

Article

# Post-Electric Current Treatment Approaching High-Performance Flexible n-Type Bi<sub>2</sub>Te<sub>3</sub> Thin Films

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**Abstract:** Inorganic n-type Bi<sub>2</sub>Te<sub>3</sub> flexible thin film, as a promising near-room temperature thermoelectric material, has attracted extensive research interest and application potentials. In this work, to further improve the thermoelectric performance of flexible Bi<sub>2</sub>Te<sub>3</sub> thin films, a post-electric current treatment is employed. It is found that increasing the electric current leads to increased carrier concentration and electric conductivity from 1874 S cm<sup>-1</sup> to 2240 S cm<sup>-1</sup>. Consequently, a high power factor of ~10.70 μW cm<sup>-1</sup> K<sup>-2</sup> at room temperature can be achieved in the Bi<sub>2</sub>Te<sub>3</sub> flexible thin films treated by the electric current of 0.5 A, which is competitive among flexible n-type Bi<sub>2</sub>Te<sub>3</sub> thin films. Besides, the small change of relative resistance <10% before and after bending test demonstrates excellent bending resistance of as-prepared flexible Bi<sub>2</sub>Te<sub>3</sub> films. A flexible device composed of 4 n-type legs generates an open circuit voltage of ~7.96 mV and an output power of 24.78 nW at a temperature difference of ~35 K. Our study indicates that post-electric current treatment is an effective method in boosting the electrical performance of flexible Bi<sub>2</sub>Te<sub>3</sub> thin films.

**Keywords:** thermoelectric; Bi<sub>2</sub>Te<sub>3</sub>; flexible; thin film; electric current treatment

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## 1. Introduction

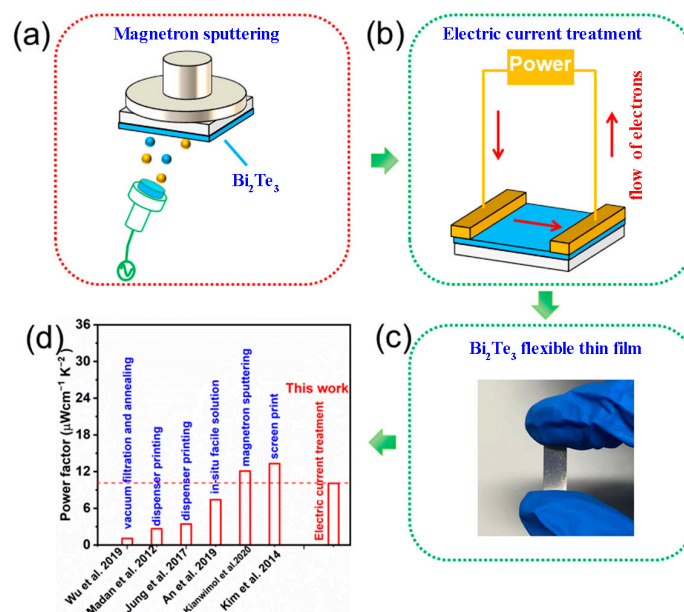
Flexible thermoelectric (TE) devices, with the advantages of being self-powering, sustainable, and of small volume, provide a reliable power supply solution for wearable electronics, implantable electronics, and chip-sensors at near-room temperature [1–3]. The main challenge for flexible TE devices lies in the TE material performance and device integration technology. The performance of TE materials is evaluated by dimensionless figure-of-merit  $ZT$  ( $ZT = S^2\sigma T/\kappa$ , where  $S$ ,  $\sigma$ ,  $S^2\sigma$ ,  $T$ , and  $\kappa$  represent Seebeck coefficient, electrical conductivity, power factor, absolute temperature, and thermal conductivity, respectively) [4,5]. Recently, the flexible thin film (f-TF) provides an avenue for flexible TE devices due to the excellent flexibility, comparing with the bulk TE counterparts [6,7]. Organic f-TFs, including P3HT ( $S^2\sigma < \sim 0.04 \mu\text{W cm}^{-1} \text{K}^{-2}$  at room temperature) [8], PEDOT:PSS ( $S^2\sigma < \sim 0.5 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [9], and PANI ( $S^2\sigma < \sim 0.6 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [10], are typically highly flexible with relatively low TE performance compared with the inorganic f-TFs. Inorganic f-TFs with excellent TE performance have received extensive attention, such as SnSe ( $S^2\sigma = \sim 3.5 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [11], CuI ( $S^2\sigma = \sim 3.75 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [12], Ca<sub>0.35</sub>CoO<sub>2</sub> ( $S^2\sigma = \sim 0.5 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [13], Ag<sub>2</sub>Se ( $S^2\sigma = \sim 9.874 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [14], and Bi<sub>2</sub>Te<sub>3</sub>-based f-TFs ( $S^2\sigma = \sim 25 \mu\text{W cm}^{-1} \text{K}^{-2}$  at 300 K) [15].

