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## Optimal Scheduling of a Battery Energy Storage System with Electric Vehicles' Auxiliary for a Distribution Network with Renewable Energy Integration

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**Abstract:** With global conventional energy depletion, as well as environmental pollution, utilizing renewable energy for power supply is the only way for human beings to survive. Currently, distributed generation incorporated into a distribution network has become the new trend, with the advantages of controllability, flexibility and tremendous potential. However, the fluctuation of distributed energy resources (DERs) is still the main concern for accurate deployment. Thus, a battery energy storage system (BESS) has to be involved to mitigate the bad effects of DERs' integration. In this paper, optimal scheduling strategies for BESS operation have been proposed, to assist with consuming the renewable energy, reduce the active power loss, alleviate the voltage fluctuation and minimize the electricity cost. Besides, the electric vehicles (EVs) considered as the auxiliary technique are also introduced to attenuate the DERs' influence. Moreover, both day-ahead and real-time operation scheduling strategies were presented under the consideration with the constraints of BESS and the EVs' operation, and the optimization was tackled by a fuzzy mathematical method and an improved particle swarm optimization (IPSO) algorithm. Furthermore, the test system for the proposed strategies is a real distribution network with renewable energy integration.

After simulation, the proposed scheduling strategies have been verified to be extremely effective for the enhancement of the distribution network characteristics.

**Keywords:** battery energy storage system (BESS); electric vehicles (EVs); optimal scheduling

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## 1. Introduction

Renewable energy generation, such as photovoltaic (PV), wind, biomass, *etc.*, integrated into distribution power systems, expected to be one of the main solutions for clean power supply, will be considerably developed throughout the world during the next couple of decades. Currently, many countries have implemented or are in the process of implementing policies to promote renewable energy in the distribution network. This is because distributed energy resources (DERs) in the distribution power system could provide a better balance between the increasing electricity demand and traditional power exportation, reduce the power losses occurring in the feeders during energy transmission, as well as enhance the controllability of energy deployment, which would be the main component of the next generation distribution network framework, namely the active distribution network, with intelligent monitoring techniques and advanced management measures [1,2].

However, the fluctuation of DERs is still the main concern for large-scale implementation in low or medium voltage networks. Thus, the energy storage system (ESS) has to be involved to mitigate the bad effects of the DERs' integration. Compared to other types of ESS, a battery energy storage system (BESS) is relatively the most stable, easy to access and control, as an extremely effective way to cooperate with DERs. [3] Therefore, the operation strategies for BESS have become a research hotspot from different perspectives.

Actually, many researchers have proposed some optimal strategies to solve the BESS operation problems, as well as for EVs. In [4], an EV scheduling scheme has been proposed with an uncertain real-time price, taking the battery degradation into account. For another, a real-time scheduling strategy for EVs was presented in [5] to increase the voltage margin and tent to minimize the line loss. The two works above were inclined to solve the EV scheduling problem with different visions, the originality of which could also be applied in BESS scheduling. In [6], a mathematical model for a BESS scheduling procedure was proposed to simulate the charging/discharging process, with the objective of minimizing the line losses; however, only the aspect of the power losses was taken into account. Besides, BESS used for ramp rate control, frequency droop response, power factor correction, solar time-shifting and output leveling have been mentioned in [7], focusing on BESS operation to enable solar energy, which tends to solve BESS scheduling in a transient process. Furthermore, BESS was implemented to deal with power quality disturbances and to compensate reactive power in [8], as well as the optimal power flow in [9]. It is noted that the distribution network operation usually deals with power scheduling problems in the steady-state horizon, so in this paper, the BESS scheduling strategies, following the distribution network operation rules in China, are put forward with intervals of 15 min, which is also apparently a compromise decision between precision and computation quantity. Besides, Most of the strategies proposed from the works above were implemented one day ahead, considerably depending on the accuracy of prediction for renewable energy and power demand. Additionally, the errors from forecasting usually do not

account for the evaluation of model validity, which may affect the applicability of the model when launching in practice. Therefore, a real-time strategy is the most effective approach for power scheduling.

In this paper, optimal scheduling strategies for BESS operation in both the day-ahead and real-time scale have been proposed, to minimize the renewable energy curtailment, to reduce active power loss, to mitigate the voltage fluctuation, as well as to lower the electricity cost. In addition, the EVs considered as the auxiliary technique are also introduced to attenuate the DERs' influence. Besides, all of the scheduling produced by the proposed strategies has considered the constraints of BESS and EVs' operation, as well as the power flow. Furthermore, the proposed scheduling strategies were simulated in a real distribution network with renewable energy integration, part of Beijing Jiaotong University power network, obtaining promising results and verifying the effectiveness of the proposed strategies.

The remainder of this paper is organized as follows: Section 2 describes the relationships between load variance and power loss, as well as between power deviation and voltage deviation. Additionally, some simplifications have been utilized. Section 3 formulates the multi-objective optimization model. Section 4 presents the procedure of the day-ahead and real-time strategy to solve the optimization problem, as well as the solution of the multi-objective optimization model. Section 5 introduces our numerical studies and analyzes the results, followed by conclusions in Section 6.

## 2. Problem Derivation

In [10], it has been noted that minimizing distribution system losses could be equally considered as maximizing the load factor and minimizing load variance if the feeder is a single line from the substation with all loads at the end of the line. Actually, this conclusion could be generalized in a radial distribution system under some assumptions as follows:

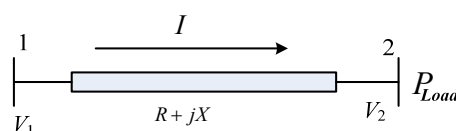
Assuming that the mean value of each load in the radial distribution power system could keep constant during normal operation.

