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The Optimization, Kinetics Model, and Lab-Scale Assessments of Phenol Biodegradation Using Batch and Continuous Culture Systems

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Abstract: Phenol was considered a severe hazard to all ecosystems even at low concentrations. The bioremediation process is an eco-friendly process for complete phenol degradation and bioelectricity generation. In the present study, a consortium of native isolates was used for phenol biodegradation and bioenergy generation using nano-graphite electrodes. The optimization of nutritional and environmental parameters using batch culture revealed that the optimum conditions for maximum phenol degradation and energy generation were inoculum concentration, 1%; incubation period, 48 h; phenol, 6 ppm; MgSO₄, 70 mg/L; K₂HPO₄, 175 mg/L; and CaCl₂, 1 mg/L. Phenol biodegradation reached 93.34% with a power density of 109.419 mW/cm³. A lab-scale bioreactor was used as a continuous culture with aeration rate, agitation speed, and dissolved oxygen of 0.5 v/v/m, 750 rpm, and 30%, respectively. On using the continuous culture, phenol biodegradation and bioenergy production reached 97.8% and 0.382 W/cm³, respectively. A kinetics study using Haldane's kinetics model reported the best fit to achieve a significant correlation coefficient (R²) value (0.9865) reaching maximum specific growth rate with initial phenol concentration of approximately 9 mg L⁻¹ where the specific growth rates (μ, h⁻¹) varied with different initial phenol concentrations. In conclusion, the native isolated consortium could be considered as an economical and sustainable approach to phenol biodegradation in industrial wastewater as well as bioelectricity generation.

Keywords: phenol degradation; bioelectricity generation; industrial effluents; optimization; continuous culture



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1. Introduction

Organic pollutants, especially phenolic compounds, are the most widely abundant pollutants in industrial wastewater. In general, petrochemicals, coke oven plants, coal mining, and petroleum oil refineries are the most important industries releasing phenolic pollutants to the ecological environment [1,2]. Phenolic pollutants were reported as biologically unmanageable. Thus, they remain in the industrial wastewater with accumulated concentrations [3]. Due to their carcinogenic effect and acute toxicity, phenolic pollutants cause serious human health hazards and harm the environment [4]. Biodegradation is the most promising and popular approach to remove toxic and hazardous pollutants, owing to its eco-friendliness, economic viability, and practical feasibility [5]. Consequently, the bioremediation strategy has emerged as a potential method for the complete biodegradation of phenolic pollutants.

On the other hand, the technique known as microbial fuel cells (MFC), which produces energy particularly from the oxidation of organic compounds brought about by the metabolic activity of microorganisms, seems to be appealing for the purpose of warranting energy power production. According to Mohan et al. [6], the use of MFC as a renewable energy source to produce electricity is seen as a dependable, clean, and effective process. This approach employs renewable ways as an alternative tool to the most widely used non-sustainable sources, and it does not result in the production of any hazardous by-products. MFCs have been shown to be an effective technology in recent years for the recuperation and on-site conversion of chemical energy into electrical energy. According to Hemashenpagam and Selvajeyanthi [7], the microbial metabolism of wastes utilizing innovative bioremediation technologies such as MFC for energy generation is recognized as the effective and ecologically benign solution. Hejazi et al. [8] reported that the phenol degradation percentage in a conventional MFC was 75% only by changing the bioreactor to a granular-activated carbon (GAC) adsorption/MFC combined system (GAMFC); the phenol degradation percentage reached 95%. Another study built a two-chamber MFC in order to treat phenol and acetone wastewater and simultaneously produce electricity. They used proton exchange poly-sulfonated (ether ketone) membrane and reported an output voltage range between 240 and 250 mV [9]. On the other hand, Moreno et al. [10] reported achieving maximum power density (777.8 mW m^{-3}) upon using continuous flow MFCs with granular graphite electrodes compared to single-rod electrodes (0.8 mW m^{-3} power density).

Hence, the aim of the present study was to:

- evaluate the phenol degradation and bioelectricity generation using a microbial consortium in batch and continuous systems;
- assess the potential application of nano-electrodes; and
- investigate the kinetic study of the tested consortium.

2. Materials and Methods

2.1. Microorganisms

Microorganisms (15 strains) were previously isolated from static wastewater effluents collected from Alexandria Mineral Oils Co “AMOC” and identified using 16S rDNA sequencing. Six bacterial strains were used in the present study, namely: *Bacillus subtilis* MW585596, *Staphylococcus equorum* MW585694, *Bacillus benzoevorans* MW597321, *Bacillus circulans* MW597408, *Pseudomonas aeruginosa* MW598228, and *Burkholderia cepacia* MW579472 [11].

The McFarland standards were employed as a point of reference for the purpose of calibrating the turbidity of bacterial suspensions derived from cultures that were 16 to 24 h old. This calibration was necessary in order to standardize the bacterial count in either sterile saline or a nutritional broth, resulting in a concentration of 1.5×10^{-6} colony-forming units per milliliter (CFU/mL). Subsequently, equivalent quantities of the six isolates, each with a numerical label, were combined to create a solution with a final concentration of 10.0% (v/v). The isolates were carefully measured to ensure that their optical density at a wavelength of 600 nm (OD_{600 nm}) fell within a range of 1.00 ± 0.40 [12].

2.2. Nano-Graphite Synthesis, Characterization, and Electrode Plating

2.2.1. Nano-Graphite Synthesis

Nano-graphite was synthesized through the utilization of a mixed microemulsion approach. This involved the combination of two distinct microemulsions, one containing a sucrose solution and the other containing sulfuric acid. The sulfuric acid microemulsion component consisted of 20 μL of sulfuric acid and 1 mL of a surfactant solution with a mass ratio of 1:7:8/2 for cetyltrimethylammonium chloride (CTAC), cyclohexane, and pentanol, respectively. The sucrose microemulsion component was made using 20 μL of aqueous sucrose, along with 1 g of the same surfactant solution in an aliquot. The aqueous sucrose microemulsion and sulfuric acid microemulsion were combined in equal proportions. The

product was clear isotropic phase, which was then left for three days in room temperature for nano-graphite synthesis [13].

2.2.2. Nano-Graphite Characterization

The dynamic light scattering (DLS) technique (Malvern Zetasizer, Worcestershire) was the chosen method to assess the particle size (PS), polydispersity index (PDI), and zeta potential of the synthesized nano-graphite. Nano-structured graphite ultra-structure, size, and shape were examined using transmission electron microscopy (TEM, JEOL 2100F FEG-200 kV TEM operating at 80 kV) [14].

2.2.3. Nano-Graphite Electrode Plating

The cathode was prepared by grinding 70% graphite nanoparticles with 10% Super-P(Carbon) and 20% Polyvinylidene fluoride (PVDF) in a high-power ball milling machine at 500 rpm for 24 h in the presence of argon. N-methyl-2-pyrrolidinone (NMP) solvent was used for mixture dispersion with continuous stirring. The slurry was pasted on metal collectors using a minicoater (MC-20, Hohsen) and dried at 80 °C for 2 h [15].

2.3. Phenol Degradation and Bioelectricity Estimation

The phenol concentration was measured spectrophotometrically using the HACH[®] phenol kit [16], while the bioelectricity biogenerated from a microbial fuel cell (MFC) was estimated using the synthesized nano-graphite as cathode and copper as anode. To calculate the power density PD (w/cm^3), 15 pieces of MFC (connected to each other by a salt bridge) with an external resistance was connected in series and 3 sets of these connected cells were connected in parallel (Figure 1). The power density was calculated using the following equation:

$$PD = \frac{V \times I}{U} \quad (1)$$

where V was the cell voltage (V), I was the current (A), and U was the anodic solution volume.

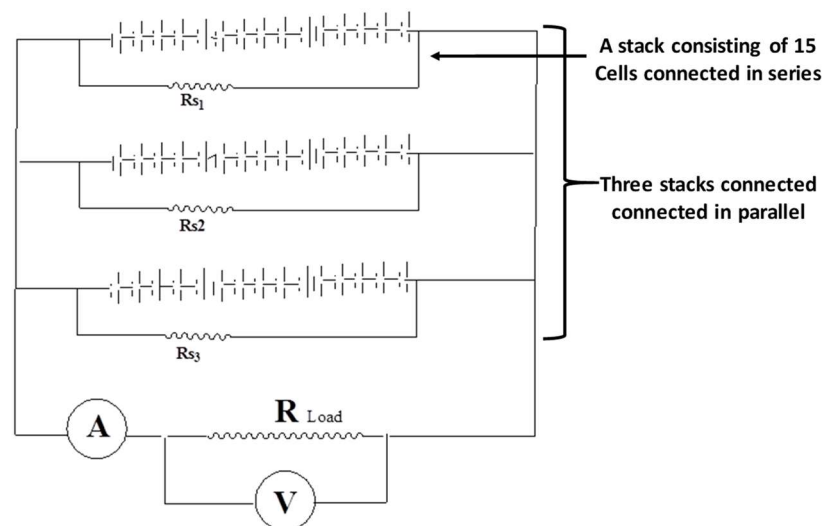


Figure 1. Scaling up the power density using Stacked MFC.

