

Article

Improvement of Single Event Transient Effects for a Novel AlGaN/GaN High Electron-Mobility Transistor with a P-GaN Buried Layer and a Locally Doped Barrier Layer

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Abstract: In this paper, a novel AlGaN/GaN HEMT structure with a P-GaN buried layer in the buffer layer and a locally doped barrier layer under the gate (PN-HEMT) is proposed to enhance its resistance to single event transient (SET) effects while also overcoming the degradation of other characteristics. The device operation mechanism and characteristics are investigated by TCAD simulation. The results show that the peak electric field and impact ionization at the gate edges are reduced in the PN-HEMT due to the introduced P-GaN buried layer in the buffer layer. This leads to a decrease in the peak drain current (*I*_{peak}) induced by the SET effect and an improvement in the breakdown voltage (BV). Additionally, the locally doped barrier layer provides extra electrons to the channel, resulting in higher saturated drain current (*I*D,sat) and maximum transconductance (*g*max). The *I*_{peak} of the PN-HEMT (1.37 A/mm) is 71.8% lower than that of the conventional AlGaN/GaN HEMT (C-HEMT) (4.85 A/mm) at 0.6 pC/ μ m. Simultaneously, $I_{D, sat}$ and BV are increased by 21.2% and 63.9%, respectively. Therefore, the PN-HEMT enhances the hardened SET effect of the device without sacrificing other key characteristics of the AlGaN/GaN HEMT.

Keywords: GaN HEMT; single event transient (SET) effect; P-GaN buried layer; locally doped barrier layer

1. Introduction

In recent years, high electron-mobility transistors (HEMTs) based on GaN/AlGaN heterostructures have made significant progress due to their excellent material properties, including high electron mobility, a high electric field strength, a wide bandgap, and more [\[1–](#page-7-0)[4\]](#page-7-1). With the continuous improvement of microelectronics fabrication techniques, the current gain cutoff frequency (f_T) and maximum oscillation frequency (f_{max}) of GaN HEMTs have greatly increased [\[5–](#page-8-0)[7\]](#page-8-1), making them highly suitable for aerospace and satellite power applications [\[8](#page-8-2)[–10\]](#page-8-3).

When GaN HEMTs are used in space equipment, their operating characteristics can be limited by irradiation effects. One of the most common radiation effects is the single event transient (SET) effect caused by high-energy heavy ions in space [\[11](#page-8-4)[–13\]](#page-8-5), which can alter the operating state of the device and even lead to permanent damage. To date, the SET effects in GaN HEMTs have been extensively studied by many researchers [\[14](#page-8-6)[–17\]](#page-8-7). The high impact ionization rate in the high electric field region of GaN HEMTs results in the generation of more electron–hole pairs, leading to a significant increase in electron collection by the drain electrode and, consequently, increased sensitivity to SET effects [\[18,](#page-8-8)[19\]](#page-8-9). Therefore, one method to improve the radiation hardness of GaN HEMTs against SET effects is to reduce

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the electric field. To modulate the electric field distribution, a gate field plate is commonly utilized [\[20–](#page-8-10)[22\]](#page-8-11). However, the field plate will induce additional parasitic gate capacitance, decaying the f_T and f_{max} of the device. Introducing a P-type buried layer structure is an effective method to modulate the channel electric field and has been reported by many encenve method to modulate the channel electric herd and has been reported by many
researchers [\[23](#page-8-12)[–26\]](#page-8-13). A dual-channel P-type buried layer has been used to decrease the electric field near the drain channel, resulting in an increase in single-event burnout voltage for GaN MISFETs [27]. However, the P-type buried layer reduces the electron concentration in the channel, leading to the degradation of GaN HEMT characteristics. Therefore, a method that reduces the sensitivity of the device to SET effects without sacrificing other characteristics is needed.

characteristics is needed.
In this work, to enhance the SET hardening and DC characteristics of GaN HEMTs, in this work, to challing the *SET* randering that *DC* characteristics of Sat Criminis,
a novel HEMT with a p-GaN buried layer in the buffer layer and a locally doped barrier layer under the gate (PN-HEMT) is proposed and investigated by TCAD simulation. It was observed that the peak drain current (*I*_{peak}) induced by the SET effect in the PN-HEMT is significantly decreased due to the P-GaN buried layer. The $I_{\rm peak}$ of the PN-HEMT is 71.8% lower than that of the conventional HEMT (C-HEMT). Furthermore, it was found that the saturated drain current (*I_{D,sat}*) of the PN-HEMT is slightly increased by 21.2% compared with that of the C-HEMT, due to the locally doped barrier layer.