The voltage fluctuation of the initial nodes is supposed to be neglected, in consideration of these nodes usually being connected to the substation.

Besides, the reactive power in the distribution network could be ignored since the power factor correction facilities take effect.

### 2.1. Relationship between Load Shaving and Power Loss

The model utilized in this derivation is shown in Figure 1. The active power loss for this single branch could be formulated as Equation (1).



**Figure 1.** Diagram of a single branch.

$$P_{loss} = \sum_t^T I_t^2 R = \sum_t^T \left(\frac{P_t}{U_{rate}}\right)^2 R = \frac{\overline{P^2} R}{U_{rate}^2} \quad (1)$$

where  $P_{loss}$  is the active power loss of the single branch;  $I_t$  shows the current value running in the corresponding branch at time  $t$ ;  $P_t$  represents the active power of Node 2 at time  $t$ ;  $U_{rate}$  means the rated voltage in the assigned level; and  $R$  is the equivalent resistance value [10].

The load variance could be shown as,

$$\sigma_P^2 = \frac{1}{T} \cdot \sum_t^T (P_t - \bar{P})^2 \quad (2)$$

where  $\sigma_P^2$  is the load variance and  $\bar{P}$  is the mean value of the load;  $T$  represents the time duration, which is 24 h in this paper.

The conclusion could be derived in Equations (3) and (4),

$$\sigma_P^2 = \frac{1}{T} \cdot \sum_t^T (P_t)^2 - 2\bar{P} \frac{1}{T} \sum_t^T P_t + \frac{1}{T} \cdot \sum_t^T (\bar{P})^2 \quad (3)$$

$$\overline{P^2} = (\bar{P})^2 + \sigma_P^2 \quad (4)$$

Equation (4) could be plugged into Equation (1); in this way, the relation between  $P_{loss}$  and  $\sigma_P^2$  is expressed in Equation (5),

$$P_{loss} = \frac{R}{U_{rate}^2} \cdot (\bar{P})^2 + \frac{R}{U_{rate}^2} \cdot \sigma_P^2 \quad (5)$$

In Equation (5), the active power loss is linear to the load variance in the single branch, if the deviation of the rated voltage could be neglected.

## 2.2. Relationship between Load Smoothing and Voltage Deviation

The voltage deviation in Figure 1 could be shown as Equation (6), and the relationship between real power and voltage magnitude could be easily derived based on Kirchhoff's theory in Equation (7). Then, the combination of Equations (6) and (7) contributed to Equation (8), the relationship between power deviation and voltage deviation.

$$V_{dev} = \sum_{t=0}^T \Delta V_2^2 = \sum_{t=0}^T (V_{2,t+\Delta t} - V_{2,t})^2 \quad (6)$$

$$P_{2,t} = \frac{V_{2,t}(V_{1,t} - V_{2,t})}{R} = \frac{-V_{2,t}^2 + V_{1,t}V_{2,t}}{R} \quad (7)$$

$$P_{dev} = V_{dev} \sum_{t=0}^T \left(\frac{V_{2,t+\Delta t} + V_{2,t} - V_{1,t}}{R}\right)^2 \quad (8)$$

In the equations above,  $V_{1,t}$  and  $V_{2,t}$  represent the voltage magnitude of Nodes 1 and 2 at time  $t$ , respectively. Additionally,  $P_{2,t}$  is the real power of Node 2 at time  $t$ . When the subscript shows  $t + \Delta t$  instead of  $t$ , it denotes the assigned quantity at time  $t + \Delta t$ .

In Equation (7), assuming constant  $V_{1,t}$ , with the consideration that Node 1 is close to the substation, it presents an inverted-U quadratic function relationship between  $P_{2,t}$  and  $V_{2,t}$ . Clearly,  $V_{2,t}$  is definitely more than  $1/2 V_{1,t}$  under normal circumstances, which means it would follow the right-half rules of quadratic function;  $P_{2,t}$  would be decreasing synchronously with the increasing of  $V_{2,t}$ . Anyway, the variation absolute values show the same trend. Furthermore, in Equation (8),  $(V_{2,t+\Delta t} + V_{2,t} - V_1)^2$  is apparently positive with the quadratic term; this also suggests the positive correlation relationship between  $P_{2,t}$  and  $V_{2,t}$ .

Through the derivation procedure above, the strong positive correlation between load variance and power losses is shown; likewise, the strong positive correlation between power deviation and voltage deviation. For the traditional optimization process with a distribution network, the power flow calculation must be involved with a slow computation speed and weak convergence degree. Hence, the tedious iterative work could be avoided, when load variance and power deviation minimizing, to simplify, are utilized for power losses and voltage deviation minimizing, respectively.

### 3. Model Formulation

In a distribution network with DER integration, BESS and EV are introduced for minimizing the bad side effect from DERs' access. An optimization framework has been proposed for reducing renewable energy curtailment, cutting feeder losses, mitigating voltage fluctuation and lowering electricity expense, considering the constraints of BESS and EV operation. The charging and discharging power of BESS and the charging period of EV are recognized to be control variables, and the optimization would be realized under minimizing one or more objective functions while satisfying the several equality and inequality constraints. Its mathematical model can be established as,

$$\begin{aligned} \text{Min } & f(x) \\ \text{s.t. } & g(x) = 0, \quad h(x) \leq 0 \end{aligned} \quad (9)$$

where  $f$  is the objective function to be optimized;  $g$  and  $h$  are the equality and inequality constraints, respectively;  $x$  is the vector of charging or discharging power or the period selection variable. The detailed description of the objective functions, equality and inequality constraints are stated as follows.

