsilon''$  are, respectively, the real and the imaginary part, and *j* the imaginary unit. The real part of permittivity ( $\varepsilon'$ ) is also known as the dielectric constant and it represents the energy storage capacity of a material exposed to an electromagnetic field or, in other words, the ability to polarize [32]. The charged molecules contained within materials, under an electromagnetic field, try to orientate following the field and storing electromagnetic energy [6]. This phenomenon is the so-called polarization phenomena: higher values of  $\varepsilon'$  represent a greater capacity to store electromagnetic energy due to the electronic charge orientation following the field [33]. Four different kinds of polarization phenomena can occur in materials: electronic, atomic, ion, and orientation polarization [34]. The first one occurs in neutral atoms when an electric field displaces the nucleus with respect to the electrons that surround it, resulting in a dipole moment that responds to the applied field, whereas atomic polarization results from nuclei displacement of different atoms in a molecule [35]. The orientation polarization exists only in polar materials and consists of the re-orientation of permanent dipoles caused by the electromagnetic field [36]. This is the dominant mechanism at microwave frequencies [37], persisting in a wide frequency range, approximately  $10^2-10^{10}$  Hz, and it depends on the material conductivity and temperature [34].

The imaginary part of permittivity ( $\varepsilon''$ ), on the other side, is related to the dielectric loss, which generally originates from the processes of conduction and polarization and it is known as loss factor [38]. So, materials with a high  $\varepsilon''$  dissipate more energy and are easier to heat than materials with a low  $\varepsilon''$  [26]. A perfect insulator has a great value of  $\varepsilon'$  and its electric charge can instantly react to the field by orientating according to this; however, most of the materials present a phase delay between the dipole alignment and the appearance of the electromagnetic field, so part of the radiation energy is converted into thermal energy. At radio and microwave frequencies, ionic conduction and dipole rotation are the dominant loss mechanisms [39]. In addition to the material ionic conductivity and dipole rotation ability, permittivity depends on the material composition [28] and texture [40], and to a lesser extent on pressure [41]; however, the parameters that mainly affect this variable are frequency and temperature [41]. The frequency influence, in the case of pure liquids, is described by the Debye model [42], where the relaxation time of the material is also taken into account. The relaxation time is a measure of the polarization ability of the material, as it represents the time delay on the material response to an electric field change; this parameter is correlated to the molecular conformation and, in general, increases with the size of molecules [43].

#### 2. Materials and Methods

#### 2.1. Measurement Method

Several techniques for permittivity measurement are available, but all methods have limitations of sample kind and especially in the frequency range.

Alcohols or other dielectric liquids can be considered as good solvents for many biological molecules, body tissues, blood, and bone marrow; therefore, an in-depth permittivity study of various common solvents is essential for chemical and biomedical research. Several techniques have been developed for the measurement of the complex permittivity of liquids. For instance, the most commonly used techniques are coaxial line measurements and capacitive techniques; also the waveguide, the open-ended waveguide, the open-ended coaxial line, the dispersive Fourier transform spectroscopy (DFTS), and the microwave resonant methods, have been applied [44]. In the case

of the present study, the parallel plate technique was used. This technique is characterized by the following advantages: it is relatively easy to use, non-destructive, it gives quick responses [45], and it is acceptably accurate ( $\pm$ 5%) [29]. For the measurement by this technique, the sample is packed between two electrodes, so realizing an electric condenser, and the value of permittivity is estimated from impedance measurements obtained with the use of an impedance analyzer or an LCR meter [33]. In this work, an impedance analyzer was used, as already done in previous work [29]. This kind of instrument is usually used to measure the transmission and reflection characteristics of devices and networks when a sinusoidal signal with time-variable frequency is applied. After this, the transmitted or reflected signal is compared with the transmitted signal and converted into an impedance measure. In particular, the impedance (*Z*) values were calculated using the following equation [46]:

$$Z_R = Z_0 \, \frac{1 + S_{11}}{1 - S_{11}},\tag{2}$$

where  $Z_R$  is the impedance of the measuring cell,  $Z_0$  is the reference impedance of the instrument, calculated using its calibration process, and  $S_{11}$  is the reflection coefficient that takes into account the electromagnetic waves that are reflected by the measurement device. To correlate the impedance measures with the dielectric ones, the following expressions derived from the dielectric theory [31] were used:

