

Supplementary Information

Kinetics and mechanisms of Cr(VI) Removal by nZVI:

Influencing parameters and modification

Submitted to

Catalysts

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Text S1.

1. The reduction rates of nZVI for Cr(VI) reduction were obtained by following formula [1]:

$$\text{Cr removal efficiency (\%)} = \frac{C_0 - C_t}{C_0} \times 100\%$$

C_0 : is the initial Cr(VI) concentration in the solution;

C_t : the concentration of Cr(VI) in the solution at min.

2. The kinetic equation for the removal of Cr (VI) by nZVI was as follows:

first-order [2]: $\ln C = k_1 t + C_0$

second-order [3]: $1/C = k_2 t + C_1$

pseudo-first-order [4]: $\ln(q_e - q_t) = k_3 t + C_2$

pseudo-second-order [5]: $t/q_t = k_4 t + C_3$

C : the concentration of Cr(VI) in the solution at min.

3. The Langmuir and Freundlich isotherm models can be represented as follows:

Langmuir [6]: $q = kc^{1/n}$

Freundlich [7]: $q = q_e * bc / (1 + bc)$

q : adsorption capacity at different time ($\text{mg} \cdot \text{g}^{-1}$)

4. Intraparticle [8]: $q_t = k * t^{0.5} + C$

5. Formula for calculating adsorption capacity [9]: $q = \frac{v(c_0 - c)}{m}$

q : Adsorption capacity at adsorption equilibrium, mg/g ;

V : Solution volume, L;

C_0 : Initial concentration of solution, mg/L ;

C : The concentration of solution at adsorption equilibrium at min, mg/L ;

Q_t : adsorption capacity of solution at adsorption equilibrium at min, mg/g ;

Q_e : maximum adsorption capacity, mg/g .

Table S1. The EDS results of pre- and post-reaction of Cr(VI) with nZVI.

	Element	unn. C	norm. C	Atom. C	Error (3 Sigma)
		[wt.%]	[wt.%]	[at.%]	[wt.%]
pre-reaction	Iron	74.01	95.16	84.92	6.03
	Oxygen	3.77	4.84	15.08	2.10
	Gold	0.00	0.00	0.00	0.00
	Total:	77.78	100.00	100.00	
post-reaction	Iron	69.72	70.93	42.04	5.67
	Oxygen	27.07	27.54	56.99	10.20
	Chromium	1.50	1.53	0.97	0.23
	Gold	0.00	0.00	0.00	0.00
	Total:	98.29	100.00	100.00	

Table S2. Comparison of R^2 values fitted by various kinetic models at different temperatures.

	First order	Second order	Pseudo-first order	Pseudo-second order
293K	$\text{Ln}C = 0.031t + 2.93$ $R^2 = 0.7075$	$1/C = 0.0001t + 0.054$ $R^2 = 0.6673$	$\text{Ln}(Q_e - Q_t) = 0.0195t + 2.85$ $R^2 = 0.8123$	$t/Q_t = 0.019t + 0.075$ $R^2 = 0.9998$
303K	$\text{Ln}C = 0.0109t + 2.29$ $R^2 = 0.2352$	$1/C = -0.0002t + 0.053$ $R^2 = 0.5492$	$\text{Ln}(Q_e - Q_t) = 0.0361t + 0.068$ $R^2 = 0.6822$	$t/Q_t = 0.01972t + 0.049$ $R^2 = 0.9997$
313K	$\text{Ln}C = 0.0033t + 2.89$ $R^2 = 0.6809$	$1/C = -9E-0.5t + 0.050$ $R^2 = 0.9122$	$\text{Ln}(Q_e - Q_t) = -0.0407t + 3.63$ $R^2 = 0.8307$	$t/Q_t = 0.019t + 0.097$ $R^2 = 0.9983$

Table S3. Comparison of R^2 values fitted by isothermal adsorption model.

T (K)	Langmuir			Freundlich		
	Q_m (mg/g)	K_L (L/mg)	R^2	$n/1$	K_F	R^2
293	57.077	1.46	0.9719	0.4329	25.11	0.9017

Table S4. Intraparticle diffusion coefficients and intercept values for Cr(VI)

adsorption on nZVI particles at different temperatures.