2. Device Structure and Simulation Details

 $\mathbf{f}(\mathbf{f}) = \mathbf{f}(\mathbf{f})$ shows the structure of the PN-HEMT. A p-GaN buried layer in the buffer in the buffer

Figure 1a shows the structure of the PN-HEMT. A P-GaN buried layer in the buffer layer and a locally doped barrier layer under the gate are the notable features of the piezo-PN-HEMT. The simulations are carried out in Sentaurus TCAD [\[28\]](#page-8-15), and physics models FIVENT. The simulations are carried out in Semantius Terric $[20]$, and physics models are introduced, such as the DopingDep and High-field dependent mobility model, the piezoelectric polarization (strain) model, the impact ionization model, and the Schockley– Read-Hall recombination model. The length and thickness of locally doped $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ barrier are 2.1 µm and 20 nm, respectively. The doping concentration of the locally doped Al_{0.3}Ga_{0.7}N barrier is 1 × 10¹⁸ cm⁻³. The distance from the P-GaN buried layer to the GaN channel (D) is 50 nm and the thickness of the P-GaN buried layer is 0.1 μ m. The doping channel (D) is 50 fun and the thickness of the P-GaN buried layer is 0.1 µm. The doping concentration of the P-GaN buried layer is 7×10^{17} cm⁻³. Figure [1b](#page-1-0) shows the structure of the C-HEMT. The work function of gate is set as 5.2 eV to model the Ni/Au Schottky contact of the actual device [\[29\]](#page-8-16). The other parameters are shown in Table [1.](#page-2-0)

Figure 1. Schematic cross-section of (a) PN-HEMT and (b) C-HEMT.

Table 1. Parameters of the PN-HEMT in simulation. **Parameter Value** α and α is α in a summation.

Table 1. Parameters of the PN-HEMT in simulation.

To investigate the SET performance of the devices, the HeavyIon model is adopted. Under the harshest conditions, the incidence position of the particle is set at the gate edge closest to the drain $[19,26]$ $[19,26]$, with the particle traveling vertically across the device. After the particle strike, the generation rate of electron–hole pairs is described by a spatial and temporal Gaussian function, which is expressed as follows [\[30,](#page-8-17)[31\]](#page-9-0):
 $IET \qquad \qquad [(x - x_0)^2] \qquad \qquad [(t - T_0)^2]$

$$
rate(x,t) = \frac{LET}{q\pi\omega_0 T_C} \exp\left[-\frac{(x-x_0)^2}{\omega_0^2}\right] \cdot \exp\left[-\frac{(t-T_0)^2}{T_C^2}\right]
$$
(1)

where the spatial Gaussian function width ω_0 and the temporal Gaussian function width T_C are set as 0.06 μ m and 5×10^{-12} s, respectively. The initial time T_0 of the charge generation is set to 2 × 10⁻¹¹ s. The LET value in simulation is 0.6 pC/ μ m, which corresponds to 63.8 MeV \cdot cm²/mg for Ta [\[32\]](#page-9-1), with a conversion factor of 0.0095 [\[33\]](#page-9-2).

3. Results and Discussion *3.1. Basic Characteristics*

3.1. Basic Characteristics

Figure [2](#page-2-1) illustrates the DC characteristics of the PN-HEMT, C-HEMT, N-HEMT (with The results are be entired the results of the FN TEMT, C TEMT, IN TEMT (with only the locally doped barrier layer), and P-HEMT (with only the P-GaN buried layer). The results show that a much higher saturated drain current (*I_{D,sat}*) and maximum transconducted for the N-HEMT and PN-HEMT. tance (g_{max}) are achieved for the N-HEMT and PN-HEMT. This improvement is attributed to the locally doped barrier layer in the proposed structures. In the PN-HEMT and Nthe locally doped barrier layer provides additional electrons to the channel, thereby HEMT, the locally doped barrier layer provides additional electrons to the channel, thereby enhancing electron density from the *x*-coordinate at the gate's right-side edge to the locally doped barrier's right-side edge [\[34\]](#page-9-3), as shown in the dashed pink box in Figure [3.](#page-3-0) Consequently, a much higher *I_{D,sat}* is observed for the N-HEMT and PN-HEMT. Moreover, the lowest *I*_{D,sat} is observed in the P-HEMT, as the buried P-GaN island partially depletes the 2DEG. Compared to the *I*_{D,sat} and g_{max} of 591 mA/mm and 254 mS/mm in the C-HEMT, a higher *I*_{D,sat} of 716 mA/mm and g_{max} of 267 mS/mm are achieved in the PN-HEMT. $\frac{1}{2}$ to the local doped barrier layer layer in the proposed structure of $\frac{1}{2}$ and $\frac{1}{2}$ the interaction on the proposed structure of $\frac{1}{2}$ and $\frac{1}{2}$ the interaction on the proposed structure of $\frac{1$

Figure 2. (**a**) Output and (**b**) transfer characteristics for different devices.