#### 3.1. Minimizing Renewable Energy Curtailment

It is widely accepted that, in power system operation, the power generated is always equal to the power demand in any moment. Assuming that there is no energy storage facility in the regional distribution network, the extra DERs' power has to be injected back to the substation or curtailed, resulting in extra power losses and unfortunate waste of renewable energy, when the DERs' generated power is in excess of the power demand. Therefore, the BESS is integrated into the regional distribution network with renewable energy integration for minimizing DER curtailment [11], as Equation (10) shows,

$$\text{Min } \sum_{t=0}^T P_{\text{DER-curtail}} \quad (10)$$

where  $P_{\text{DER-curtail}}$  is the DER power curtailment.

### 3.2. Minimizing Feeder Losses

Minimizing feeder losses is a crucial indicator for power system economic operation and also a key means for energy conservation [6]. In this paper, reducing feeder losses is also proposed for BESS scheduling and EV coordinated charging. In terms of the theoretical derivation in Section 2, the load variance minimization could be used to substitute feeder loss minimization.

$$\text{Min } P_{\text{loss}} \propto \text{Min } \sigma_p^2 = \frac{\sum_{t=0}^T (P_{\text{load},t} - P_{\text{average}})^2}{T} \quad (11)$$

where  $P_{\text{load},t}$  is the load power at time  $t$ , and  $P_{\text{average}}$  means the average power for the assigned duration.

### 3.3. Minimizing Voltage Deviation

With DERs integrated into the distribution network, their intermittent and fluctuation characteristics have aggravated the power and voltage volatility in the distribution power system, serving as the immediate cause of power quality reduction and electric equipment damage. Thus, the objective function of minimizing voltage deviation is proposed to mitigate the fluctuation brought by the DERs' integration, similarly to the last optimization target, which is formulated by the power deviation in Equation (12).

$$\text{Min } V_{\text{dev}} \propto \text{Min } P_{\text{dev}} = \sum_{t=0}^T (P_{\text{load},t+1} - P_{\text{load},t})^2 \quad (12)$$

### 3.4. Minimizing Electricity Cost

Besides the power demand of the regular load, the charging cost of BESS and EV also contribute to electricity bills. On the contrary, the discharging power of BESS and the injected power of DERs facilitate reducing the utility expense. As a consequence, through the optimal scheduling of BESS associated with EV coordinated charging, the electricity cost could be reduced as Equation (13) shows,

$$\text{Min } C_{\text{bill}} = \sum_{t=0}^T c_t \cdot P_t \quad (13)$$

where  $C_{\text{bill}}$  is the overall electricity cost in the distribution network with duration  $T$ , and  $c_t$  means the time of use (TOU) electricity price at time  $t$ .

### 3.5. Constraints of BESS Operation

For the optimal scheduling strategy of BESS, the constraints of BESS are presented as the charging/discharging power limitation, the energy capacity restriction and the charging/discharging balance requirement.

The constraint of charging/discharging power of BESS refers to the upper/lower power limitation during the BESS charging/discharging process; this means that the charging/discharging process should be within the allowance boundaries, as Equation (14) shows,

$$-P_{\text{max}} \leq P_{\text{storage},t} \leq P_{\text{max}} \quad (14)$$

where  $P_{storage,t}$  represents the charging/discharging power of BESS at time  $t$ , and  $-P_{max}$  and  $P_{max}$  signify the upper and lower boundaries of BESS power, respectively.

The constraint of the energy capacity of BESS stands for the upper/lower energy limitation during BESS operation, to guarantee the capability for emergency incidents. In this work, the energy boundaries of BESS are from 10% to 90% of the energy capacity.

$$E_{storage,t} \leq 90\% \cdot E_{storage,max} \quad (15)$$

$$E_{storage,t} = E_{storage,0} + \int_0^t P_{storage,k} dk \quad (16)$$

In Equations (15) and (16),  $E_{storage,t}$  and  $E_{storage,max}$  are the state of energy at time  $t$  and the designed energy capacity for BESS, respectively. Moreover,  $E_{storage,0}$  indicates the initial energy state of BESS.

The constraint of the charging/discharging balance of BESS means that the charging energy is supposed to be equal to the discharging energy during a certain period.

$$\left| \int_{t_a}^{t_b} P_{ch} dt - \int_{t_c}^{t_d} P_{dis} dt \right| \leq \varepsilon \quad (17)$$

In Equation (17),  $t_a$ ,  $t_b$  denote the charging region and, similarly,  $t_c$ ,  $t_d$  the discharging region. Besides,  $P_{ch}$ ,  $P_{dis}$  represent the charging and discharging power, respectively. Additionally,  $\varepsilon$  stands for the permissible error of the charging/discharging balance.

It is to note that, since the BESS optimal scheduling strategy would be used in the duration of 24 h, the degradation of batteries is not considered in this paper. For long time operation, the boundaries of power and energy limitation should be reset for specified condition.

### 3.6. Constraints of EVs' Operation

As an auxiliary technique, the coordinated charging strategy of EVs has been used to assist the BESS scheduling, and the constraints of EVs are presented as the constraints of the charging period and the charging pattern.

The constraint of the EV charging period refers to that the charging period selection, which should meet the transport demands of EV users. In this paper, this means the start charging moment should be restricted as Equation (18) shows,

$$T_{arrive,i} \leq T_{start,i} \leq T_{leave,i} - T_{c,i} \quad (18)$$

$$T_{c,i} = (1 - SOC_{arrive,i}) \cdot T_{full} \quad (19)$$

In Equations (18) and (19),  $T_{arrive,i}$ ,  $T_{start,i}$  and  $T_{leave,i}$  are the arriving, start charging and leaving moment for  $EV_i$ , and  $T_{c,i}$  represents the charging duration for  $EV_i$ . Furthermore, the expression of  $T_{c,i}$  in Equation (19) has been given, where  $SOC_{arrive,i}$  means the state of charge (SOC) condition of  $EV_i$  when arriving at the charging spot, and  $T_{full}$  stands for the full charging duration for the assigned EV model.