$$\frac{\varepsilon'}{\varepsilon_0} \propto C; \tag{3}$$

$$C = \frac{1}{\omega X};\tag{4}$$

$$\frac{\varepsilon''}{\varepsilon_0} \propto \frac{1}{R};\tag{5}$$

$$Z = R + jX; (6)$$

where *C* is the capacitance, *X* is the reactance, and *R* is the resistance of the system. The dielectric constant is inversely proportional to the reactance, while the loss factor is inversely proportional to the resistance. So, two calibration straight lines have been built, one where  $\varepsilon'$  is a function of the inverse of reactance, and another one where  $\varepsilon''$  is a function of the inverse of resistance, taking as the references two substances with known values of permittivity. This method allowed us to estimate the value of permittivity of the different mixtures analyzed here.

## 2.2. Design of the Parallel Plate Cell

The parallel plate system (shown in Figure 1), to be connected to the impedance analyzer, is a cell, the body of which is made of plastic material (PVC). The cell has two circular copper electrodes of 30 mm diameter and a spacing of 6 mm. In the volume included between the two copper plates, the liquid sample is inserted.

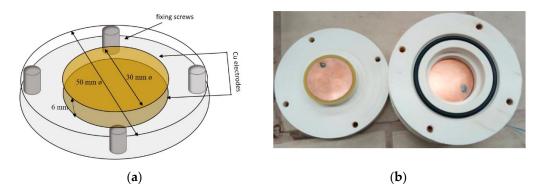
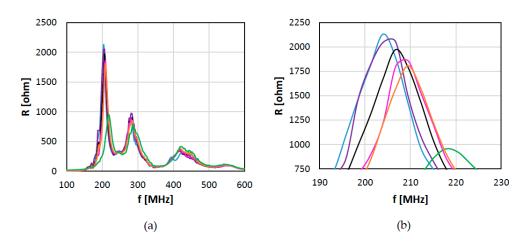


Figure 1. Sketch (a) and picture (b) of the measuring cell [47].

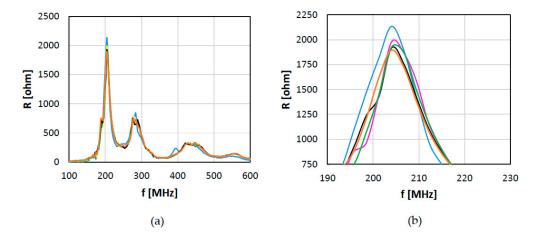
## 2.3. Experimental

The impedance analyzer used in this work was a Vector Network Analyzer (Hewlett-Packard, model 8720C). This instrument works in the range of frequencies between 50 MHz and 20 GHz, with a frequency resolution of 100 kHz. The cell was connected to the analyzer through a coaxial cable and an SMA connector. Water–ethanol and water–NaCl mixtures, with different compositions, were prepared and measured at room temperature (25 °C). Because of the different structure and varying dynamic response to the external field, each material shows a unique complex dielectric spectrum in the radio–microwave frequency range.

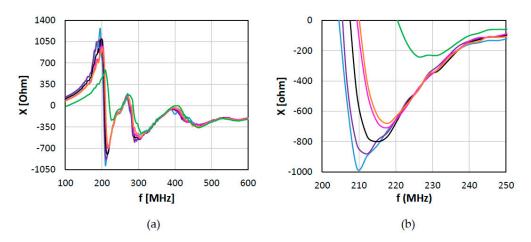
Analyzing the frequency spectra of *R* reported in Figures 2 and 3, and of *X* in Figures 4 and 5, we see that the maximum differences of these values among the various mixtures are located in the maximum peak zone for *R* and the minimum peak zone for *X*. This is true both for water–ethanol mixtures (Figures 2 and 4) and for water–NaCl mixtures (Figures 3 and 5).