2.4. Optimization of Nutritional and Environmental Factors

The optimization of the key variables influencing phenol biodegradation and bioelectricity production processes was achieved by employing two statistical designs: firstly the Plackett–Burman design (PBD) and subsequently the central composite design (CCD), as applied by Boudraa et al. [17] and Du et al. [18] using Minitab 19[®].

2.4.1. Plackett–Burman Design (PBD)

Twelve factors were investigated by applying the Plackett–Burman design to determine the phenol biodegradation and bioelectricity generation effective factors at a 95% confidence level. Bacterial inoculum concentration, culture volume, phenol concentration, pH, and incubation time, plus KH_2PO_4 , K_2HPO_4 , $(\text{NH}_4)_2\text{SO}_4$, NaCl , $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$, $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$, and $\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$ concentrations, were tested for nutritional and environmental factors. The following first-order polynomial model was used for the mathematical modeling (Equation (2)):

$$Y = \beta_0 + \sum \beta_i X_i \quad (2)$$

The projected response Y represents the percentage of phenol degradation. The model intercept is denoted as β_0 , the linear coefficient as β_i , and the level of the independent variable as X_i . The current study aimed to examine the model fitting and the impact of all parameters through an analysis of variance (ANOVA) using t -tests and p -values. The researchers examined each independent variable across three levels, denoted as -1 , 0 , and $+1$, as shown in Table 1 [19]. Further optimization of both phenol biodegradation and bioelectricity generation responses was conducted by taking into account the essential elements. This was achieved through the use of a central composite design (CCD).

Table 1. Parameters under investigation using a PBD.

No.	Factor	Unit	Levels		
			−1	0	1
1	Bacterial inoculum concentration	%	1.0	3.0	5.0
2	Culture volume	mL	75.0	100.0	125.0
3	Concentration of phenol	ppm	6.0	13.0	20.0
4	pH	-	6.5	7.5	8.5
5	Incubation time	h	48.0	72.0	96.0
6	Concentration of KH_2PO_4	mg/L	120.0	420.0	720.0
7	Concentration of K_2HPO_4	mg/L	175.0	375.0	675.0
8	$(\text{NH}_4)_2\text{SO}_4$	mg/L	144.0	244.0	344.0
9	NaCl	mg/L	5.0	15.0	35.0
10	$\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$	mg/L	34.0	54.0	74.0
11	$\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$	mg/L	30.0	50.0	70.0
12	$\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$	mg/L	5.0	15.0	35.0

2.4.2. Optimization Using Central Composite Design (CCD)

The optimization of the most effective factors and their interactions, including inoculum size, MgSO_4 , K_2HPO_4 , CaCl_2 , phenol concentration, and incubation length, was conducted using response surface methodology (RSM) statistical multifactorial modelling. The parameters were varied at five levels (-2 , -1 , 0 , 1 , and 2) as shown in Table 2.

The quadratic relationship between the response value (y) and the independent parameters (x_1 , x_2 , x_3 , x_4 , x_5 , and x_6) was demonstrated using a second-degree polynomial equation (Equation (3)). The equation included a constant term (b_0) and linear coefficients (b_1 , b_2 , b_3 , b_4 , b_5 , and b_6) for each independent parameter. Additionally, the equation incorporated interaction coefficients (b_{12} , b_{13} , b_{14} , b_{15} , b_{16} , b_{23} , and b_{24}) to account for the combined effects of different parameter combinations. The cross-product coefficients in the model were denoted as b_{25} , b_{26} , b_{34} , b_{35} , b_{36} , b_{45} , b_{46} , and b_{56} . On the other hand, the quadratic coefficients were represented by b_{11} , b_{22} , b_{33} , b_{44} , b_{55} , and b_{66} . A total of 53 iterations were conducted in order to estimate the coefficients of the model through the utilization of multiple linear regressions.

$$\begin{aligned}
 y = & b_0 + b_1x_1 + b_2x_2 + b_3x_3 + b_4x_4 + b_5x_5 + b_6x_6 + b_{11}x_1^2 + b_{22}x_2^2 + b_{33}x_3^2 + b_{44}x_4^2 \\
 & + b_{55}x_5^2 + b_{66}x_6^2 + b_{12}x_1x_2 + b_{13}x_1x_3 + b_{14}x_1x_4 + b_{15}x_1x_5 + b_{16}x_1x_6 \\
 & + b_{23}x_2x_3 + b_{24}x_2x_4 + b_{25}x_2x_5 + b_{26}x_2x_6 + b_{34}x_3x_4 + b_{35}x_3x_5 + b_{36}x_3x_6 \\
 & + b_{45}x_4x_5 + b_{46}x_4x_6 + b_{56}x_5x_6
 \end{aligned} \quad (3)$$

Table 2. Parameters under investigation using a CCD.

No.	Factor	Unit	Levels				
			−2	−1	0	1	2
1	Bacterial inoculum concentration	%	0.3	0.5	1.0	1.5	1.8
2	Incubation period	h	24.0	36.0	48.0	60.0	72.0
3	Phenol concentration	ppm	1.0	3.0	6.0	9.0	12.0
4	Concentration of MgSO ₄	mg/L	10.0	40.0	70.0	100.0	130.0
5	Concentration of K ₂ HPO ₄	mg/L	50.0	100.0	175.0	250.0	300.0
6	Concentration of CaCl ₂	mg/L	1.0	3.0	5.0	8.0	10.0

2.5. Lab-Scale Generation of Bioelectricity and Biodegradation of Phenol in a Continuous Stir Tank Bioreactor

A larger scale generation of bioelectricity and biodegradation of phenol was carried out in a 4-L fermenter (BIOCANVAS, Centrion bioreactor). Before inoculation, the optimized condition was set and standardized. Moreover, the optimum aeration rate, agitation speed, and the dissolved oxygen were tested and fixed at $0.5 v/v/m$, 750 rpm, and 30%, respectively. During the whole fermentation phase, the feed flow rate was set to be 1 mL/min, while the sample collection was every 2 h for 4 days to measure the phenol degradation percentage. Furthermore, power density and potentiodynamic polarization curves were recorded in the potential region from open circuit potential -50 mV to $+500$ mV (vs. Ag/AgCl), while the electrochemical behavior was assessed using cyclic voltammetry at a potential range of -500 mV to $+500$ mV (vs. Ag/AgCl) at a scan rate of 10 mV/s using PARSTAT 226 [20,21].

2.6. Kinetic Model Development of Cells

The specific growth rate of cells (μ) under batch culture was determined through the exponential phase (by applying the optimum conditions obtained from CCD optimization) and it was expressed according to Bera et al. [22]:

$$\mu = \frac{\ln(X_t/X_0)}{t - t_0} \quad (4)$$

The variables X_t and X_0 represent the concentration of cells at specified time points t and t_0 , respectively. The calculation of the parameter μ was derived by analyzing the gradient of a linear graph depicting the natural logarithm of the ratio of the final value (X_t) to the initial value (X_0) against the elapsed time (t) during the logarithmic growth phase of the curve.

In contrast, it was observed that phenol, when used as a substrate, exhibited a suppression of cell development when subjected to elevated starting phenol concentrations. The use of Haldane kinetics was employed to represent the cellular growth phenomenon, as elucidated using the subsequent equation:

$$\mu = \frac{\mu_{\max} S}{K_s + S + S^2/K_i} \quad (5)$$

In the given context, μ represents the specific growth rate (h^{-1}), μ_{\max} denotes the maximum specific growth rate (h^{-1}), K_s signifies the half-saturated constant of substrate ($mg L^{-1}$), and K_i represents the inhibition constant ($mg L^{-1}$).

Furthermore, the experimental results about the breakdown of phenol at different combinations of initial phenol concentrations were employed to calculate the yield of cellular development [23] using the subsequent equation:

$$Y = \frac{X - X_0}{S_0 - S} \quad (6)$$

In the context of cellular growth, Y represents the growth yield of cells. X and X_0 denote the cell concentration and initial cell concentration, respectively, measured in milligrams per liter (mg L^{-1}). Similarly, S and S_0 represent the substrate concentration and initial substrate concentration, respectively, with the substrate being phenol and the units being mg L^{-1} .

3. Results and Discussion

3.1. Nano-Graphite Synthesis and Characterization

After the nanoparticles' synthesis, the vessel containing suspended nanoparticles was dispersed in deionized water. The nanoparticles were ultra-centrifuged at 20,000 rpm for 30 min. The dynamic light scattering technique revealed that the nano-graphite had good stability and relevant homogeneity (zeta potential -38.2 mV and 0.34 PDI) (Figure 2a). The HR-TEM study showed a spherical shape in the nano-range with diameter 86.9 nm (Figure 2b). Yu et al. [24] synthesized graphite nanoparticles using the microemulsion technique and reported that nano-graphite had good dispersibility and agglutination with zeta size reached 200 nm. Moreover, it was reported that nano-graphite has more space for charge/discharge reactions than the porous graphite rod [25] hence it was used in the plated electrodes to enhance the conductivity.