Among many inorganic f-TFs, Bi<sub>2</sub>Te<sub>3</sub> based ones are the most widely applied due to the excellent TE performance at room temperature [16,17]. Wu et al. [18] reported that

hybridizing  $\text{Bi}_2\text{Te}_3$  f-TFs with graphene oxide by vacuum filtration and annealing, and an  $S^2\sigma$  of  $\sim 1.08 \mu\text{W cm}^{-1} \text{K}^{-2}$ , is approached at  $\sim 297 \text{ K}$ . Chen et al. [19] successfully prepared  $\text{Bi}_2\text{Te}_3$  nanowire-based f-TFs with an  $S^2\sigma$  of  $1.10 \mu\text{W cm}^{-1} \text{K}^{-2}$  at  $400 \text{ K}$  by solution phase printing methods. Madan et al. [20] successfully fabricated Se-doped  $\text{Bi}_2\text{Te}_3$  based f-TFs with the  $S^2\sigma$  of  $\sim 2.65 \mu\text{W cm}^{-1} \text{K}^{-2}$  at  $\sim 297 \text{ K}$  by mechanically alloyed and dispense printing method.  $\text{Bi}_2\text{Te}_3$  f-TFs fabricated by in situ solution method has approached  $\sim 7.4 \mu\text{W cm}^{-1} \text{K}^{-2}$  at  $\sim 297 \text{ K}$  [21].  $\text{Bi}_2\text{Te}_3$  f-TFs fabricated by thermal diffusion methods can achieve the  $S^2\sigma$  of  $\sim 14.65 \mu\text{W cm}^{-1} \text{K}^{-2}$  at room temperature [22]. Additionally, many post-treatment techniques have been used to further improve the TE performance of n-type  $\text{Bi}_2\text{Te}_3$  based f-TFs, such as heat treatment [23], laser treatment [24,25], infrared treatment [26], and electric current treatment [27].

Electric current treatment, as an effective and fast method, has attracted research interest [28]. Tan et al. [29] strengthened the anisotropy of electron mobility of  $\text{Bi}_2\text{Te}_3$  based thin films by introducing electric current during the deposition process, and achieved a high  $S^2\sigma$  of  $45 \mu\text{W cm}^{-1} \text{K}^{-2}$ . Zhu et al. [27] also used post-electric current treatment (P-ECT) methods to optimize phase transformations and crystal orientation of  $\text{Bi}_{0.5}\text{Sb}_{1.5}\text{Te}_3$  thin film, resulting in an increase in  $\sigma$ . It is typically understood that P-ECT can enhance the recrystallization kinetics, promote dislocation movement, and facilitate the formation of oriented microstructures in a short time [30,31]. It was worth mentioning that the thermal annealing effect is Joule thermal effect, and the athermal effect was mainly attributed to the electronic wind on atom diffusion [31]. Further research will analyze the effect of thermal effect and athermal effect on the doped  $\text{Bi}_2\text{Te}_3$  f-TFs, respectively.