The constraint of the charging pattern means the constant-current constant-voltage (CC-CV) mode for individual EV charging [12–14].

### 3.7. Other Constraints

In this paper, the constraints of the balance between power demand and supply and the voltage upper/lower limits are also considered in the optimization procedure.

Besides, the reverse-flow control is also introduced as Equation (20) illustrates, to eliminate the unnecessary power losses.

$$P_{load,t} \geq P_{DG,t} + P_{storage,t} \quad (20)$$

where  $P_{DG,t}$  means the sum of the DERs' generation at time  $t$ .

## 4. Solution Technique

To tackle the optimization model proposed in Section 3, day-ahead and real-time scheduling strategies have been presented, respectively. The day-ahead strategy tends to settle the optimization problem one day ahead, which means obtaining the next day BESS operation profile globally and precisely. Alternatively, the real-time scheduling strategy is to solve it with interval updating, to avoid the related effect of regular load and DER forecasting errors.

Both of the strategies are suitable for BESS scheduling and EVs' coordinated charging.

In terms of the positive performance of the optimization solution in [15], both of the multi-objective optimization problems derived from the two strategies above could be tackled by fuzzification multi-objective optimization and an improved particle swarm optimization (IPSO) algorithm. More specifically, the detailed description is illustrated as follows.

### 4.1. Day-Ahead Strategy

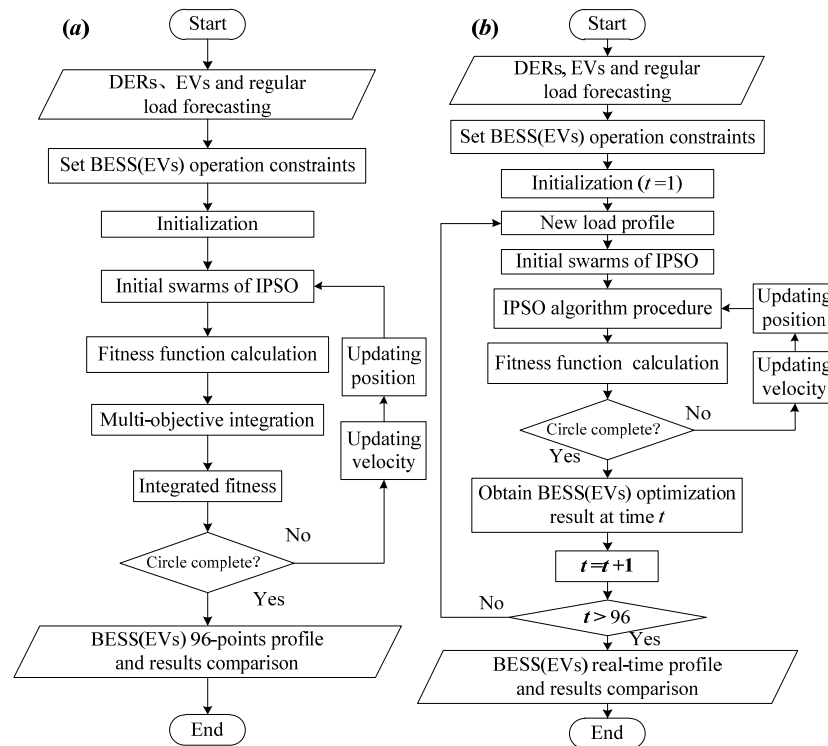
For the day-ahead strategy, DERs, EVs and regular load forecasting should be predicted before this procedure. The BESS scheduling profile of the next day with certain precise time, 15 min in this work, could be optimized, incorporated with minimizing the DERs' curtailment, load variance, load deviation and electricity cost, to be the objective. The detailed procedure flow is demonstrated below and in Figure 2a.

Step 1: According to the forecasting results of the regular load, DERs and EVs, the corresponding 96-point profiles could be set for subsequent optimizing with a 15-min interval.

Step 2: In the day-ahead strategy, the variables for BESS optimizing were  $P_{storage} = [P_1, P_2, \dots, P_{96}]$ , and the variables for EVs' coordinated charging were  $T_{start} = [T_1, T_2, \dots, T_{96}]$ . For better performance, the initial BESS variables would be set as a zero vector, and the initial EVs' variables would be set as the forecasting vector.

Step 3: The multi-optimization procedure and intelligent algorithm were implemented as in Sections 4.3 and 4.4.





**Figure 2.** (a) Day-ahead strategy flow chart; (b) real-time strategy flow chart.

#### 4.2. Real-Time Strategy

In this section, a real-time strategy was proposed to solve the optimization problem, as well as to handle the dependency for forecasting errors. Both the forecasting data and real time capture data have been combined for optimizing globally and meeting the requirements of BESS or EVs' operation.

The real-time optimizing framework is illustrated in Figure 3. In every 15 min, the optimization procedure was performed once to get the optimal operation value for the current point. Additionally, the real-time data have been used for the duration from the beginning to the current point, as the orange lines show in Figure 3, and the forecasting data have been used for the duration from the current point to the end of the day, as the blue lines show in Figure 3. Besides being comparable to the day-ahead strategy, another reason to have optimization in a one-day scale is to ensure the charging and discharging balance for BESS operation. Then, the detailed procedure is shown below and in Figure 2b.

Step 1: According to the forecasting results of the regular load, DERs and EVs, the corresponding 96-point profiles could be prepared for subsequent optimizing with a 15-min interval.