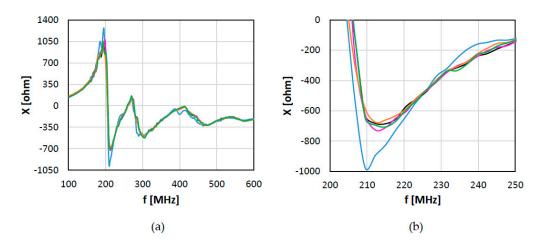
**Figure 2.** Spectra of *R* (**a**) and values of the maximum peak in the restricted range considered for the measurements (**b**), for water (–), 1-propanol (–) and water–ethanol mixtures with ethanol molar fraction of 0.007 (–), 0.219, (–), 0.495 (–), and 0.854 (–).



**Figure 3.** Spectra of *R* (**a**) and maximum peak values in the restricted range considered for the measurements (**b**), for water (–) and water–NaCl mixtures with NaCl molar fraction of  $2.3 \times 10^{-4}$  (–),  $4.5 \times 10^{-4}$  (–),  $1.35 \times 10^{-3}$  (–), and  $1.8 \times 10^{-3}$  (–).



**Figure 4.** Spectra of *X* (**a**) and values of the minimum peak in the restricted range considered for the measurements (**b**), for water (–), 1-propanol (–) and water–ethanol mixtures with ethanol molar fraction of 0.007 (–), 0.219, (–), 0.495 (–), and 0.854 (–).



**Figure 5.** Spectra of X (**a**) and values of the minimum peak in the restricted range considered for the measurements (**b**), for water (–) and water–NaCl mixtures with NaCl molar fraction of  $2.3 \times 10^{-4}$  (–),  $4.5 \times 10^{-4}$  (–),  $1.35 \times 10^{-3}$  (–), and  $1.8 \times 10^{-3}$  (–).

According to this, an indication can be obtained focusing on these peak values of *R* and *X* and, in particular, on the maximum values of *R* and the minimum values of *X*. Before carrying out the measurements, the calibration lines were built. Calibration lines for water–ethanol mixtures were obtained using water and 1-propanol with known permittivity values as references, so the measuring range was between 77.5 and 16 for  $\varepsilon'$ , and between 6.32 and 1.24 for  $\varepsilon''$  (values of the permittivity of the pure substances—water and 1-propanol, respectively) [41]. For the water–NaCl mixtures, instead, water and water–NaCl 0.1 N (0.584%) were chosen as the reference since the tests showed a flat trend of  $\varepsilon''$  as the salt increased over this concentration, so it was not useful to utilize solutions with higher salt concentrations. Considering this, the measuring range, in this case, was between 77.0 and 76.0 for  $\varepsilon'$  and between 59.28 and 1.24 for  $\varepsilon''$  [41], but in this case, the interest was mainly focused on the imaginary part measure. In Figures 2 and 4, we show that the R and X values of the water–ethanol solutions lie between those of the reference substances and that an increase of the ethanol concentration in the solution corresponds to a decrease of *R* (Figure 2), and to an increase of *X*. Similar conclusions can be formulated for NaCl–water solutions (Figures 3 and 5).

#### 2.4. Data Modeling

The experimental data were fitted using two literature models: the Acree model [48] and the King and Queen model [49].

The Acree model is a thermodynamic derivation one that finds application in the prediction of mixtures properties like density, viscosity, surface tension, molar volume [50], and solute solubility in binary solvent mixtures [51]. In this case, it was used in the form given in the literature [52], where to calculate permittivity of a binary mixture with water and alcohol, as was done also by Jouyban [53], was used; therefore, this was the most appropriate to describe the dielectric properties of water–ethanol mixtures, at least. The model equations, respectively for water–ethanol (Equation (7)) and water–NaCl (Equation (8)) mixtures, are the following:

$$\ln \varepsilon' = (1 - x_{Eth}) ln \varepsilon'_{W} + x_{Eth} ln \varepsilon'_{Eth} + x_{Eth} (1 - x_{Eth}) \cdot \sum_{i=1}^{2} K_i (x_{Eth} - (1 - x_{Eth}))^i;$$
(7)

$$\ln \varepsilon' = x_W \ln \varepsilon'_W + (1 - x_W) \ln \varepsilon'_s + x_W (1 - x_W) \cdot \sum_{i=1}^2 K_i (x_W - (1 - x_W))^i;$$
(8)