In this study, the magnetron sputtering is combined with P-ECT to prepare n-type  $\text{Bi}_2\text{Te}_3$  f-TF on polyimide (PI) substrate (Figure 1a,b). Figure 1c shows an optical image of a typical n-type  $\text{Bi}_2\text{Te}_3$  f-TF. Through optimizing the P-ECT current, the increase of carrier concentration ( $n_e$ ) is achieved, leading to a high  $\sigma$  of  $\sim 2065 \text{ S cm}^{-1}$ . The corresponding  $S^2\sigma$  is  $\sim 10.70 \mu\text{W cm}^{-1} \text{K}^{-2}$ , which is comparable with the reported n-type  $\text{Bi}_2\text{Te}_3$  f-TF (Figure 1d). Applications of as-prepared n-type  $\text{Bi}_2\text{Te}_3$  f-TFs were investigated via an assembled TE device, which is composed of 4 n-type  $\text{Bi}_2\text{Te}_3$  legs. The device can generate the maximum open circuit voltage of  $\sim 7.96 \text{ mV}$  and the maximum output power of  $24.78 \text{ nW}$  at the temperature difference ( $\Delta T$ ) of  $\sim 35 \text{ K}$ .



**Figure 1.** Schematic diagram of: (a) magnetron sputtering, (b) electric current treatment, (c)  $\text{Bi}_2\text{Te}_3$  f-TF, (d) mechanically alloyed and dispenser printing (2012) [20]; screen print (2014) [32]; dispenser printing (2017) [21]; vacuum filtration and annealing (2019) [18]; in situ solution (2019) [33]; magnetron sputtering (2020) [34].

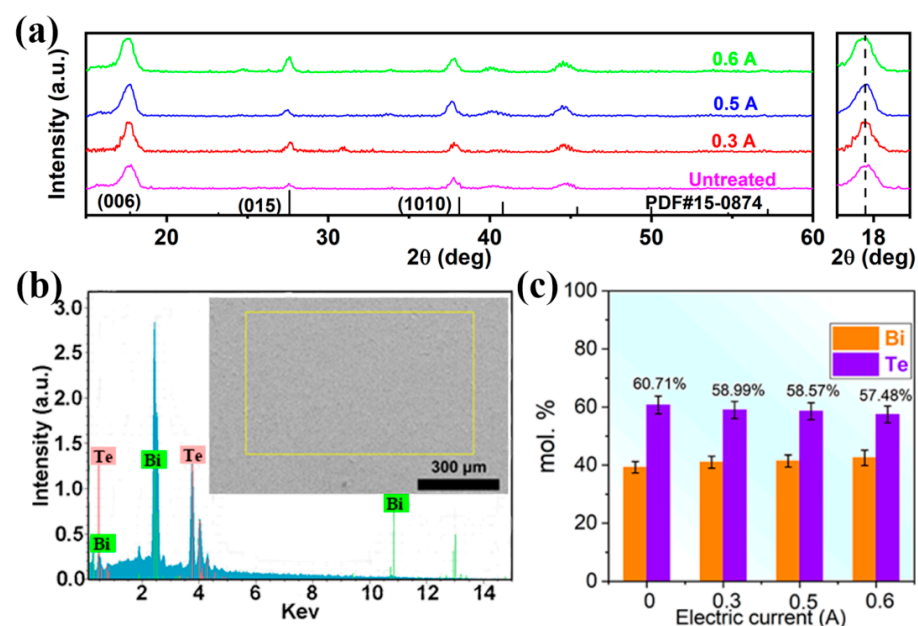
## 2. Experimental Section

The *n*-type Bi<sub>2</sub>Te<sub>3</sub> f-TFs were deposited on a flexible PI substrate using a magnetron sputtering method. The deposition parameters of the thin film are presented as follows: the working pressure of 1 Pa, radio frequency sputtering power of 50 W, the sputtering temperature of 573 K, the background vacuum of  $7.0 \times 10^{-4}$  Pa, and argon flow of 40 Scm. The KPS-3005D generator with the maximum output of 5.000 A was used to provide an electric pulse current. Bi<sub>2</sub>Te<sub>3</sub> f-TFs were post-treated by electric current with duration of 1 s and interval of 1 s. The electric current was set as 0.3 A, 0.5 A, and 0.6 A, respectively, and the electric current time was 10 min. The thickness range of the Bi<sub>2</sub>Te<sub>3</sub> f-TFs was ~580 nm. Finally, the flexible thermoelectric device was assembled with 4 *n*-type single-legs.