Figure 3. Electron concentration along the channel for different devices. **Figure 3.** Electron concentration along the channel for different devices.

Figure 2. (**a**) Output and (**b**) transfer characteristics for different devices.

breakdown voltage (BV) is extracted from the *I_{DS}*−*V_{DS}* curve when $I_{DS} = 1$ mA/mm. Compared to the ^{BV} of 289 V in the C-HEMT, a higher BV of 800 V is achieved by the proposed PN-HEMT. Figure 4b,c show the distribution of equipotential lines for the PN-HEMT and C-HEMT at breakdown. As shown in Figure [4b](#page-3-1), the equipotential lines are more field of the P−GaN buried layer [\[35](#page-9-4)[,36\]](#page-9-5). However, the equipotential lines for the C-HEMT are more crowded near the gate. Additionally, the buffer leakage current is reduced by the P−GaN buried layer, further increasing the BV. Consequently, the PN-HEMT achieves a more crowded near the gate crowded near the gate. Additionally, the buffer leakage current is reduced by the buffer leakage current is reduced by the buffer leakage current is reduced by the buffer leakage current is reduc Figure [4a](#page-3-1) compares the I−V characteristics of the PN-HEMT and C-HEMT. The uniformly distributed between the gate and drain owing to the redistribution of the electric higher BV.

Figure 4. (**a**) I–V characteristics curves and (**b**,**c**) distribution of equipotential lines at breakdown.

3.2. SET Effect

 $F(4.85 \text{ A/mm})$. Additionally, the drain current pulse duration of the PN-HEMT is shorter
the attack of the GLUNAT Therefore, the PNLUEMT day are taken a work help a solitance down. to the SET effect compared to the C-HEMT.The variations in *I*_{DS} over time for the PN-HEMT and C-HEMT after a particle strike at V_{DS} = 50 V and V_{GS} = −6 V (off state) are shown in Figure [5.](#page-4-0) After the particle strike, the *I*_{DS} for both devices initially increase rapidly and reach their peaks (*I*_{peak}), then quickly decrease. The *I*_{peak} of the PN-HEMT (1.37 A/mm) is 71.8% lower than that of the C-HEMT than that of the C-HEMT. Therefore, the PN-HEMT demonstrates a much better resistance

Figure 5. Drain currents as a function of time after heavy ion strike (V_{DS} = 50 V and V_{GS} = -6 V).

for the PN-HEMT and C-HEMT at peak time is analyzed, as shown in Figure 6a. It can be seen that, due to the P-GaN buried layer depleting electrons in the channel between and buried in the P-GaN buried is a noncentration from the channel between the addition, the effect on electron concentration from the locally doped barrier layer under the gate is minimal. However, the electron density remains high in the C-HEMT. To further elucidate the low electron concentration in the PN-HEMT, the impact ionization rate (IR) for [th](#page-4-1)e PN-HEMT and C-HEMT at peak time is analyzed, as shown in Figure 6b. The PN-HEMT is smaller than that of the C-HEMT. This is mainly due to the lower electric field
PN-HEMT is smaller than that of the C-HEMT. This is mainly due to the lower electric field FOR FIGURE AND C-HEMT AND C-HEMT AND C-HEMT AND C-HEMT and C-HEMEL SURVEY SECURE FIGURE AND along the particle incident path in the PN-HEMT, as shown in Figure [7,](#page-5-0) which suppresses electron-hole pair ionization. Hence, fewer electrons are generated in the PN-HEMT at peak time, resulting in a significantly lower *I*_{peak}. To explain the lower I_{peak} for the PN-HEMT, the electron density in the channel (BB') the gate and drain in the PN-HEMT, there is a noticeable reduction in electron density. In results show that the IR at the AlGaN barrier (AA') and GaN channel (BB') interface for the

for PN-HEMT and C-HEMT at peak time. **Figure 6.** (**a**) Channel electron density distribution (along the line BB') and (**b**) impact ionization rate

Figure 7. Electric field distribution (along the line BB') at peak time. **Figure 7.** Electric field distribution (along the line BB') at peak time.

drain electrode. Consequently, the *I*_{peak} of the PN-HEMT is further decreased. **@***V***DS = [50V](#page-5-1),** *V***GS =** −**6V** in Figure 8, resulting in more electrons being recombined before they are collected by the In addition, the P-GaN buried layer increases the SRH recombination rate, as shown *x* **x x x x x**

Figure 8. SRH recombination rate at peak time for (a) PN-HEMT and (b) C-HEMT.