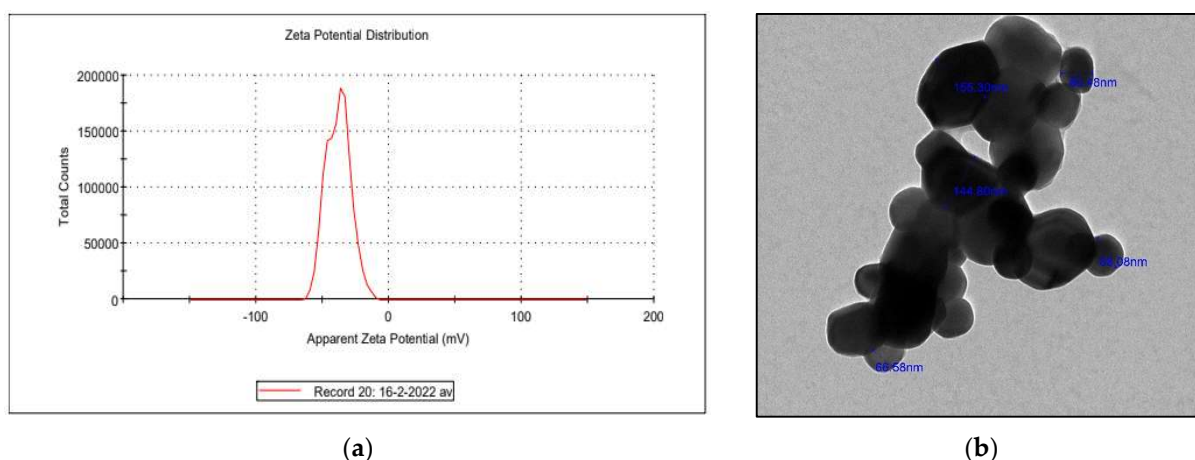


Figure 2. Nano-graphite characterization: zeta potential (a) and HR-TEM (b).

3.2. Optimization of Nutritional and Environmental Factors

3.2.1. Plackett–Burman Design (PBD)

Phenol biodegradation (response 1) and bioelectricity generation (response 2) was achieved by applying the Plackett–Burman design (PBD) using Minitab 19[®] (Table 3). Each individual factor was represented in the regression equations while the significance of each factor was determined using analysis of variance (ANOVA) through assessing t -test and p -values (Table 4). Some variables, namely: inoculum size, CaCl_2 , phenol concentration, and incubation period were the most significant factors for phenol biodegradation with model summary ($S = 2.3$, $R\text{-sq} = 92.56\%$, $R\text{-sq}(\text{adj}) = 81.40\%$ and $R\text{-sq}(\text{pred}) = 44.85\%$) and regression equation:

Table 3. PBD matrix for phenol biodegradation percentage and bioelectricity power density.

Run	Inoculum Size	Culture Volume	Phenol Conc.	pH	Incubation Period	KH ₂ PO ₄	K ₂ HPO ₄	(NH ₄) ₂ SO ₄	NaCl	FeCl ₃	MgSO ₄	CaCl ₂	Phenol Degradation %	Phenol Removal Amount per OD600 (mg/OD600)	Power Density (mW/cm ³)
1	1	1	-1	-1	1	1	-1	1	1	-1	-1	-1	72.57	7.3	6.10
2	-1	-1	-1	1	-1	1	-1	1	1	1	1	-1	85.24	8.7	19.57
3	1	-1	1	1	-1	-1	-1	-1	1	-1	1	-1	79.75	8.9	11.63
4	1	-1	-1	1	1	-1	1	1	-1	-1	-1	-1	76.79	7.4	4.17
5	1	1	-1	1	1	-1	-1	-1	-1	1	-1	1	73.47	7.3	5.56
6	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	83.33	8.7	16.32
7	-1	-1	1	1	-1	1	1	-1	-1	-1	-1	1	81.22	8.8	12.82
8	-1	1	-1	1	1	1	1	-1	-1	1	1	-1	83.76	8.0	12.26
9	1	1	1	-1	-1	1	1	-1	1	1	-1	-1	71.87	6.4	5.72
10	-1	1	1	1	1	-1	-1	1	1	-1	1	1	77.79	7.2	11.18
11	-1	1	1	-1	-1	-1	-1	1	-1	1	-1	1	79.58	7.7	9.93
12	-1	1	1	-1	1	1	-1	-1	-1	-1	1	-1	82.43	8.2	17.82
13	0	0	0	0	0	0	0	0	0	0	0	0	75.41	7.1	9.23
14	-1	-1	-1	-1	1	-1	1	-1	1	1	1	1	82.49	8.6	13.78
15	1	1	-1	-1	-1	-1	1	-1	1	-1	1	1	77.73	7.9	7.90
16	-1	-1	1	-1	1	-1	1	1	1	1	-1	-1	80.29	7.0	9.85
17	1	-1	1	1	1	1	-1	-1	1	1	-1	1	62.52	5.2	8.58
18	-1	1	-1	1	-1	1	1	1	1	-1	-1	1	81.99	8.1	9.45
19	1	-1	1	-1	1	1	1	1	-1	-1	1	1	69.58	6.7	5.63
20	1	1	1	1	-1	-1	1	1	-1	1	1	-1	75.63	7.8	11.58
21	1	-1	-1	-1	-1	1	-1	1	-1	1	1	1	73.36	7.5	8.67

Table 4. Analysis of variance of phenol biodegradation percentage and bioelectricity power density.

Source	Phenol Biodegradation Percentage					Bioelectricity Power Density				
	DF	Adj SS	Adj MS	F-Value	p-Value	DF	Adj SS	Adj MS	F-Value	p-Value
Model	12	572.356	47.696	8.29	0.003	12	304.938	25.412	5.95	0.009
Linear	12	572.356	47.696	8.29	0.003	12	304.938	25.412	5.95	0.009
Inoculum size	1	359.891	359.891	62.57	0.000	1	164.910	164.910	38.61	0.000
Culture volume	1	0.255	0.255	0.04	0.838	1	9.126	9.126	2.14	0.182
Phenol conc.	1	45.240	45.240	7.87	0.023	1	0.049	0.049	0.01	0.917
pH	1	1.210	1.210	0.21	0.659	1	1.275	1.275	0.30	0.600
Incubation period	1	39.256	39.256	6.83	0.031	1	17.428	17.428	4.08	0.078
KH ₂ PO ₄	1	24.864	24.864	4.32	0.071	1	1.119	1.119	0.26	0.623
K ₂ HPO ₄	1	6.407	6.407	1.11	0.322	1	24.620	24.620	5.76	0.043
(NH ₄) ₂ SO ₄	1	1.647	1.647	0.29	0.607	1	13.236	13.236	3.10	0.116
NaCl	1	2.394	2.394	0.42	0.537	1	0.049	0.049	0.01	0.917
FeCl ₃	1	11.220	11.220	1.95	0.200	1	0.305	0.305	0.07	0.796
MgSO ₄	1	29.089	29.089	5.06	0.055	1	49.644	49.644	11.62	0.009
CaCl ₂	1	50.880	50.880	8.85	0.018	1	23.177	23.177	5.43	0.048
Error	8	46.014	5.752			8	34.171	4.271		
Total	20	618.370				20	339.109			

$$\begin{aligned} \text{Phenol degradation \%} = & 77.472 - 4.242 \text{ Inoculum size} + 0.113 \text{ Culture volume} - 1.504 \text{ Phenol conc.} \\ & + 0.246 \text{ pH} - 1.401 \text{ Incubation period} - 1.115 \text{ KH}_2\text{PO}_4 + 0.566 \text{ K}_2\text{HPO}_4 - 0.287 \text{ (NH}_4\text{)}_2\text{SO}_4 - 0.346 \text{ NaCl} - \\ & 0.749 \text{ FeCl}_3 + 1.206 \text{ MgSO}_4 - 1.595 \text{ CaCl}_2 \end{aligned} \quad (7)$$

On the other hand, inoculum size, MgSO₄, K₂HPO₄, and CaCl₂ were found to be significant for bioelectricity generation with model summary (S = 2.06, R-sq = 89.92%, R-sq(adj) = 74.81% and R-sq(pred) = 21.53%) and regression equation:

$$\begin{aligned} \text{Power density} = & 10.373 - 2.872 \text{ Inoculum size} - 0.676 \text{ Culture volume} + 0.050 \text{ Phenol conc.} \\ & + 0.253 \text{ pH} - 0.933 \text{ Incubation period} + 0.237 \text{ KH}_2\text{PO}_4 - 1.110 \text{ K}_2\text{HPO}_4 - 0.813 \text{ (NH}_4\text{)}_2\text{SO}_4 - \\ & 0.050 \text{ NaCl} + 0.123 \text{ FeCl}_3 + 1.576 \text{ MgSO}_4 - 1.076 \text{ CaCl}_2 \end{aligned} \quad (8)$$

Furthermore, the production of Pareto charts was undertaken to visually represent the set of factors being tested in relation to their impact on two specific outcomes: phenol biodegradation (response 1) and bioelectricity generation (response 2) (as depicted in Figure 3). Hence, the aforementioned parameters were chosen to undergo further optimization using five coded levels (−2, −1, 0, 1, and 2) in order to conduct a comprehensive study of the entire process through the implementation of a central composite design (CCD).