X-ray diffraction (XRD, D/max 2500 Rigaku Corporation, Tokyo, Japan, CuK $\alpha$  radiation) was employed to investigate the crystal structures of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs. SEM (Zeiss supra 55) was used to characterize the surface morphology. EDS (Bruker Quantax 200) was used to analyze the compositions of Bi<sub>2</sub>Te<sub>3</sub> f-TFs. Hall measurement system (HL5500PC, Nano metrics) was employed to record  $n_e$  and mobility ( $\mu$ ) values. A profilometer (Dektak XT, BRUKER, Germany) was employed to measure the thickness of flexible *n*-type Bi<sub>2</sub>Te<sub>3</sub> thin films. And  $\sigma$  and  $S$  were simultaneously measured by the SBA458 (Nezsch, Germany).

## 3. Results and Discussion

XRD patterns were employed to analyze the crystal structure of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs as shown in Figure 2a. As can be seen, all the diffraction peaks can be indexed as the Bi<sub>2</sub>Te<sub>3</sub> (PDF#15-0874), and no impurity peaks were observed. The right inset of Figure 2a shows the enlarged (006) peaks. The strongest peaks of all XRD patterns can be indexed as (006), indicating (00*l*) preferred orientation of all as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs. Figure S1 shows that no obvious crystallinity changes have been observed due to similar peak intensity and Full-Width Half-Maximum. Figure 2b shows a typical SEM-EDS pattern of Bi<sub>2</sub>Te<sub>3</sub> f-TFs treated under the electric current of 0.5 A. The chemical compositions of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs are shown in Figure 2c and Table 1. Before P-ECT, the as-deposited Bi<sub>2</sub>Te<sub>3</sub> f-TF presents the standard chemical stoichiometric ratio of ~2:3. With the increase of electric current, the Te content decreases due to the release of the unstable Te. With increasing the electric current from 0 to 0.6 A, the Bi content increases from 39.29 to 42.52 *at. %*, and Te content decreases from 60.71 to 57.48 *at. %*, indicating the increasing content of Te vacancies.