Step 2: The initialization: At time  $t = 1$  ( $t = 1, 2, \dots, 96$ ), the real-time data of the DERs, EVs and regular load at current time  $t = 1$  replaced the forecasting data at time  $t = 1$ , and the new load profile would be used for optimization. Afterwards, the BESS or EVs' 96-point operation results could be obtained. Only the optimal value at time  $t = 1$  was picked to be the operation value for time  $t = 1$ .

Step 3: Go to the next moment  $t = t + 1$ ;

Step 4: To make the load profile at time  $t$ , the real-time data from the beginning to time  $t$  have been used to replace the corresponding period of forecasting data. At the same time, the variables for BESS are  $P_{storage} = [P_t, P_{t+1}, \dots, P_{96}]$ ,  $96-t + 1$  variables in all, and similarly, the variables for EVs are  $T_{start} = [T_t, T_{t+1}, \dots, T_{96}]$ .

Step 5:  $P_t$  and  $T_t$  to obtain the optimal results for the current time  $t$  through the following optimization techniques.

Step 6: Go back to Step 3, until completing the circle of 96 points.

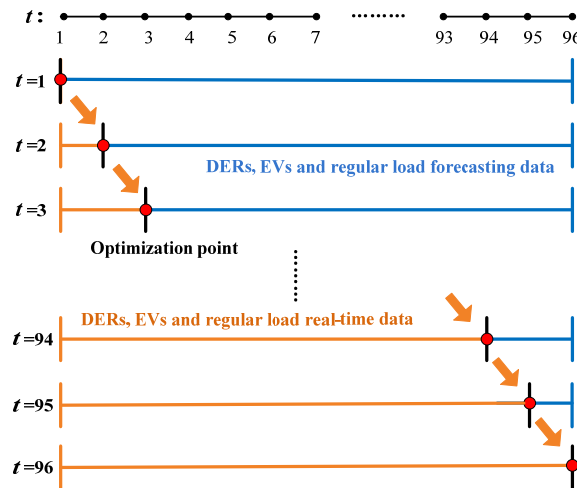


Figure 3. Framework of real-time optimizing.

### 4.3. Fuzzy Multi-Objective Optimization

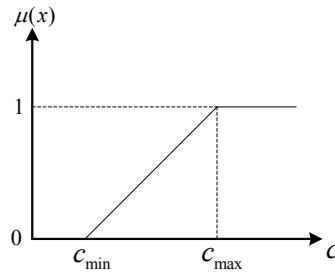
In this paper, the optimization problem is actually a multi-objective optimization problem. The fuzzy mathematics method, with the membership function, has been utilized to perform the objective function fuzzification to transfer the multi-objective optimization to a single-objective issue [15,16].

For objectively considering the weight of each optimization objective, the linear membership function is used, which can be described as:

$$\mu_x(x) = \begin{cases} 0 & f_i(x) \leq c_{i \min} \\ \frac{f_i(x) - c_{i \min}}{c_{i \max} - c_{i \min}} & c_{i \min} < f_i(x) < c_{i \max} \\ 1 & f_i(x) \geq c_{i \max} \end{cases} \quad (21)$$

$i = 1, 2, 3, 4$

where  $f_i(x)$  is the  $i$ -th objective function of the fuzzy multi-objective problem;  $\mu_i(x)$  is the membership function of  $f_i(x)$ ;  $m$  is the number of objective functions;  $c_{i \min}$ ,  $c_{i \max}$  are the upper and lower limit values of  $f_i(x)$ , respectively;  $c_{i \min}$  is the optimal value obtained by the single-objective function; and  $c_{i \max}$  is initial value of each objective function. Besides, the curves of the membership function by Equation (21) are shown in Figure 4.



**Figure 4.** Membership function of the sub-objective.

After the fuzzification, the sub-objectives also need to be integrated. In this work, minimizing the maximum of sub-objectives has been applied as shown in Equation (22),

$$fitness = \max(\mu_1, \mu_2, \mu_3, \mu_4) \tag{22}$$

where *fitness* means the integrated fitness for multi-objective optimization.

#### 4.4. IPSO Algorithm

The optimization model proposed above is considered as a complex multi-constraint, nonlinear optimization problem. Compared to classical algorithms, such as linear programming, quadratic programming, the gradient descending method and other numerical algorithms, the heuristic algorithms are novel algorithms for solving the optimization problem and much easier to implement and extend, such as the genetic algorithms (GA), particle swarm optimization (PSO), differential evolution (DE), artificial immune algorithm and artificial bee colony (ABC) algorithm.

The PSO algorithm possesses superior performance in its implementation and a good trade-off between exploration and exploitation ability, with a simple structure, a simple parameter setting and a fast convergence speed. It has been widely applied in function optimization, mathematical modelling, system control and some other areas [17–19].

In basic PSO algorithms,  $\omega$ ,  $c_1$  and  $c_2$  are fixed values. For the search accuracy and search speed, in this paper, the improved inertia weight is shown in Equation (25). The algorithm may adjust  $\omega$  dynamically via Equation (25), so that it can optimize dynamically by taking both global search and local search into account during changing The improved PSO is shown as follows:

$$v_{id}^{k+1} = \omega(k)v_{id}^k + c_1r_1(p_{id} - z_{id}^k) + c_2r_2(p_{gd} - z_{id}^k) \tag{23}$$

$$z_{id}^{k+1} = z_{id}^k + v_{id}^{k+1} \tag{24}$$

$$\omega(k) = \omega_{start} - (\omega_{start} - \omega_{end})\left(\frac{k}{K}\right)^2 \tag{25}$$

where  $\omega_{start}$  and  $\omega_{end}$  represent the initial value and the final value of  $\omega$ , respectively;  $K$  is the maximum number of evolutionary generations;  $k$  is the current number of evolutionary generations.