3.2.2. Central Composite Design (CCD)

Parameters, namely: inoculum size (x1), incubation period (x2), phenol concentration (x3), MgSO₄ (x4), CaCl₂ (x5), and K₂HPO₄ (x6) were investigated using Minitab 19[®] with phenol degradation and bioelectricity generation (Table 5) as responses. The results of the second-order response surface model fitting in the form of an analysis of variance (ANOVA) were calculated (Table 6). The phenol degradation model was shown to be significant with (S = 2.0, R-sq = 95.64%, R-sq(adj) = 90.93% and R-sq(pred) = 68.30%) and regression equation:

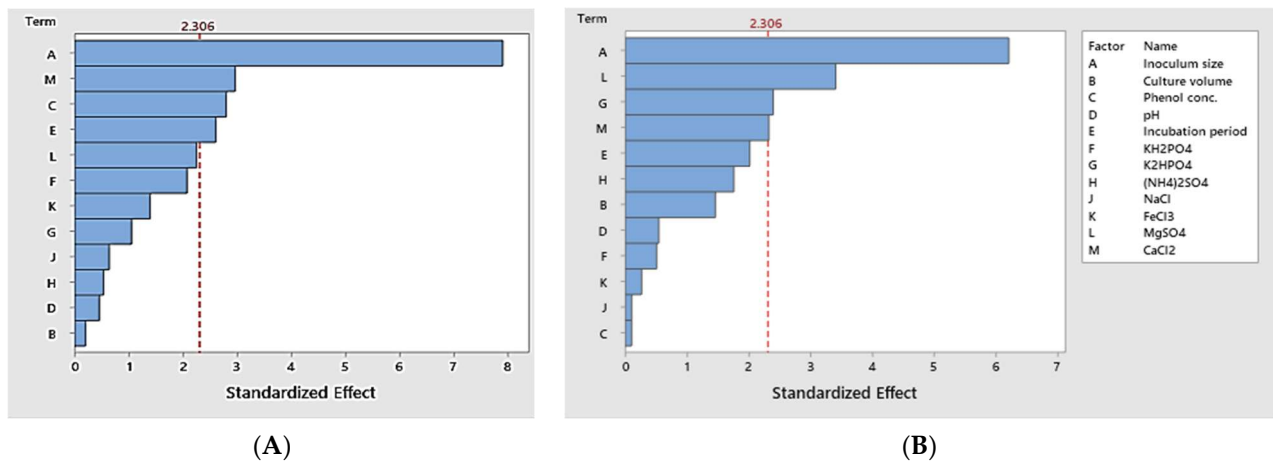


Figure 3. Pareto chart showing the contribution percentage and the effects of all parameters on the phenol biodegradation percentage (A) and the bioelectricity power density (B).

$$\begin{aligned} \text{Phenol degradation \%} = & 89.866 + 0.413 x_1 - 0.458 x_2 + 0.580 x_3 + 0.173 x_4 + 0.209 x_5 - 0.584 x_6 - \\ & 0.144 x_1x_1 - 5.304 x_2x_2 - 0.293 x_3x_3 - 1.014 x_4x_4 + 0.382 x_5x_5 + 0.112 x_6x_6 + 1.104 x_1x_2 - 0.123 x_1x_3 - \\ & 3.839 x_1x_4 - 0.816 x_1x_5 + 1.473 x_1x_6 + 1.663 x_2x_3 + 0.562 x_2x_4 - 2.584 x_2x_5 + 1.159 x_2x_6 - \\ & 0.780 x_3x_4 + 2.247 x_3x_5 - 1.589 x_3x_6 - 0.445 x_4x_5 - 0.431 x_4x_6 + 1.694 x_5x_6 \end{aligned} \quad (9)$$

However, the bioelectricity generation model was also shown to be significant with ($S = 5.04$, $R\text{-sq} = 91.70\%$, $R\text{-sq}(\text{adj}) = 82.74\%$ and $R\text{-sq}(\text{pred}) = 56.99\%$) and regression equation:

$$\begin{aligned} \text{Power density} = & 85.75 + 0.668 x_1 + 3.982 x_2 + 2.240 x_3 - 0.305 x_4 - 3.258 x_5 + 0.500 x_6 - 3.854 x_1x_1 - \\ & 5.926 x_2x_2 - 0.353 x_3x_3 + 0.611 x_4x_4 - 0.591 x_5x_5 - 2.728 x_6x_6 - 0.842 x_1x_2 + \\ & 1.618 x_1x_3 - 3.548 x_1x_4 + 2.275 x_1x_5 - 2.098 x_1x_6 - 5.855 x_2x_3 + 0.716 x_2x_4 + \\ & 0.926 x_2x_5 + 1.877 x_2x_6 + 4.385 x_3x_4 + 4.561 x_3x_5 - 0.610 x_3x_6 + 1.585 x_4x_5 + 0.354 x_4x_6 + 2.054 x_5x_6 \end{aligned} \quad (10)$$

Table 5. CCD matrix for phenol biodegradation percentage and bioelectricity power density after significant parameters optimization.

Run	Inoculum Size	Incubation Period	Phenol Concentration	MgSO ₄	CaCl ₂	K ₂ HPO ₄	Phenol Degradation %	Phenol Removal Amount per OD600 (mg/OD600)	Power Density (mW/cm ³)
1	−1	1	−1	−1	1	−1	68.22	6.3	72.963
2	0	0	0	0	0	0	89.57	9.5	86.203
3	1	−1	−1	1	1	1	82.48	7.2	49.105
4	−1	1	−1	1	1	1	80.81	7.1	81.359
5	1	−1	−1	−1	1	−1	86.24	8.5	60.666
6	1	1	−1	−1	1	1	87.12	9.9	82.600
7	−1	−1	1	1	−1	−1	86.17	8.7	81.983
8	−1	−1	1	−1	1	−1	89.59	10.5	62.968
9	−1	1	−1	1	−1	−1	89.49	9.4	81.847
10	−1	−1	−1	1	−1	1	88.46	9.9	67.025
11	0	0	0	2	0	0	85.32	8.5	90.000
12	1	1	1	1	−1	−1	86.14	8.0	70.788
13	0	0	0	0	0	−2	92.65	11.4	73.952

Table 5. Cont.

Run	Inoculum Size	Incubation Period	Phenol Concentration	MgSO ₄	CaCl ₂	K ₂ HPO ₄	Phenol Degradation %	Phenol Removal Amount per OD600 (mg/OD600)	Power Density (mW/cm ³)
14	-1	1	1	1	-1	1	81.12	8.8	82.179
15	0	0	0	0	-2	0	93.34	12.4	109.419
16	1	1	1	-1	-1	1	91.55	11.6	67.593
17	0	0	0	0	0	0	89.57	9.0	86.203
18	2	0	0	0	0	0	92.28	10.3	70.984
19	1	-1	1	-1	1	1	92.59	11.9	82.494
20	0	0	0	0	0	0	89.57	10.3	88.203
21	0	0	0	0	2	0	90.78	10.8	70.287
22	-1	-1	-1	1	1	-1	89.71	9.6	45.385
23	1	1	-1	1	-1	1	87.80	9.5	71.394
24	1	1	1	-1	1	-1	84.07	8.7	75.400
25	-1	-1	1	1	1	1	90.82	10.0	84.089
26	1	-1	-1	-1	-1	1	84.09	8.2	73.238
27	-1	1	1	1	1	-1	92.74	11.7	73.920
28	1	-1	1	1	-1	1	68.58	6.9	61.420
29	1	1	-1	-1	-1	-1	84.67	8.0	92.136
30	-1	1	-1	-1	-1	1	76.88	7.5	93.331
31	-1	1	1	-1	-1	-1	83.00	8.5	60.240
32	0	0	0	0	0	0	89.57	9.6	86.203
33	-1	1	1	-1	1	1	80.46	8.4	62.299
34	0	-2	0	0	0	0	69.73	7.2	52.296
35	0	0	0	0	0	2	89.31	9.8	78.652
36	-1	-1	-1	-1	-1	-1	82.75	8.0	74.055
37	1	1	-1	1	1	-1	69.92	7.3	63.941
38	1	-1	1	1	1	-1	81.02	8.5	87.955
39	0	0	0	0	0	0	89.57	9.7	87.203
40	-2	0	0	0	0	0	87.63	9.9	72.612
41	-1	-1	-1	-1	1	1	83.27	8.5	53.603
42	1	1	1	1	1	1	82.72	8.2	85.810
43	0	0	0	0	0	0	89.57	9.4	86.203
44	0	2	0	0	0	0	68.90	7.6	74.726
45	0	0	-2	0	0	0	88.70	8.7	79.572
46	0	0	2	0	0	0	90.02	10.0	92.032
47	1	-1	1	-1	-1	-1	86.81	8.5	85.437
48	0	0	0	0	0	0	89.57	9.3	86.203
49	-1	-1	1	-1	-1	1	67.94	7.2	68.347
50	0	0	0	0	0	0	89.57	8.8	86.203
51	0	0	0	0	0	0	89.57	8.9	73.203
52	1	-1	-1	1	-1	-1	82.83	7.0	65.595
53	0	0	0	-2	0	0	87.63	8.0	89.322

Table 6. Analysis of variance of phenol biodegradation percentage and bioelectricity power density.