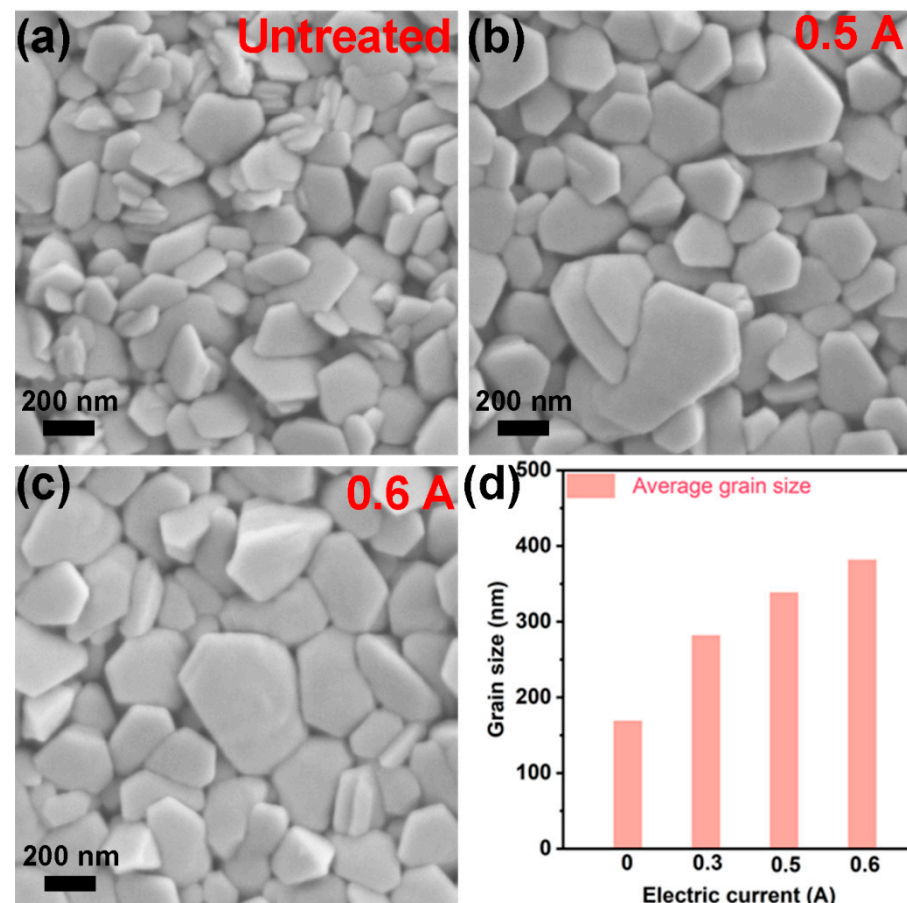


**Figure 2.** (a) XRD patterns of Bi<sub>2</sub>Te<sub>3</sub> f-TF fabricated under different electrical intensities. (b) The SEM-EDS pattern. (c) The pattern of chemical stoichiometric ratio of Bi<sub>2</sub>Te<sub>3</sub> f-TF.

**Table 1.** SEM-EDS results of Bi<sub>2</sub>Te<sub>3</sub> f-TF.

Electric Current	Thickness	Bi (at. %)	Te (at. %)
0 A	~580 nm ± 5 nm	39.29	60.71
0.3 A	~581 nm ± 5 nm	41.01	58.99
0.5 A	~583 nm ± 5 nm	41.43	58.57
0.6 A	~584 nm ± 5 nm	42.52	57.48

To characterize the morphology of Bi<sub>2</sub>Te<sub>3</sub> grains, the SEM images of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs treated under the electric current 0, 0.5, and 0.6 A are shown in Figure 3a–c, respectively. As can be seen, the as-prepared BT f-TFs are composed of hexagonal flakes stacking parallel to substrate. As the electric current increases from 0 A to 0.6 A, larger Bi<sub>2</sub>Te<sub>3</sub> grains can be observed. Figure 3d shows the average grain size of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TF as a function of electric current. With the increasing of the electric current from 0 to 0.6 A, the average grain size increased from ~168 to ~381 nm. Figure S2 compares the morphologies of as-prepared 0.6 A-Bi<sub>2</sub>Te<sub>3</sub> thin film before and after cycling measurement of TE performance, where no obvious difference has been observed, indicating excellent stability. The grain growth with increasing electric current can be attributed to the additional energy supply from post-electric treatment [28,30].



**Figure 3.** The SEM images of (a) untreated Bi<sub>2</sub>Te<sub>3</sub> f-TF; (b) 0.5 A-Bi<sub>2</sub>Te<sub>3</sub> f-TF; (c) 0.6 A-Bi<sub>2</sub>Te<sub>3</sub> f-TF. (d) The average grain size of Bi<sub>2</sub>Te<sub>3</sub> f-TF.

Room temperature TE performance of as-prepared Bi<sub>2</sub>Te<sub>3</sub> f-TFs is shown in Figure 4. Figure 4a shows the room temperature  $\sigma$ ,  $S$ , and  $S^2\sigma$  for Bi<sub>2</sub>Te<sub>3</sub> f-TF as a function of electric current. The  $\sigma$  increases from 1874 to 2240 S cm<sup>-1</sup> with increasing the electric current from 0 to 0.6 A, and the  $|S|$  decreases from 74 to 61  $\mu$ V K<sup>-1</sup>. To better understand the change of