where *x* represents the molar fraction, the subscripts "*Eth*" and "*W*" respectively stand for ethanol and water, and the "*s*" one represents NaCl (salt); *i* indicates the *i*-component in the mixture and  $K_i$ are the model parameters. For the specific cases under study, the permittivity real part values for the pure substances are  $\varepsilon'_W/\varepsilon_0 = 77.5$  and  $\varepsilon'_{Eth}/\varepsilon_0 = 22.3$  [41].  $\varepsilon'_S/\varepsilon_0$  was set as a model parameter for different reasons: aside the impossibility of measuring, with the same experimental apparatus, the dielectric constant of the pure NaCl, this condition is well outside the range of composition that was studied and would be closer to a biphasic system than to a monophasic (homogeneous) one. Even if, in the cited literature, the model was applied only to the real part of the permittivity, in the present work it was used, with acceptable results, also for the imaginary one, just substituting  $\varepsilon$ " to  $\varepsilon'$  in Equations (7) and (8), and considering that, for the pure substances, the permittivity imaginary part values are  $\varepsilon''_W/\varepsilon_0 = 1.24$  and  $\varepsilon''_{Eth}/\varepsilon_0 = 5.62$  [41];  $\varepsilon''_S/\varepsilon_0$  was set, also in this case, as a model parameter. To calculate  $\varepsilon$ " of the water–salt mixtures, also  $\varepsilon''_W/\varepsilon_0$  was set as a model parameter to avoid the calculation problems due to the very high impact of NaCl on the  $\varepsilon''$  mixture value.

The King and Queen model, instead, was suggested in the literature for the representation of dielectric constant properties of mixtures [52,54]. It was introduced to model other physical properties like critical temperature, density, and compressibility factor [49]. This model uses the Padè approximation of polynomial functions and it is frequently used because its equation form describes the trend of different scientific quantities. In Equation (9) shows the form used to describe the dielectric constant for water–ethanol mixtures, whereas in Equation (10) shows the one used for the water–NaCl real part of permittivity regressions, both in the form proposed by Jouyban et al. [52]:

$$\varepsilon' = \frac{\alpha_0 + \alpha_1 x_{Eth}}{\beta_0 + \beta_1 x_{Eth}};\tag{9}$$

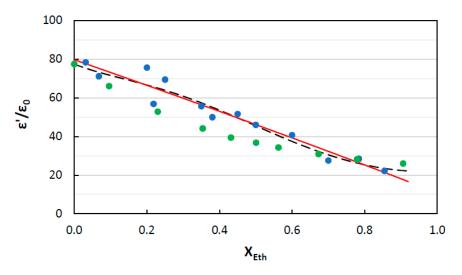
$$\varepsilon' = \frac{\alpha_0 + \alpha_1 x_s}{\beta_0 + \beta_1 x_s};\tag{10}$$

where  $\alpha_{0,1}$  and  $\beta_{0,1}$  are the model parameters. Also, in this case, the use of this model was extended to the imaginary part of permittivity, notwithstanding the absence of any application in the literature (as far as we know).

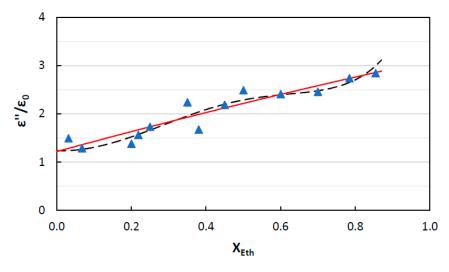
## 3. Results

The values of experimental  $\varepsilon' / \varepsilon_0$  (Figure 6) and  $\varepsilon'' / \varepsilon_0$  (Figure 7) of the water–ethanol mixtures are reported as a function of ethanol mole fraction. Looking at the graphs, the trend as a function of the composition is near to being linear for both  $\varepsilon'$  and  $\varepsilon''$ . We also compared the experimental values of  $\varepsilon'$ , for different compositions, to the water–ethanol mixtures data reported in the literature [55]. The experimental values are different from the literature values near the intermediate compositions,

and less for high water or high ethanol concentrations. The overall differences are quite small and the trend is very similar, so it is possible to deduce that the measurement technique is reliable and sufficiently accurate. Both the models, Acree and King and Queen in Figure 6, revealed their ability to accurately describe  $\varepsilon'/\varepsilon_0$ . The comparison between the two models shows that Acree is more accurate for the measured data.