### 5. Case Study

#### 5.1. The Case Setting

For the project requirement, all of the simulation cases in this paper are carried out based on the framework of the campus distribution network and corresponding regular loads, as Figure 5a shows. Furthermore, PV, EVs and BESS are integrated into the network in some cases, of which there are a 300-kWp PV, 100 EVs and a 150-kWh BESS. The details of the case setting are described in Table 1. Additionally, the profiles of regular load forecasting, EV load estimation, PV forecasting and the total load prediction of this framework are shown in Figure 5b.

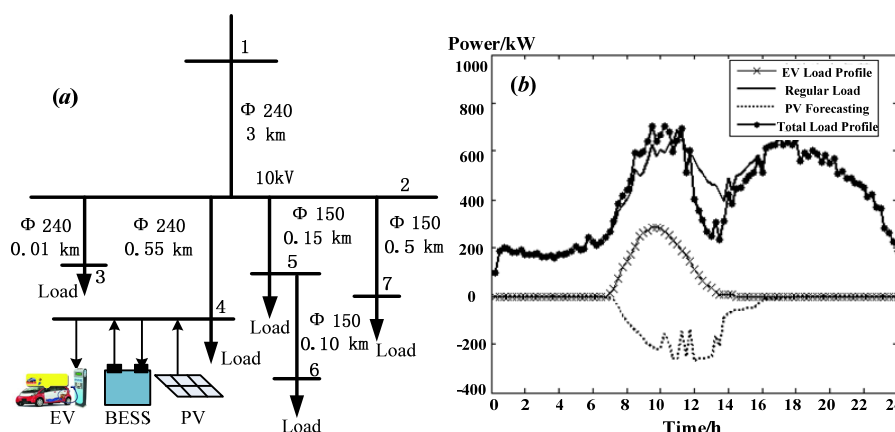


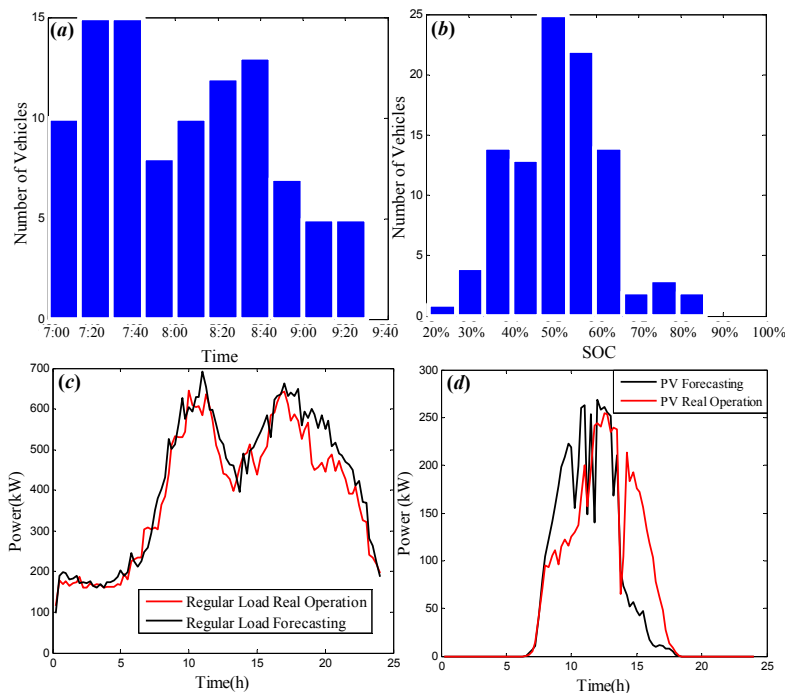
Figure 5. (a) The simulation case setting; (b) The simulation case data.

Table 1. The simulation cases’ settings.

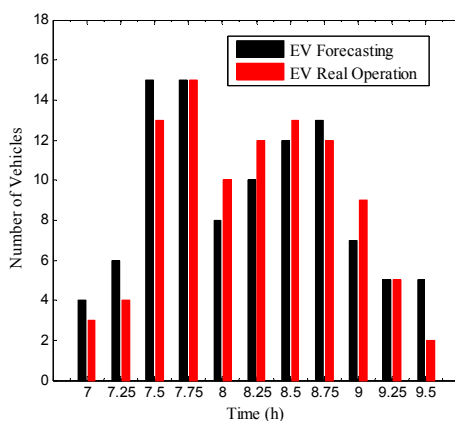
Category	Settings	Optimization scheme
Case 1	Loads	No optimization
Case 2	Loads, PV and uncoordinated charging EVs	No optimization
Case 3	Loads, PV, BESS and uncoordinated charging EVs	Day-ahead optimization
Case 4	Loads, PV, BESS and uncoordinated charging EVs	Real-time optimization
Case 5	Loads, PV, BESS and coordinated charging EVs	Day-ahead optimization
Case 6	Loads, PV, BESS and coordinated charging EVs	Real-time optimization

During the IPSO optimizing,  $c_1, c_2 = 1.49$ ,  $\omega_{start} = 0.9$ ,  $\omega_{end} = 0.4$ , and the velocity step is 1 kW for BESS optimizing and 15 min for the EVs’ coordinated charging.

Besides, the charging/discharging power limitation of BESS is 50 kW; the initial energy state is 75 kWh. Additionally, the arriving time distribution and the arriving SOC distribution of EVs are demonstrated in Figure 6a,b, respectively. Furthermore, the difference between real-time operation data and the forecasting data for the regular load, PV and arriving time of EVs are also given in Figure 6c,d and Figure 7.