$S$  and  $\sigma$ , the  $n_e$  was measured as shown in Figure 4b. The  $n_e$  increases from  $2.03 \times 10^{20}$  to  $3.84 \times 10^{20} \text{ cm}^{-3}$  with the increase of electric current. A simple relationship between  $n_e$  and  $S$  can be exhibited by Mott formula [35]:

$$S = \frac{8\pi^2 K_B^2 T}{3eh^2} m_{\text{DOS}}^* \left( \frac{\pi}{3n_e} \right)^{2/3} \quad (1)$$

where  $K_B$ ,  $e$ ,  $h$ , and  $m_{\text{DOS}}^*$  present Boltzmann constant, electron, Planck Constant, and, the density of state's effective mass, respectively. The reduced  $|S|$  is attributed to the increase of  $n_e$  according to their inverse relationship between  $S$  and  $n_e$  as expressed in Equation (1). Furthermore, according to the relationship between  $\sigma$  and  $n_e$  as expressed in formula  $\sigma = \mu n_e e$ , the increase of  $\sigma$  is mainly attributed to the increase of  $n_e$ . It is worth mentioning that the  $|S|$  of  $\text{Bi}_2\text{Te}_3$  f-TFs is still lower than that of bulk materials due to the high  $n_e > 1 \times 10^{20}$  (detailed discussion in Supplementary Materials). And the increased  $n_e$  should be mainly attributed to the increased amount of Te vacancies with increasing the electrical current. The room temperature  $S^2\sigma$  of  $\text{Bi}_2\text{Te}_3$  f-TF as a function of electric current is shown in Figure 4a. The maximum  $S^2\sigma$  of  $\sim 10.70 \mu\text{W cm}^{-1} \text{ K}^{-2}$  can be achieved mainly due to the high  $\sigma$  of  $\sim 2065 \text{ S cm}^{-1}$  and moderate  $S$  of  $-72 \mu\text{V K}^{-1}$ . The TE performance tests of the 0.5 A- $\text{Bi}_2\text{Te}_3$  f-TF were repeated 3 times to verify the stability of as-prepared  $\text{Bi}_2\text{Te}_3$  f-TFs as shown in Figure S3. Nearly unchanged TE performance during successive measurement cycles indicates high stability of our  $\text{Bi}_2\text{Te}_3$  f-TFs. Element-doped  $\text{Bi}_2\text{Te}_3$  based thin films usually have higher  $S^2\sigma$  [36–38], and further research will analyze the effect of the electric current treatment on the doped  $\text{Bi}_2\text{Te}_3$  f-TFs.