Source	Phenol Biodegradation Percentage					Bioelectricity Power Density				
	DF	Adj SS	Adj MS	F-Value	p-Value	DF	Adj SS	Adj MS	F-Value	p-Value
Model	27	2380.87	88.180	20.31	0.000	27	7035.73	260.58	10.23	0.000
Linear	6	45.26	7.543	1.74	0.154	6	1291.21	215.20	8.45	0.000
x1	1	6.81	6.806	1.57	0.222	1	17.85	17.85	0.70	0.410
x2	1	8.37	8.372	1.93	0.177	1	634.37	634.37	24.91	0.001
x3	1	13.48	13.479	3.10	0.090	1	200.70	200.70	7.88	0.010
x4	1	1.20	1.204	0.28	0.603	1	3.73	3.73	0.15	0.705
x5	1	1.76	1.756	0.40	0.531	1	424.55	424.55	16.67	0.001
x6	1	13.64	13.642	3.14	0.088	1	10.01	10.01	0.39	0.536
Square	6	1012.59	168.764	38.87	0.000	6	2163.20	360.53	14.16	0.000
x1 x1	1	0.69	0.692	0.16	0.693	1	496.37	496.37	19.49	0.001
x2 x2	1	939.94	939.937	216.49	0.001	1	1173.38	1173.38	46.07	0.001
x3 x3	1	2.86	2.863	0.66	0.424	1	4.17	4.17	0.16	0.689
x4 x4	1	34.35	34.351	7.91	0.009	1	12.49	12.49	0.49	0.490
x5 x5	1	4.88	4.883	1.12	0.299	1	11.65	11.65	0.46	0.505
x6 x6	1	0.42	0.421	0.10	0.758	1	248.71	248.71	9.77	0.004
2-Way Interaction	15	1323.03	88.202	20.31	0.000	15	3581.32	238.75	9.37	0.000
x1 x2	1	39.03	39.029	8.99	0.006	1	22.66	22.66	0.89	0.355
x1 x3	1	0.48	0.480	0.11	0.742	1	83.74	83.74	3.29	0.082
x1 x4	1	471.71	471.706	108.64	0.001	1	402.83	402.83	15.82	0.001
x1 x5	1	21.32	21.320	4.91	0.036	1	165.58	165.58	6.50	0.017
x1 x6	1	69.44	69.443	15.99	0.001	1	140.85	140.85	5.53	0.027
x2 x3	1	88.45	88.445	20.37	0.001	1	1097.03	1097.03	43.07	0.001
x2 x4	1	10.10	10.103	2.33	0.140	1	16.43	16.43	0.64	0.429
x2 x5	1	213.62	213.624	49.20	0.001	1	27.42	27.42	1.08	0.309
x2 x6	1	43.01	43.013	9.91	0.004	1	112.70	112.70	4.42	0.046
x3 x4	1	19.47	19.469	4.48	0.044	1	615.19	615.19	24.15	0.001
x3 x5	1	161.55	161.550	37.21	0.001	1	665.64	665.64	26.13	0.001
x3 x6	1	80.77	80.772	18.60	0.001	1	11.92	11.92	0.47	0.500
x4 x5	1	6.34	6.337	1.46	0.238	1	80.38	80.38	3.16	0.088
x4 x6	1	5.93	5.934	1.37	0.253	1	4.01	4.01	0.16	0.695
x5 x6	1	91.80	91.801	21.14	0.001	1	134.95	134.95	5.30	0.030
Error	25	108.55	4.342			25	636.74	25.47		
Lack-of-Fit	17	108.55	6.385			17	473.85	27.87	1.37	0.336
Pure Error	8	0.00	0.000			8	162.89	20.36		
Total	52	2489.42				52	7672.47			

Furthermore, the 3D curve interpretation revealed that the phenol biodegradation percentage and bioelectricity power density increased by decreasing the inoculum size and incubation period (Figures 4 and 5). The correlation between the initial phenol concentration (x_3) and the incubation period (x_5) revealed that, upon increasing both factors, maximum phenol degradation and bioelectricity generation was noticed (almost in a similar pattern) (Figures 4 and 5),

while a completely different pattern was noticed when correlating between the initial phenol concentration (x_3) and pH (x_4) (Figures 4 and 5). This is in accordance with Puig et al. [26], who stated that, by increasing the pH to be higher than the optimal one, anodic bacteria were affected, and power generation ceased. Moreover, it was reported that, when the cultural media pH decreased with growth, the phenol degradation was impeded below pH 5.4 [27].

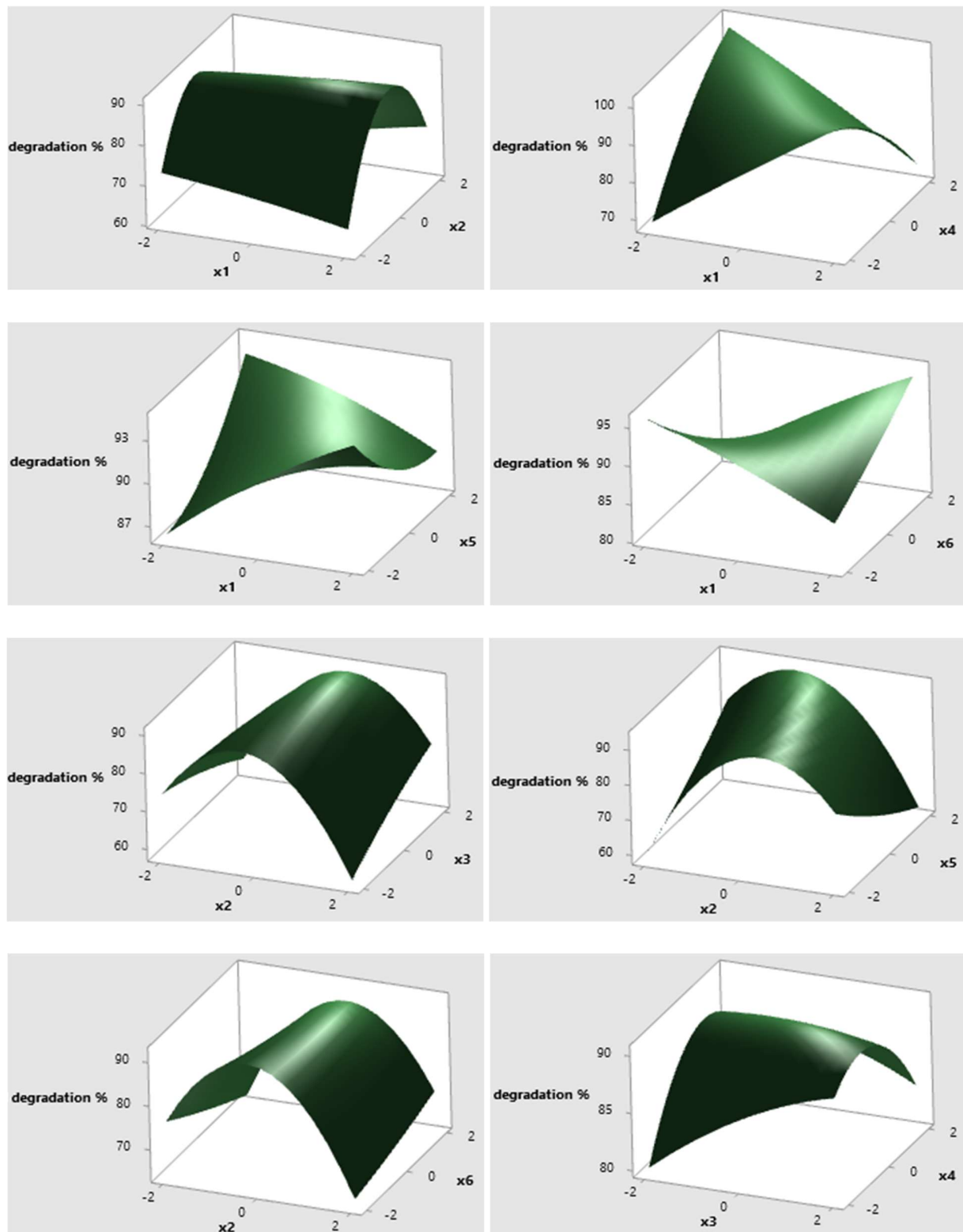


Figure 4. Cont.