The influences of *D* and N_P on the I_{peak} of the PN-HEMT at $T = 0.05 \mu m$ are shown in Figure [9a](#page-6-0). The results indicate that the I_{peak} of the PN-HEMT decreases to a minimum and then increases again with the increase in D and N_P . Figure 9b shows the effects of T on the I_{peak} . As T increases, the I_{peak} initially decreases and then increases. This is mainly due to the higher electric field that is obtained with the thicker T , as shown in Figure [10.](#page-6-1)
Channel in the destrie field in the derive have a increasing of the field on the IP. Therefore, the IR is higher for the thicker *T*, as shown in Figure [11,](#page-6-2) and therefore more electron-hole pairs will be generated at a thicker T, resulting in a higher I_{peak} . When N_P is $7 \times 10^{17} \text{ cm}^{-3}$, T is 0.1 μ m, and D is 0.05 μ m, the I_{peak} of the PN-HEMT reaches its lowest value (1.37 A/mm). Simultaneously, $I_{D, \text{sat}}$ and BV are increased by 21.2% and 63.9%, respectively. Therefore, the PN-HEMT enhances the device's resistance to SET effects without sacrificing other key
characteristics of the CaN HEMT Simultaneously, *I*D,sat and BV are increased by 21.2% and 63.9%, respectively. Therefore, Changes in the electric field in the device have an important effect on the IR. Therefore, the characteristics of the GaN HEMT.

characteristics of the GaN HEMT. The GaN HEMT Construction of the GaN HEMT.

Figure 10. Electric field distribution for different T at peak time.

Figure 11. Impact ionization rate for PN-HEMT with different T at peak time.

steps start with epitaxially growing GaN buffer and P-GaN layers on a Si substrate by MOCVD in Figure [12a](#page-7-2). The realization of an epitaxial P-GaN layer could be achieved by using Mg as dopant. The P-GaN layer is selectively etched by ICP until the GaN buffer is exposed, as shown in Figure [12b](#page-7-2), and, then, surface treatment is used to improve the surface quality [\[37\]](#page-9-6). The GaN buffer/GaN channel/AlGaN/N⁺-AlGaN are regrown by MOCVD, as shown in Figure [12c](#page-7-2) [\[38\]](#page-9-7). The ICP is utilized to selectively etch N+-AlGaN until the AlGaN layer is exposed, as shown in Figure [12d](#page-7-2), which is followed by surface treatment. Subsequently, the regrowth of the AlGaN layer is achieved by MOCVD and a SiN_x passivation layer is formed by LPCVD, as shown in Figure [12e](#page-7-2). Afterwards, digital etching is used to form the source and drain trenches, as shown in Figure [12f](#page-7-2). Figure 12 illustrates the key feasible fabrication process flows for the PN-HEMT. The Figure [12](#page-7-2) illustrates the key feasible fabrication process flows for the PN-HEMT. The

The Ti/Al/Ni/Au stack is deposited with a low-temperature Ohmic process and lift-off for source and drain electrode are performed, as shown in Figure [12g](#page-7-2). Finally, the gate electrode is formed by e-beam evaporation after selectively removing SiN_x by RIE, and is then lifted off, as shown in Figure [12h](#page-7-2).

Figure 12. Key fabrication process steps for PN-HEMT. **Figure 12.** Key fabrication process steps for PN-HEMT.

4. Conclusions

4. Conclusions In this paper, a novel HEMT with a P-GaN buried layer in the buffer layer and a locally doped barrier layer under the gate is proposed to enhance resistance to SET effects. The results show that the *I*_{peak} of the PN-HEMT is significantly decreased due to the reduction
in the *E*_T effects. In lay the *D.C.M* having large and its the PM is the increased. In addition The *IPeak* and IN *I_J* and I can Vented myer, while the *IV* is also improved. In dualities, the locally doped barrier layer provides extra electrons to the channel, enhancing electron density, resulting in a much higher *I_{D,sat}* for the PN-HEMT. Consequently, compared to the I_{peak} of 4.85 A/mm in the C-HEMT, the novel PN-HEMT achieves an I_{peak} of 1.37 A/mm, a reduction of 71.8%. The *I*_{D,sat} and BV of the PN-HEMT are increased to 716 mA/mm and 800 V, respectively, from 591 mA/mm and 289 V in the C-HEMT, representing increases of 21.2% and 63.9%, respectively. in the *E*peak and IR by the P-GaN buried layer, while the BV is also improved. In addition,

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