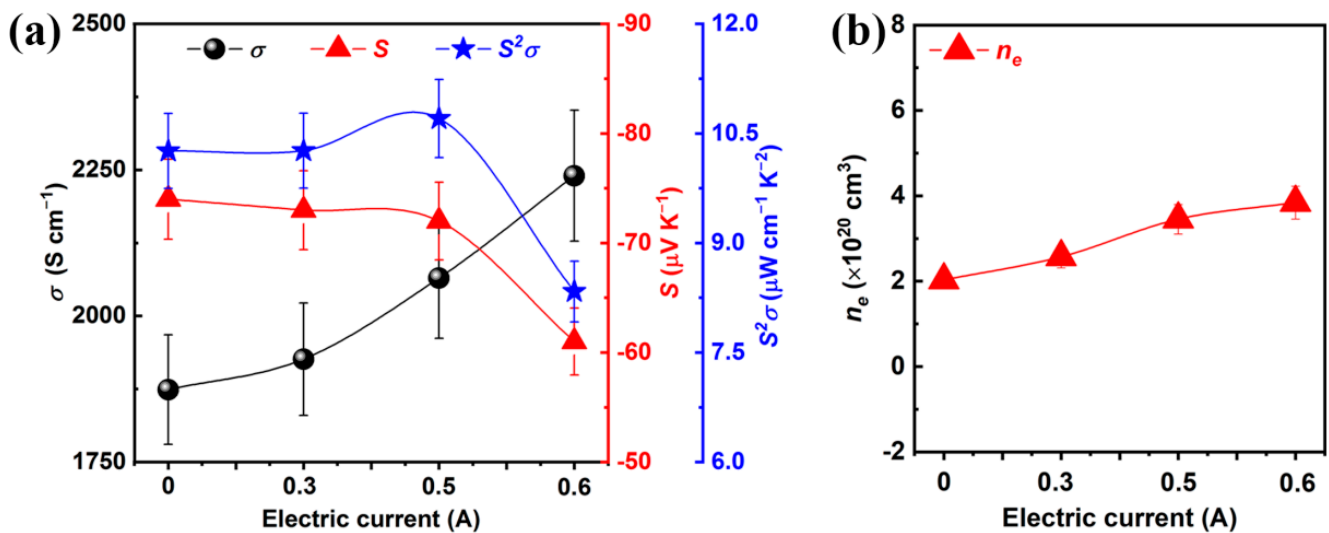
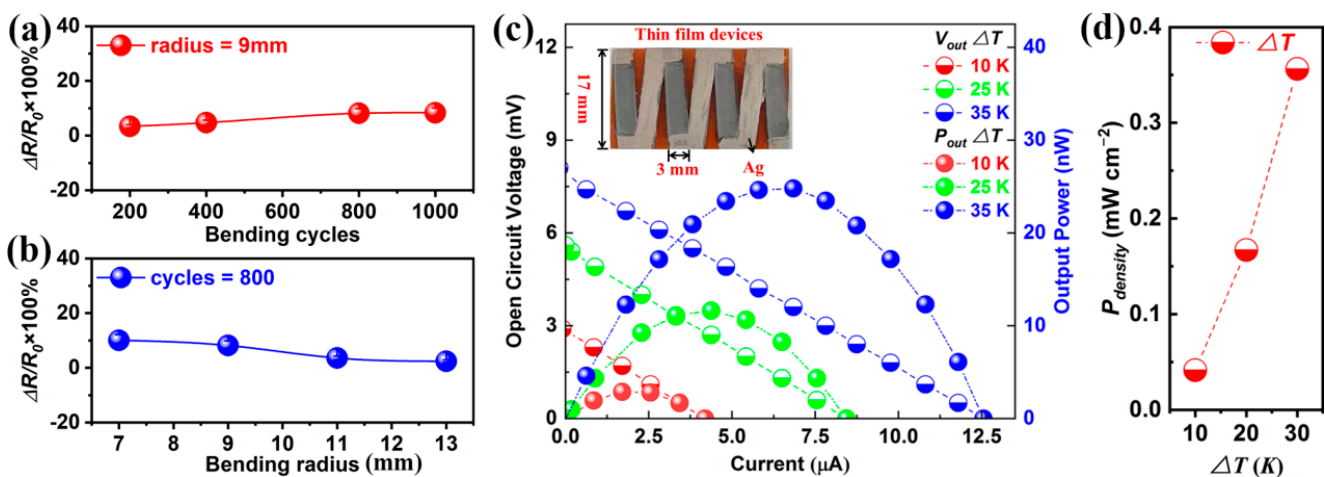


Figure 4. (a) The room temperature  $\sigma$ ,  $S$ , and  $S^2\sigma$  of  $\text{Bi}_2\text{Te}_3$  f-TF as a function of electric current. (b) Room temperature  $n_e$  of  $\text{Bi}_2\text{Te}_3$  f-TF as a function of electric current.

The bending tests were employed to investigate the bending resistance of as-prepared n-type  $\text{Bi}_2\text{Te}_3$  f-TFs. Figure 5a,b shows the change of relative resistance ( $\Delta R/R_0$ ) as a function of bending cycles and bending radius, respectively. With the increase of cycles from 200 to 1000 under the bending radius of 9 mm, the  $\Delta R/R_0$  increases from 3.39% to 8.34% as shown in Figure 5a. In addition, with the increase of bending radius from 7 mm to 13 mm, the  $\Delta R/R_0$  decreases from 9.98% to 2.41% as shown in Figure 5b. The  $\Delta R/R_0 < 10\%$  suggests that the  $\text{Bi}_2\text{Te}_3$  f-TFs possess excellent bending resistance [22,39]. Figure S4 shows the repetitive test result of the bending resistance before and after cycling TE performance measurement, where high mechanical stability has been demonstrated. To demonstrate the practical applicability of  $\text{Bi}_2\text{Te}_3$  f-TFs, a flexible TE device assembled of 4  $\text{Bi}_2\text{Te}_3$  legs (treated under the electric current of 0.5 A) was fabricated as schematically shown in the