**Figure 6.** (a) EVs’ arriving time distribution; (b) EVs’ arriving SOC distribution; (c) real and forecasting data of the regular load; (d) real and forecasting data of PV.



**Figure 7.** Forecasting and real data of the EVs’ arriving time.

In the simulation, there are six cases in all. The simulation case settings and the optimal schemes used are shown in Table 1.

## 5.2. The Optimizing Results

### 5.2.1. BESS Optimizing without EVs’ Auxiliary

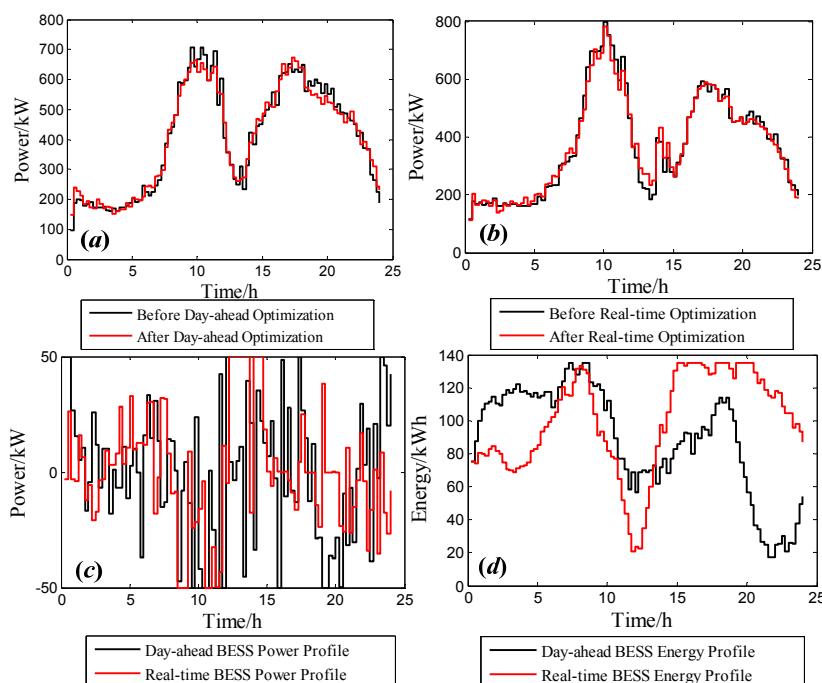
Based on the optimization model and the strategy above, first of all, the BESS day-ahead and real-time optimization without EVs’ auxiliary has been performed. The calculation results are shown in Table 2. It can be noticed that, in this work, due to the original case configuration, Objective 1, minimizing the DERs’ curtailment, is zero in all cases.

**Table 2.** Index comparison of BESS optimizing.

	Case 1	Case 2	Case 3	Case4
Objective 1	0.00	0.00	0.00	0.00
Objective 2	30,484	32,478	28,830	27,830
Objective 3	120,300	233,010	112,500	178,290
Objective 4	13,613	12,927	12,767	11,707
$P_{\text{loss}}$ (MW)	0.8661	0.8551	0.8526	0.8206
$V_{\text{dev}}$ ( $10^{-5}$ kV <sup>2</sup> )	6.18	11.2	5.59	8.49

In Table 2, it is clear that Objective 2 and 3's values in Case 2 are higher than that in Case 1, which means that the integration of PV and EVs brings about the load variance increase, with the power deviation increasing. Besides, both the day-ahead strategy and real-time strategy are effective for all of the objectives, except for zero DER curtailment, which already achieved the minimum. Comparing between the day-ahead and real-time strategy for BESS optimization without EVs' auxiliary, these two strategies displayed different advantages; the real-time strategy shows better performance in load variance, feeder losses and utility cost control, and the day-ahead strategy shows better effectiveness in the power deviation and voltage deviation control.

The load profiles of before and after BESS day-ahead and real-time optimizing are displayed in Figure 8a,b, respectively. Additionally, the BESS operation power profiles and energy profile for day-ahead and real-time are shown in Figure 8c,d, respectively. It expresses the distinct optimization tracks of day-ahead and real-time optimization.



**Figure 8.** (a) Load profiles of before and after BESS day-ahead optimizing (without EVs); (b) load profiles of before and after BESS real-time optimizing (without EVs); (c) BESS operation power profiles of day-ahead and real-time (without EVs); (d) BESS operation energy profiles of day-ahead and real-time (without EVs).

### 5.2.2. BESS Optimizing with EVs' Auxiliary

Then, the BESS with EVs' auxiliary day-ahead and real-time optimization has been implemented. The calculation results are shown in Table 3.

**Table 3.** Index comparison of BESS and EV optimizing.

	Case 1	Case 2	Case 5	Case6
Objective 1	0.00	0.00	0.00	0.00
Objective 2	30,484	32,478	29,696	17,465
Objective 3	120,300	233,010	141,050	165,490
Objective 4	13,613	12,927	12,805	10,152
$P_{\text{loss}}$ (MW)	0.8661	0.8551	0.8522	0.8156
$V_{\text{dev}}$ ( $10^{-5}$ kV <sup>2</sup> )	6.18	11.2	3.36	7.52

