

Supplementary Information

1. NH₃ Amount Added in Urea SCR Mixture ($t_R = 4.0$ s)

These tests were performed with the aim to compensate the decrease of the NO_x conversion in urea-SCR with $t_R = 4.0$ s.

Table S1. NO_x conversion in urea-SCR and NH₃-SCR depending on the experimental condition.

| Temp. (°C) | NO _x Conv. (%) in NH ₃ -SCR | NO _x Conv. (%) in Urea-SCR ($t_R = 5.2$ s) | NO _x Conv. (%) in Urea-SCR ($t_R = 4.0$ s) | NH ₃ Added (ppm) in Urea-SCR ($t_R = 4.0$ s) | NO _x Conv. (%) in Urea-SCR ($t_R = 4.0$ s) with Added NH ₃ |
|------------|---|--|--|--|---|
| 200 | 48 | 43 | 25 | 80 | 46 |
| 250 | 74 | 70 | 37 | 135 | 73 |
| 300 | 89 | 85 | 52 | 130 | 83 |
| 350 | 93 | 90 | 65 | 103 | 88 |
| 400 | 93 | 91 | 76 | 60 | 88 |
| 450 | 91 | 88 | 81 | 30 | 86 |
| 500 | 87 | 83 | 71 | 50 | 81 |

2. Effect of Gaseous NH₃ Added at 200 °C in Urea-SCR for $t_R = 4.0$ s

Figure S1 shows that during SCR test with urea ($t_R = 4.0$ s), the NO_x conversion increased with the addition of gaseous ammonia in the feed stream until approximately 50 ppm. This concentration corresponds to the necessary theoretical value to compensate the decrease of the NO_x conversion in urea-SCR with $t_R = 4.0$ s compared with $t_R = 5.2$ s at 200 °C. In the presence of excess of ammonia gas (added ammonia concentration higher than 50 ppm), the NO_x conversion becomes constant, indicating a NH₃ reaction order close to zero.

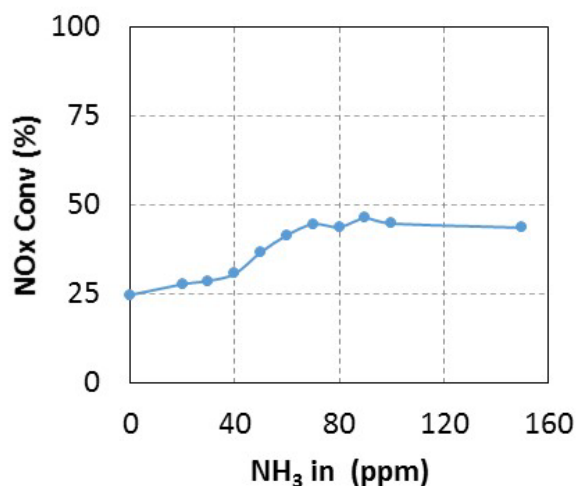


Figure S1. Effect of gaseous NH₃ added at 200 °C in urea-SCR for $t_R = 4.0$ s.

3. Thermodynamic Calculation



Table S2. Thermodynamic data.

| Products | $\Delta_f H^\circ_{298}$ (kJ·mol ⁻¹) | C_p (J·K ⁻¹ ·mol ⁻¹) | S°_{298} (J·K ⁻¹ ·mol ⁻¹) |
|---------------------|--|---|---|
| urea | -333 | 93 | 104 |
| HNCO(g) | -116.3 | 44 | 238.1 |
| H ₂ O(g) | -241.8 | 33.6 | 188.8 |
| CO ₂ (g) | -393.5 | 37.1 | 213.8 |
| NO(g) | 91.3 | 29.9 | 210.8 |
| NO ₂ (g) | 33.2 | 37.2 | 240.1 |
| O ₂ (g) | 0 | 29.4 | 204.8 |

Data are extracted from “Handbook of chemistry and physics, 78th edition, 1998, crc press” except for urea (Andersson, O.; Matsuo, T.; Suga, H.; Ferloni, P. Low-temperature heat capacity of urea. *Int. J. Thermophys.* 1993, 14, 149–158) and HNCO (Chase, M.W., Jr. *NIST-JANAF Thermochemical Tables*, Fourth Edition, *J. Phys. Chem. Ref. Data, Monograph 9*, 1998, 1–1951).

$$\Delta_r G^\circ_{573} = \Delta_r H^\circ_{573} - 573 \times \Delta_r S^\circ_{573} \quad (\text{S2})$$

$$\Delta_r H^\circ_{573} = \Delta_r H^\circ_{298} + \int_{298}^{573} (\Delta C_p)_{\text{gaz}} dT \quad (\text{S3})$$

$$\begin{aligned} \Delta_r H^\circ_{298} = & 3 \Delta_f H^\circ(\text{NO}) + 2 \Delta_f H^\circ(\text{CO}_2) + \Delta_f H^\circ(\text{H}_2\text{O}) - 2 \Delta_f H^\circ(\text{O}_2) - \Delta_f H^\circ(\text{NO}_2) - \\ & 2 \Delta_f H^\circ(\text{HNCO}) = -555.5 \text{ kJ}\cdot\text{mol}^{-1} \end{aligned} \quad (\text{S4})$$

$$\begin{aligned} (\Delta C_p)_{\text{gaz}} = & 3 C_p(\text{NO}) + 2 C_p(\text{CO}_2) + C_p(\text{H}_2\text{O}) - 2 C_p(\text{O}_2) - C_p(\text{NO}_2) - 2 C_p(\text{HNCO}) \\ & = 13.5 \text{ J}\cdot\text{K}^{-1} \text{ constant} \end{aligned} \quad (\text{S5})$$

$$\Delta_r H^\circ_{573} = -555,500 + 13.5 \cdot (573 - 298) = -551.8 \text{ kJ} \quad (\text{S6})$$

$$\begin{aligned} \Delta_r S^\circ_{298} = & 3 \Delta S^\circ(\text{NO}) + 2 \Delta S^\circ(\text{CO}_2) + \Delta S^\circ(\text{H}_2\text{O}) - 2 \Delta S^\circ(\text{O}_2) - \Delta S^\circ(\text{NO}_2) - \\ & 2 \Delta S^\circ(\text{HNCO}) = 122.9 \text{ J}\cdot\text{K}^{-1}\cdot\text{mol}^{-1} \end{aligned} \quad (\text{S7})$$

$$\Delta_r S^\circ_{573} = \Delta_r S^\circ_{298} + \int_{298}^{573} (\Delta C_p)_{\text{gaz}} dT/T = 122.9 + 13.5 \ln(573/298) = 131.7 \text{ J}\cdot\text{K}^{-1} \quad (\text{S8})$$

$$\Delta_r G^\circ_{573} = -551,800 - 573 \times (131.7) = -627 \text{ kJ} \quad (\text{S9})$$