**Figure 6.** Measured values (•), literature values [55] (•), Acree model curve (---), and King and Queen model curve (--) of  $\varepsilon' / \varepsilon_0$  for the water–ethanol mixtures, reported as a function of the ethanol molar fraction ( $x_{Eth}$ ).

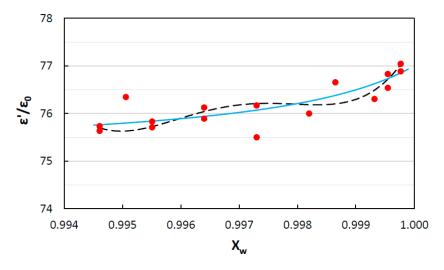


**Figure 7.** Measured values (**A**), Acree model curve (---), and King and Queen model curve (-) of  $\varepsilon'' / \varepsilon_0$  for the water–ethanol mixtures, reported as a function of the ethanol molar fraction ( $x_{Eth}$ ).

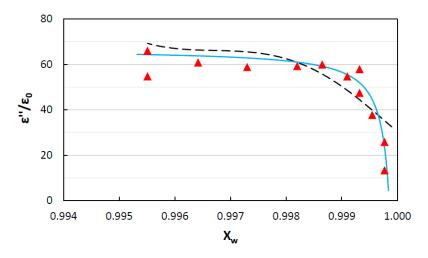
Regarding the values of  $\varepsilon''$ , it was not possible to make a similar comparison due to the lack (as far as we know) of values of this parameter for the same binary system in the literature. We used the model to test its efficiency for our experimental data. In this case, the dielectric loss is well described by the models.

Figures 8 and 9 report, respectively, the values of  $\varepsilon' / \varepsilon_0$  and of  $\varepsilon'' / \varepsilon_0$  of the water–NaCl mixtures as a function of composition. An increase in the salt concentration leads to a slight decrease of the mixture dielectric constant and a quick increase of the mixture dielectric loss, which ends with a flatter trend for high values of NaCl molar fraction (higher than 0.001). In this case, the data were modeled with the Acree and the King and Queen models, with acceptable results, especially for the dielectric

constant. Regarding the dielectric loss, the Acree model appears to be deficient in the description of the data, while the King and Queen one is better and also follows the plateau region that is reached at higher concentrations of NaCl.



**Figure 8.** Measured values (•), Acree model curve (---), and King and Queen model curve (--) of  $\varepsilon' / \varepsilon_0$   $\varepsilon'' / \varepsilon_0$  for the water–NaCl mixtures, reported as a function of the water molar fraction ( $x_w$ ).



**Figure 9.** Measured values ( $\blacktriangle$ ), Acree model curve (---), and King and Queen model curve (-) of  $\varepsilon' / \varepsilon_0$  for the water–NaCl mixtures, reported as a function of water molar fraction ( $x_w$ ).

All the values of the parameters used for the regressions and the related statistical indicators are reported for the Acree model in Table 1 while for King and Queen model in Table 2.

**Table 1.** Values of the model parameters and statistical indicators of the regression carried out with the Acree model; the superscript *K* indicates the single or the double quotes, depending on the row (real or imaginary part of permittivity); the subscript *i* indicates the second component of the mixture, depending on the row (ethanol or NaCl).

Mixture	$\epsilon^k W/\epsilon_0$	$\varepsilon^k_i/\varepsilon_0$	K <sub>0</sub>	<i>K</i> <sub>1</sub>	<i>K</i> <sub>2</sub>	SSE	RMSE	$R^2_{adj}$
W-Eth $\varepsilon'/\varepsilon_0$	4.350	3.105	0.362	1.145	-1.197	0.087	0.093	0.948
W-Eth ε" / ε <sub>0</sub>	0.215	1.726	-0.570	1.729	-2.953	0.114	0.105	0.846
W-S ε' / ε <sub>0</sub>	4.350	$3.387 \times 10^8$	$-5.938 \times 10^8$	$-3.4082\times10^8$	$-8.573 \times 10^7$	$6.673\times10^{-6}$	0.008	0.828
W-S ε" / ε <sub>0</sub>	195.548	3.414	$5.136 \times 10^{6}$	$1.037 \times 10^7$	$5.239 \times 10^{6}$	1.142	0.356	0.436