Step.1

Temperature (K)	K ($\text{mg}\cdot\text{g}^{-1}\cdot\text{h}^{0.5}$)	Intercept values (C)	R ²
293 K	10.67	2.62	0.92
303 K	11.48	2.25	0.93
313 K	10.98	1.75	0.95

Step.2

Temperature (K)	K ($\text{mg}\cdot\text{g}^{-1}\cdot\text{h}^{0.5}$)	Intercept values (C)	R ²
293 K	37.82	1.39	1
303 K	41.49	0.98	1
313 K	32.85	1.71	1

Step.3

Temperature (K)	K ($\text{mg}\cdot\text{g}^{-1}\cdot\text{h}^{0.5}$)	Intercept values (C)	R ²
293 K	50	-8.95E-15	1
303 K	45.38	0.207	1
313 K	47.26	0.441	1

Table S5. Comparison of the Cr(VI) removal efficiency of nZVI and other related materials

Sorbent	pH	Adsorption rate (mg/g/h)	Adsorption capacity (mg/g)
nano-magnetite[10]	6.0	3.7	1.5
Fe ₃ O ₄ @poly(m-phenylenediamine) particle[11]	2.0	49.2	246.0
Magnetite[12]	2.0	7.5	12.5
liquid nitrogen treated zero-valent iron[13]	6.3	0.4	0.4
graphene oxide hydrogel with shrimp shell magnetic biochar[14]	1.0	28.6	85.9
ball milling synthesized FeS ₂ @biochar composite[15]	3.0	57.5	134.0
nZVI	3.0	25.0	50.0
H ₂ A-nZVI	3.0	66.7	50.0
Starch-nZVI	3.0	200.0	50.0
Fe-Cu	3.0	100.0	50.0

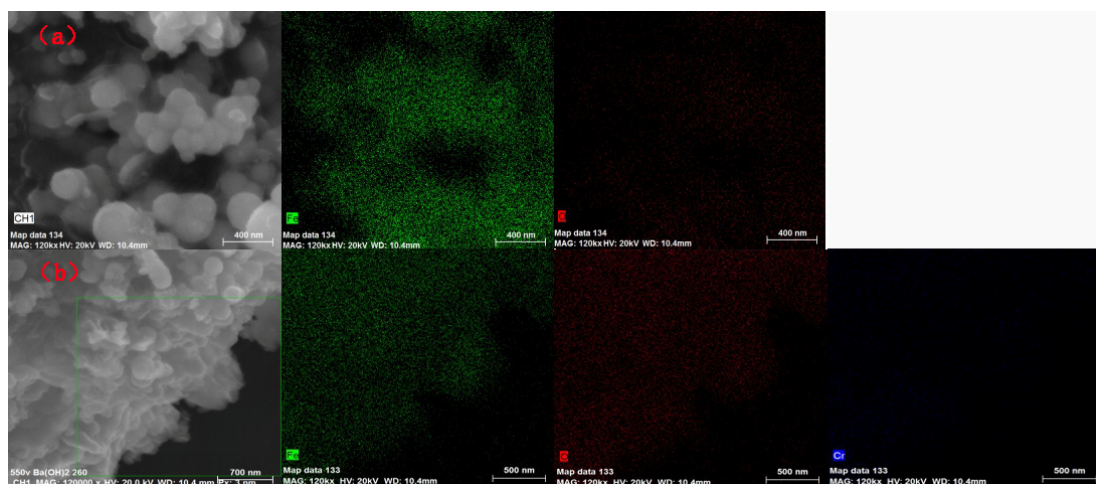


Figure S1. The EDS results of pre- (a) and post- (b) reaction of Cr(VI) with nZVI.

$$([\text{Cr(VI)}] = 25 \text{ mg/L}, [\text{nZVI}] = 0.5 \text{ g/L}, \text{pH} = 3, T = 293 \text{ K})$$

It can be seen from the Figure S1 that the content of Fe before the reaction is obviously higher than that after the reaction, while the content of O before the reaction is obviously lower than that after the reaction, which further proves that O participates in the removal of Cr(VI).