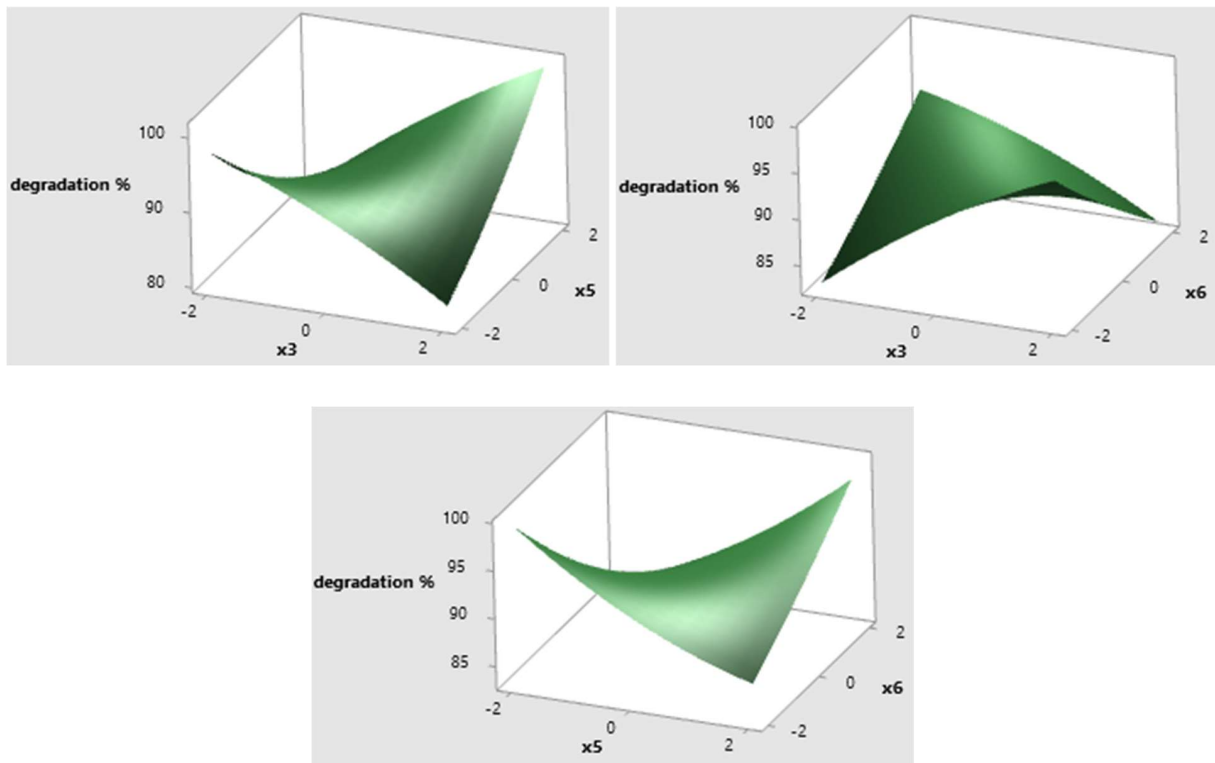


Figure 4. Three-dimensional surface plots for the effects of the significant tested parameter interactions that led to maximum phenol biodegradation.

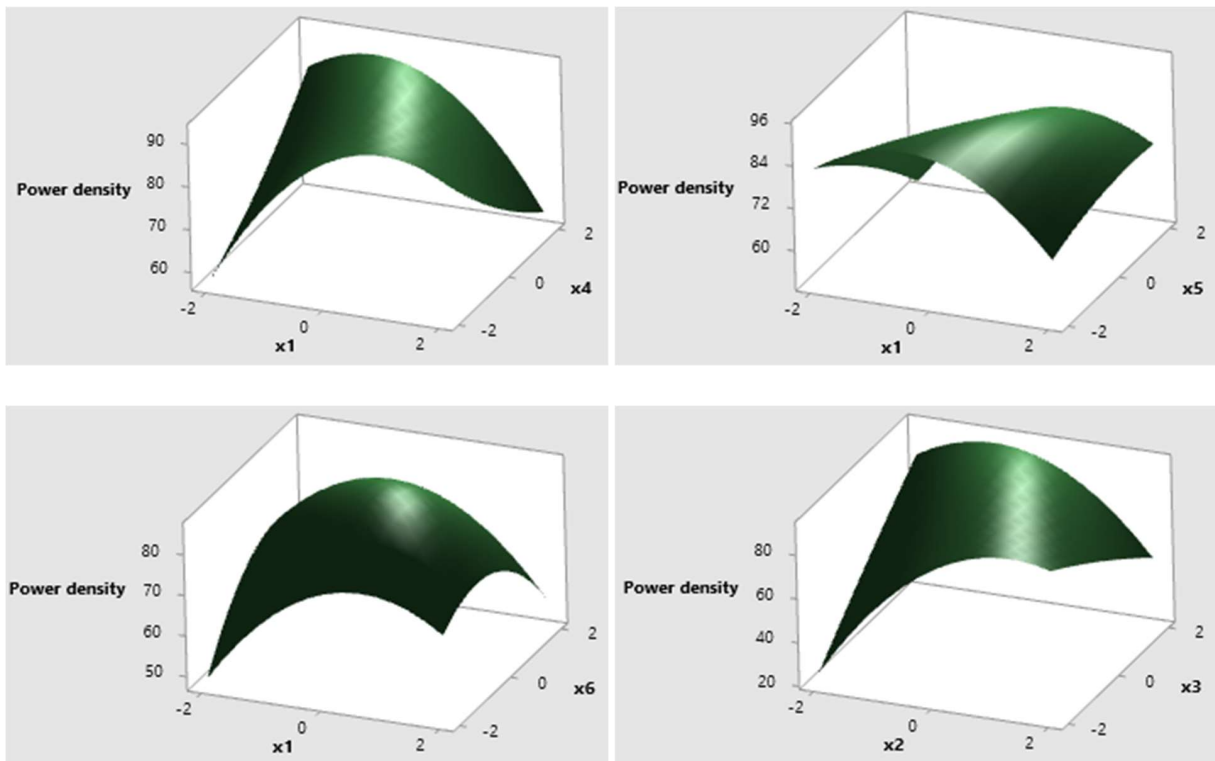


Figure 5. Cont.

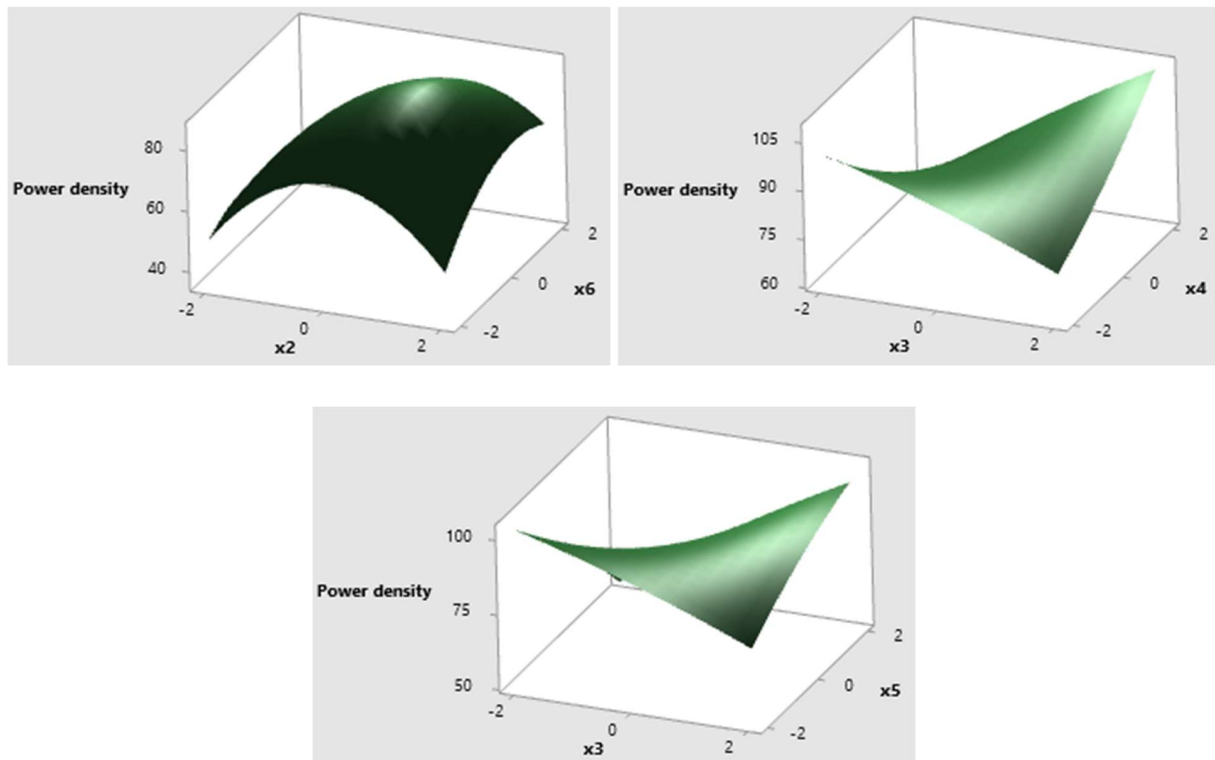


Figure 5. Three-dimensional surface plots for the effects of the tested significant parameter interactions that led to maximum bioelectricity generation.