inset of Figure 5c. And Figure 5c shows the open circuit voltage and output power as a function of electric current at the temperature difference ( $\Delta T$ ) ranging from 10 to 35 K. And a high temperature difference can be easily maintained between hot and cold side of thin films devices due to the polyimide substrate ( $\kappa < 1 \text{ W m}^{-1} \text{ K}^{-1}$ ) [40]. As can be seen, the maximum open circuit voltage of  $\sim 7.96 \text{ mV}$  can be achieved with the corresponding output power of  $24.78 \text{ nW}$  at  $\Delta T$  of 35 K. The performance of the flexible TE device can be evaluated by power density  $P_{density}$  ( $P_{density} = P_{max} / w \cdot h$ , where  $w$  and  $h$  represent the width and height, respectively) [40,41]. Figure 5d shows that the  $P_{density}$  of the flexible TE device is  $0.04 \text{ mW cm}^{-2}$ ,  $0.17 \text{ mW cm}^{-2}$  and  $0.36 \text{ mW cm}^{-2}$ , corresponding to the  $\Delta T$  of 10, 20 and 30 K, respectively.



**Figure 5.** (a) The  $\Delta R/R_0$  as a function of bending cycles at bending radius of 9 mm. (b) The  $\Delta R/R_0$  as a function of bending radius at bending cycle of 800. (c) Open circuit voltage and output power as a function of electric current at different  $\Delta T$ . (d) The power density as a function of  $\Delta T$ .

#### 4. Conclusions

In conclusion, we have successfully improved n-type  $\text{Bi}_2\text{Te}_3$  f-TFs by P-ECT. It is found that, with the increase of electric current, the  $n_e$  increases and  $\sigma$  increases from  $1874$  to  $2240 \text{ S cm}^{-1}$ . Consequently, the high  $S^2\sigma$  of the  $\text{Bi}_2\text{Te}_3$  f-TFs treated by  $0.5 \text{ A}$  achieves  $\sim 10.70 \text{ } \mu\text{W cm}^{-1} \text{ K}^{-2}$  at room temperature, which is competitive among the reported n-type  $\text{Bi}_2\text{Te}_3$  f-TFs. Besides, a small  $\Delta R/R_0 < 10\%$  is achieved after bending test, suggesting high bending resistance of our prepared  $\text{Bi}_2\text{Te}_3$  f-TFs. Subsequently, a flexible TE device composed of 4 n-type single legs generates an open circuit voltage of  $\sim 7.96 \text{ mV}$  and an output power is  $24.78 \text{ nW}$  at  $\Delta T$  of  $\sim 35 \text{ K}$ . Our work demonstrates that P-ECT method can effectively further improve the electrical performance of  $\text{Bi}_2\text{Te}_3$  f-TFs.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/mi13091544/s1>, Fgiure S1: Calculated crystallinity of 0.5 A-Bi<sub>2</sub>Te<sub>3</sub> f-TF; Fgiure S2: (a) The SEM; Figure S3: The repetitive test of TE performance of the 0.5 A-Bi<sub>2</sub>Te<sub>3</sub> thin film; Fgiure S4: (a,b) The repetitive test result of the bending resistance of 0.5 A-Bi<sub>2</sub>Te<sub>3</sub> thin film at bending radius of 9 mm and bending cycle of 800, respectively. References [42,43] are cited in the Supplementary Materials.

**Author Contributions:** D.A.: Investigation, Conceptualization, Methodology, Formal analysis, writing—original draft. W.-D.L.: Conceptualization, Project administration, Formal analysis, writing—original draft. F.M.: Investigation, Data curation, Validation. W.B.: writing—review & editing. Y.C.: writing—review & editing. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** The processed data required to reproduce these findings cannot be shared at this time as the data also forms part of an ongoing study.

**Conflicts of Interest:** The authors declare no conflict of interest.

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