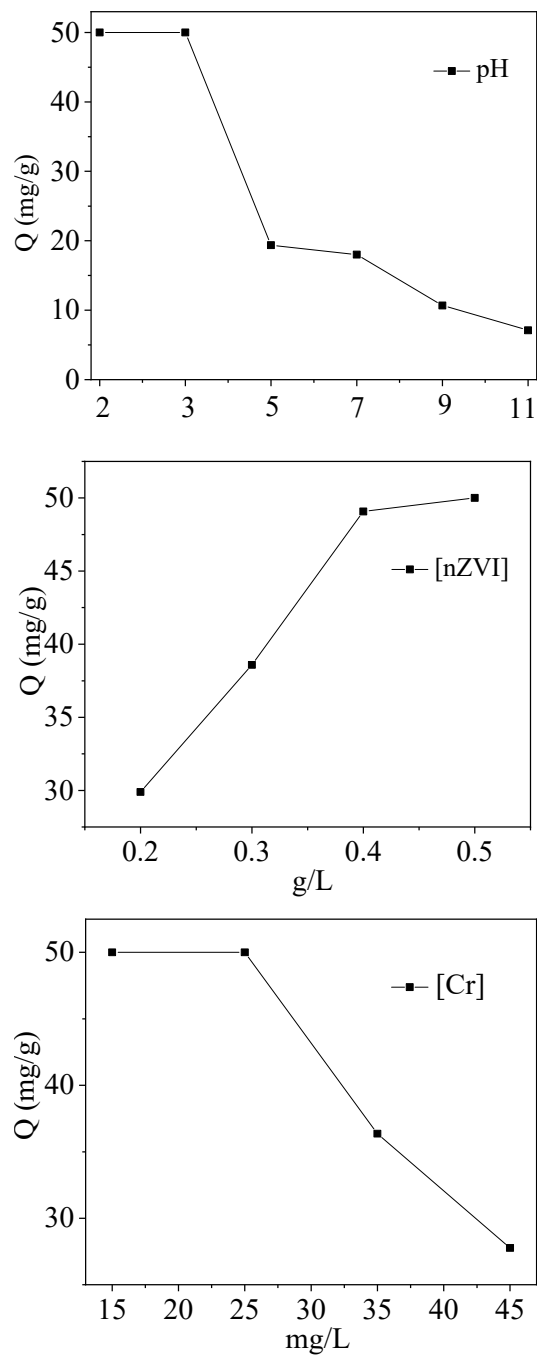


Figure S2. Changes of adsorption capacity with pH, initial concentration of Cr(VI) and dosage of nZVI.

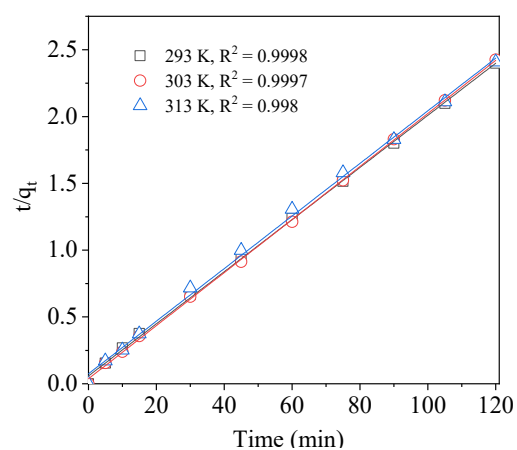


Figure S3. Pseudo-second-order kinetic fitting curve of Cr(VI) removal by nZVI.

([Cr(VI)] = 25 mg/L, [nZVI] = 0.5 g/L, pH = 3, T = 120 min)