The optimization study of phenol degradation and bioelectricity generation revealed that the optimum values for each factor that yield the maximum percentage of phenol degradation (93.34%) and power density (109.419 mW/cm^3) were: bacterial inoculum concentration, 1.0%; incubation period, 48 h; phenol concentration, 6.0 ppm; MgSO_4 concentration, 70.0 mg/L; K_2HPO_4 concentration, 175 mg/L; and CaCl_2 concentration, 1.0 mg/L.

Aisami et al. [28] considered *Pseudomonas* sp. strain AQ5-04 as a phenol degrader. Upon optimization, a pH value of 6.8 was identified as the best pH for phenol degradation. The bacterium was able to degrade up to 90% out of 5 mg/L phenol. However, the maximum percentage of phenol biodegradation has been shown to be 92.64% with the optimized conditions when compared to unoptimized conditions in the same unit volume [29]. Furthermore, the biodegradation of phenolic compounds in MFC exhibited a power density of 67.2 mW/m^2 and phenol degradation of 83.2% [21].

3.3. Bioelectricity Generation and Phenol Biodegradation under Continuous Conditions Using a Stir Tank Bioreactor

The data in Figure 6a show the phenol biodegradation percentage within 96 h, and revealed a sharp reduction in phenol with maximum phenol degradation (97.8%) after 48 h incubation using a 4 L continuous stir tank bioreactor. Moreover, the data in Figure 6b show the bioelectricity generation revealing a significant increase in the power density during the first 24 h and reaching an optimum value (0.382 mW/cm^3) after 72 h incubation. However, the Potentiodynamic polarization curve showed a sharp decrease in the generated potential (V) while increasing the current density (Figure 6c). Furthermore, cyclic voltammogram showed a steady state with a peak current at about 0.98 and 0.62 V corresponding to the phenol biodegradation (Figure 6d).

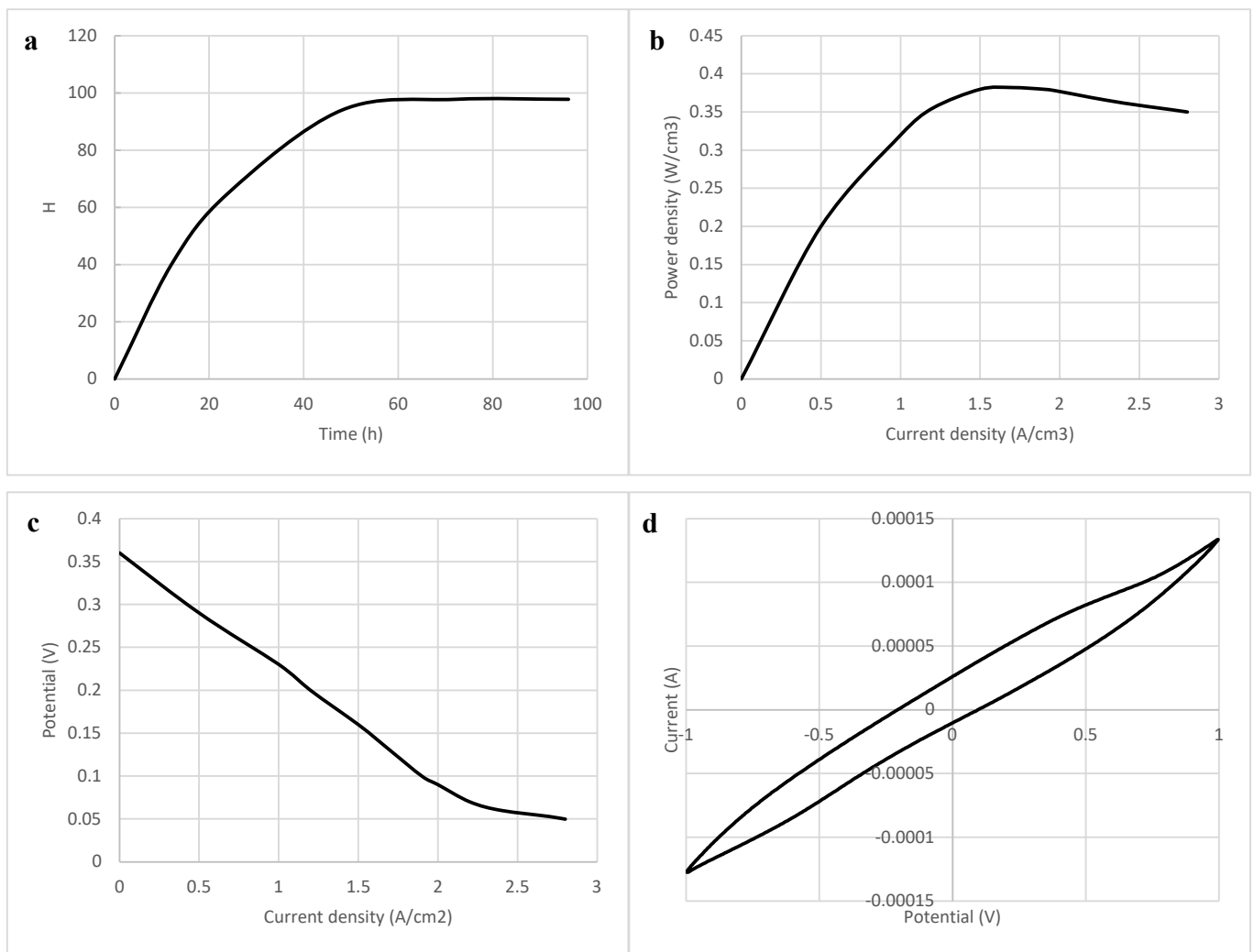


Figure 6. Phenol biodegradation percentage during 96 h (a), bioelectricity power density curve (b), Potentiodynamic polarization curve (c), and cyclic voltammetry (d).

It was reported that, in fed batch MFC, phenol biodegradation achieved 71.8%, while the bioelectricity reached 0.305 mW/m^3 [30]. Furthermore, Moreno et al. [10] stated that biodegradation of phenol produces a concomitant generation of energy in the continuous-flow MFCs. The biodegradation of phenol in batch-operated MFCs with single-rod electrodes was 71%. Nevertheless, changing the mode of operation from batch to continuous flow resulted in increased biodegradation rates as well as increased power and current densities. Additionally, the use of nano-graphite electrodes resulted in an enhancement in the performance of MFCs in terms of the electrochemical outputs produced by the device, and this improvement was seen for batch as well as continuous flow modes of operation. This was owing to the fact that graphite nanoparticles had an enlarged surface area, which made it easier for biofilm to grow and for electrons to be transferred.

Ziaedini et al. [30] reported that phenolic oxidation peaks at $120 \pm 30 \text{ mV}$ is in association with bacterial cell wall, while the peak at about $600 \pm 20 \text{ mV}$ can be attributed to a soluble active redox component secreted by electrogenic bacteria into the culture medium.