Mixture	$\alpha_0$	$\alpha_1$	$\beta_0$	$\beta_1$	SSE	RMSE	$R^2_{adj}$
W-Eth $\varepsilon'/\varepsilon_0$	15.074	-13.105	0.189	-0.009	265.208	5.429	0.915
W-Eth ε" / ε <sub>0</sub>	1.019	1.890	0.835	0.101	0.412	0.214	0.841
W-S $\varepsilon'/\varepsilon_0$	1.688	-1.683	0.022	-0.022	0.404	0.201	0.821
W-S ε" / ε <sub>0</sub>	6.694	-6.695	0.101	-0.101	186.6	5.163	0.906

**Table 2.** Values of the model parameters and the statistical indicators regarding the regression carried out with the King and Queen model; the superscript *k* indicates which part of the permittivity (real or imaginary) the parameter represents while the subscript *i* or *j* specify the pure component considered.

## 4. Discussion

The comparison of the obtained data with the literature data confirmed that the experimental device, designed and developed to measure the impedance of liquid substances and mixtures, and the method of deriving the material permittivity, are suitable to the scope. The models here tested (Acree and King and Queen), even if coming from near, but not the same, experimental applications, were revealed to well fit the experimental data, even with binary chemical systems with very different nature from the dielectric point of view (low conductivity for the water–ethanol mixtures, electrolyte solutions with high conductivity in the case of the water–NaCl systems). As far as we know, these models have been applied for the first time to the loss factor, revealing the possibility of using the same kind of models as for the dielectric constant, even if with different potential to be generalized, probably higher for the King and Queen model.

The Acree model resulted in less accuracy, especially in the case of  $\varepsilon''$  of the water–salt mixtures and, in the other cases, it showed a fluctuating behavior, unlike the King and Queen model, probably because it was set to follow the permittivity of the pure substances as references. The King and Queen model was revealed to be more versatile, offering a better description in the cases of a non-linear trend of the data.

As a goal of future work, it would be interesting to extend this approach to other mixtures and to develop proper modeling to describe possible similitudes and/or differences between similar or different substances. Deeper knowledge about the dielectric behavior of complex systems would be very helpful to make heating and reaction processes more and more selective and efficient, thus contributing to the minimization of their energy consumption and environmental impact.

## 5. Conclusions

As widely shown in the scientific literature, the use of microwaves is a valid alternative to conventional heating in many industrial processes and technological applications, due to the high efficiency and specificity concerning the heating target. In many chemical and biochemical applications, microwaves show positive effects on reaction time and selectivity. These effects are largely described in many works, but less interest is focused on the physical and chemical mechanisms of interactions between microwave electromagnetic energy and matter. On the other hand, this missing knowledge would be important for the optimization and energy-saving purposes of the microwave heating process in different cases and applications. The method and measure of microwave heating (i.e., transferred energy) strongly depend on the dielectric properties of substances and mixtures, which commonly show a non-ideal behavior concerning the pure substances, but the literature is lacking in wide and detailed databases of their dielectric properties, particularly of the loss factor (which is the main factor responsible for the heating mechanism), and extremely poor of mixtures data and models.

The present work tackles this problem and missing data by proposing a specially designed measuring system that can be used in many different cases of liquid mixtures, and presenting data,

of both the real and the imaginary part of permittivity, for two mixtures that are representative of industrially relevant chemical systems (alcohol and salt in water solution), as a function of the binary composition. After this, efforts were devoted to model the experimental data to generalize the results. Two literature models were tested with the experimental data: the Acree model and the King and Queen model. These models were applied, in the literature, to other properties, and in some cases to the real part of permittivity (the dielectric constant). Both of them were revealed to be acceptably suitable to describe the permittivity (both the real and the imaginary part) of the considered mixtures, whose components are very different from the dielectric point of view. The King and Queen model was shown to be overall more accurate. The results highlight the need for wider and deeper studies on the dielectric properties of materials, and particularly of mixtures of substances. The topic is still unconsolidated, and a complete assessment of the model accuracy in describing the permittivity of mixtures will be possible only when much more data will be available in the literature.

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