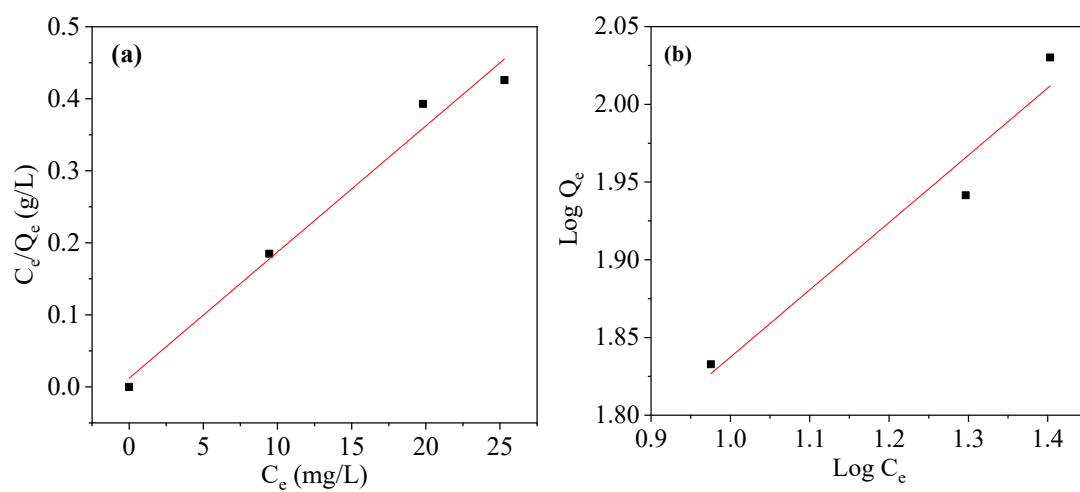


Figure S4. Fitting results of isotherm adsorption model (a: Langmuir; b: Freundlich).

([nZVI] = 0.5 g/L, pH = 3, T = 293 K)

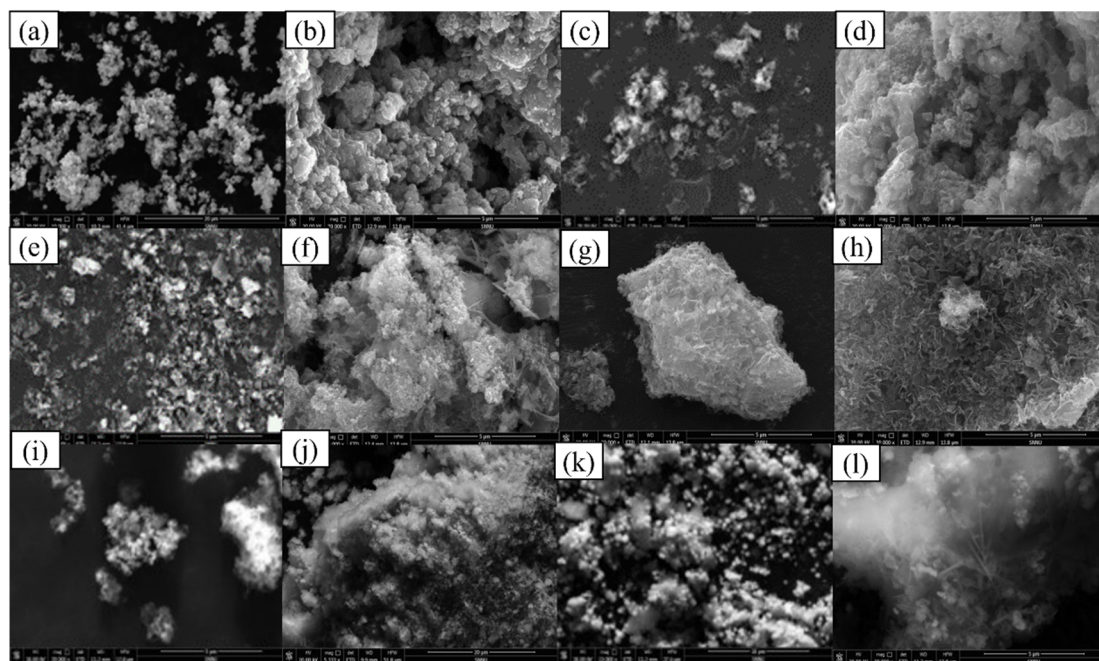


Figure S5. The SEM results of pre- and post- reaction of Cr(VI) with supported nZVI [(a,b) H₂A-nZVI; (c,d) Starch-nZVI; (e,f) Fe-Cu; (g,h) CMC-nZVI; (i,j) Fe-Zn; (k,l) Fe-Mn].

([Cr(VI)] = 25 mg/L, [nZVI] = 0.5 g/L, pH = 3, T = 293 K)

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