3.4. Kinetics Model for Monitoring the Drastic Effect of Phenol on Bacterial Cells

Using the optimum conditions obtained through the response surface methodology, the data in Figure 7 show the specific growth rate (μ, h^{-1}) variations while using different phenol concentrations. Haldane's model gave the best fit to achieve a significant correlation coefficient (R^2) value (0.9865). It was revealed that the cells reported maximum specific

growth rate with an initial phenol concentration of approximately 9 mg L^{-1} . According to Bera et al. [22], a decline in the specific growth rate might be related to the fact that increased concentrations of phenol could inhibit the metabolic activity of bacteria, which would ultimately result in cell death. Based on the results of the current growth kinetic investigation, it was determined that the bacterial cells were capable of efficiently breaking down phenol at concentrations of up to 9 mg L^{-1} . This may be attributed to the fact that the bacterial strains were naturally exposed for extended periods of time to quantities of hazardous petroleum compounds [31]. Hasan et al. [32] reported that *Pseudomonas* and *Bacillus* sp. strains transformed phenol into catechol via the *ortho*-cleavage pathway. It was reported that *Burkholderia* sp. can use both the catechol and protocatechuate branches of the β -keto adipate pathway during the early stage of phenol degradation, and only the catechol branch during the late stage [33]. In another study, *Burkholderia* sp. was reported to use a meta-ring opening cleavage phenol degradation pathway [34]. Hence, the observed high specific growth rate, initial phenol concentration, and high phenol degradation and bioelectricity generation could be attributed to the fact that we are using a bacterial consortium which may use different phenolic degradation pathways.

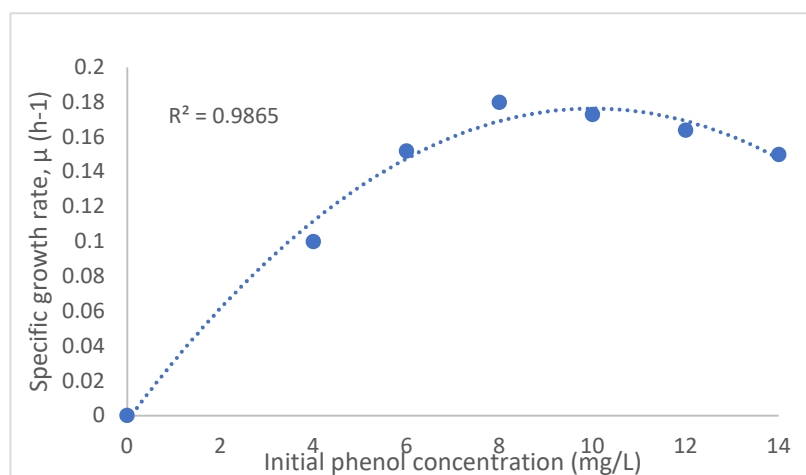


Figure 7. Bacterial specific growth rate as affected by initial phenol concentration.

As plotted in Figure 8, the bacterial growth yield (Y) was estimated using Equation (3). The calculated values of bacterial growth yield while using phenol as a sole carbon source were listed in Table 7. When the initial phenol concentration was between 100 and 600 mg/L , the growth yields ranged from 0.225547 to 0.254036 mg mg^{-1} with the average growth yield reaching $0.243177 \pm 0.011498 \text{ mg mg}^{-1}$. Similar experiments were conducted and higher growth yields were reported while using lower initial phenol concentrations, e.g., Abuhamed et al. [35], who reported a 0.44 mg mg^{-1} average growth yield upon using 10–200 mg L^{-1} initial phenol concentrations. Another study by Lin and Gu [31] reported reaching a 0.340 mg mg^{-1} average growth yield while using 50 to 600 mg L^{-1} initial phenol concentrations.

Table 7. Growth yield (Y) evaluation under various initial phenol concentrations.

Run Number	Initial Phenol Concentration (mg/L)	Bio-Kinetic Parameter (Y , mg/mg)
1	4	5.812
2	6	8.096
3	8	9.473

Table 7. Cont.

Run Number	Initial Phenol Concentration (mg/L)	Bio-Kinetic Parameter (Y, mg/mg)
4	10	10.370
5	12	10.613
6	14	10.706
Mean		9.179
Standard deviation		1.918

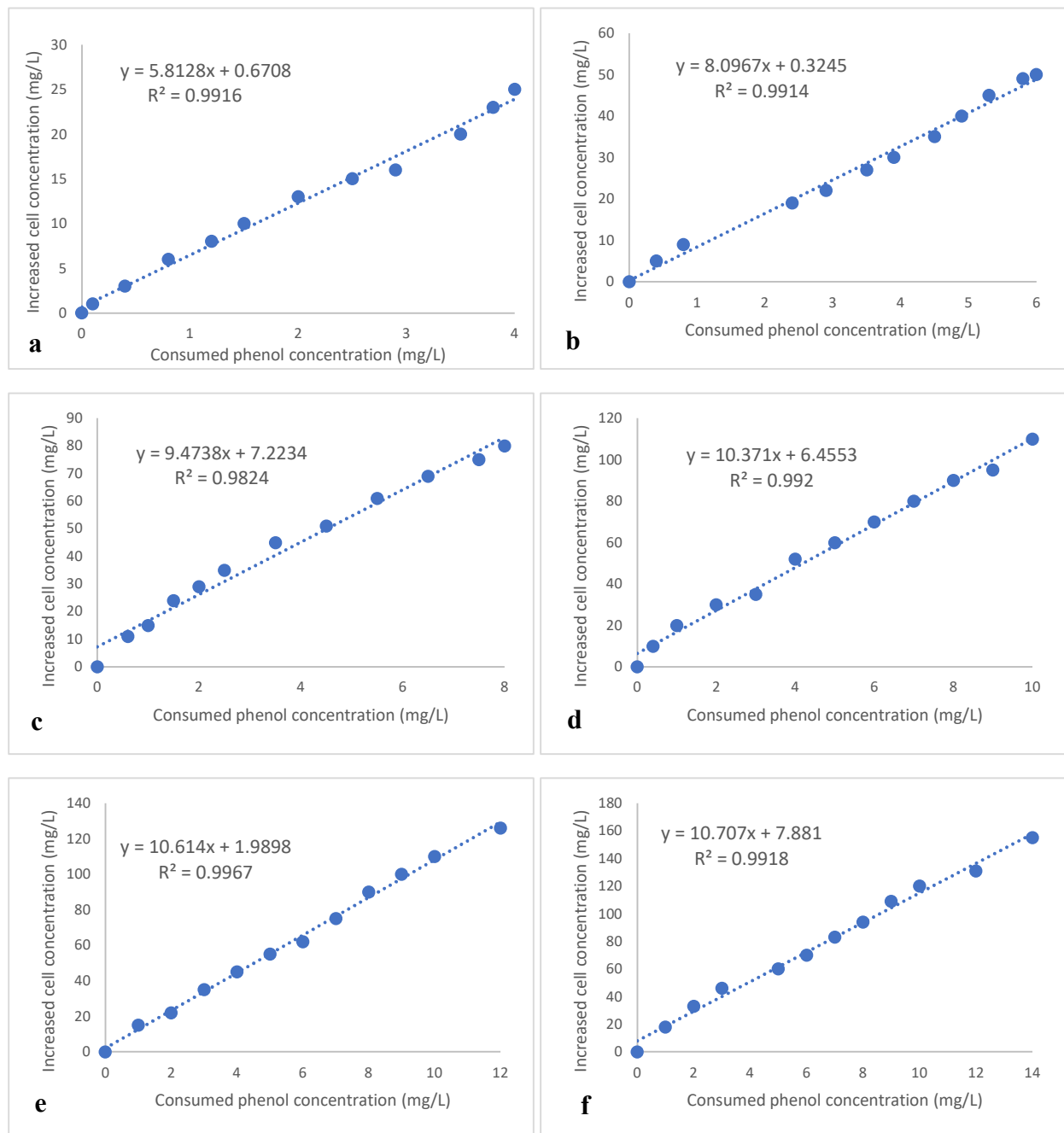


Figure 8. Bacterial growth yield kinetics under batch conditions. Initial phenol concentrations: 4 (a), 6 (b), 8 (c), 10 (d), 12 (e), and 14 (f).

4. Conclusions

The data of the present investigation demonstrated that, on using a continuous stir tank bioreactor, phenol degradation and bioelectricity generation reached 97.8% and 0.382 W/cm³, respectively. The optimization analysis for maximum phenol degradation and energy generation showed that the optimal culture conditions were bacterial inoculum concentration, 1.0%; incubation period, 48 h; phenol concentration, 6.0 ppm; MgSO₄ concentration, 70.0 mg/L; K₂HPO₄ concentration, 175 mg/L; and CaCl₂ concentration, 1.0 mg/L. Moreover, the aeration rate, agitation speed, and dissolved oxygen were 0.5 v/v/m, 750 rpm, and 30%, respectively, using a CCD and nano-graphite electrodes for power estimation. Haldane's kinetics model reported the best fit to achieve a significant correlation coefficient (R²) value (0.9865) with maximum specific growth rate with an initial phenol concentration of approximately 9 mg L⁻¹. The degradation kinetics study demonstrated that the specific growth rates (μ , h⁻¹) varied with the initial phenol concentration. Therefore, the present study revealed that the consortium of six strains displayed good phenol degradation performance. The phenol degradation rate of the bacterial strains was highly dependent on the initial phenol concentration and could be considered an economical and sustainable approach to the degradation of phenol within industrial wastewater as well as electricity generation.

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