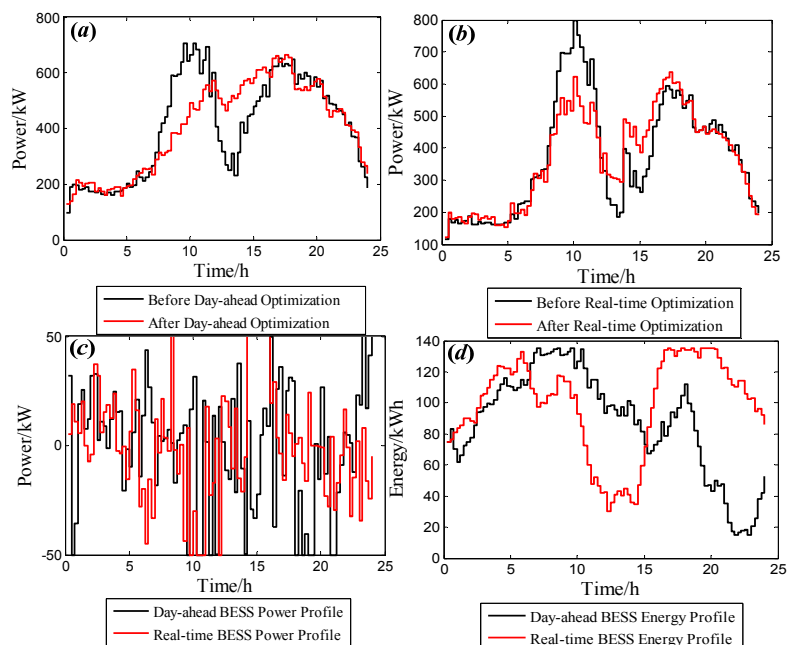
In Table 3, it is obvious that both the day-ahead strategy and real-time strategy for BESS and EV combined optimization are effective for all of the objectives, regardless of Objective 1. Compared between the day-ahead and real-time strategy for combined optimization, these two strategies also show distinct superiority, the same as BESS optimization without EVs' auxiliary; the real-time strategy shows better performance in load variance, feeder losses and utility cost control, and the day-ahead strategy shows better effectiveness in power deviation and voltage deviation control.

The load profiles of before and after combined day-ahead and real-time optimizing are displayed in Figure 9a,b, respectively. Additionally, the BESS operation power profiles and energy profile for day-ahead and real-time are shown in Figure 9c,d, respectively. It expresses the distinct optimization tracks of day-ahead and real-time optimization. Besides, in Figure 10, the EVs' profiles of forecasting, day-ahead and real-time optimization are presented.

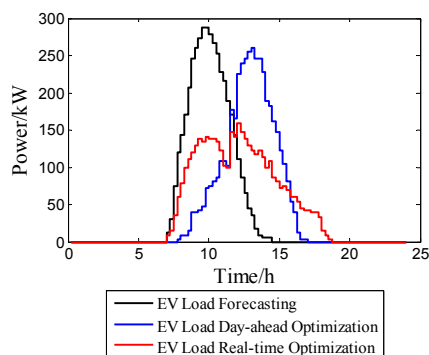
In the BESS without and with EVs' auxiliary optimization above, the results illustrated that both of the optimizing scheduling strategies took effect for individual objective and integrated fitness. Moreover, it is also clear that, under the same BESS configuration, strategies with EVs' coordinated charging show significant enhancement for all of the optimization targets. From another perspective, the day-ahead and real-time optimization, no matter if for BESS only or the BESS and EV combination, the optimization routes are totally different, resulting in various profiles of power and energy tendency.

In our view, both strategies show significant effectiveness, and the main distinction is to be applied for different requirements. The day-ahead strategy turns out to be used in the scheduling focusing on the global optimization without bidirectional communication, especially the situation with a high accuracy of profile prediction. Additionally, the real-time strategy is suitable to handle the modest accuracy degree of forecasting and to update the scheduling on the basis of two-way communication.

It should be noted that the BESS did not show the load-shaving effect in the cases above; this is because the BESS power and energy constraints would not allow this and which has been formerly set. Moreover, the main objective of BESS is to alleviate the fluctuation of DERs, which has been considerably verified in this work.



**Figure 9.** (a) Load profiles of before and after combined day-ahead optimizing (with EVs); (b) load profiles of before and after combined real-time optimizing (with EVs); (c) BESS operation power profiles of day-ahead and real-time (with EVs); (d) BESS operation energy profiles of day-ahead and real-time (with EVs).



**Figure 10.** EVs' load profiles of forecasting, day-ahead and real-time optimization.

## 6. Conclusions

In this paper, the scheduling framework for BESS operation with EVs' auxiliary in a distribution network with renewable energy integration has been proposed, to reduce the renewable energy curtailment, decrease the power losses, mitigate voltage deviation and lower the electricity expense. Moreover, the model also takes into account the BESS operation constraints and EVs' charging limitation. To tackle the scheduling problem, two optimization processes are presented, the day-ahead strategy and the real-time strategy, to be incorporated into the framework, separately. To handle the multi-objective formulation, a fuzzy mathematical method has been launched to turn multi-objective optimization into a single-objective issue; from another aspect, the IPSO algorithm has been implemented to obtain the optimal scheduling results.



Through the simulation results of six cases, it could be concluded that the proposed BESS scheduling and EVs' coordinated charging scheme are effective for the assigned distribution network, and both the day-ahead and real-time strategy procedures show significant performances. Additionally, from our perspective, the mode of the real-time strategy for BESS scheduling with EVs' auxiliary is recommended for the cases with confined load forecasting accuracy, as well as with EVs' access.

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### Author Contributions

The initial design and implementation of the optimal BESS scheduling framework and the solution were done by Yuqing Yang. She was also responsible for the simulation implementation. In addition, this work was also performed under the advisement of and regular feedback from Weige Zhang, who also revised the manuscript critically. Moreover, Jiuchun Jiang, Mei Huang and Liyong Niu also gave some useful suggestions for this work and helped revise the manuscript.

### Conflicts of Interest

The authors declare no conflict of interest.

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