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The Mechanisms of AlGaN Device Buffer Layer Growth and Crystalline Quality Improvement: Restraint of Gallium Residues, Mismatch Stress Relief, and Control of Aluminum Atom Migration Length

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Abstract: The mechanisms of AlGaN device buffer layer growth were studied. Gallium residues in the reactor chamber may be harmful to the quality of the AlN strain modulation layer, which eventually worsens the AlGaN buffer layer. By restraining the gallium residues, the crystalline quality of the AlGaN layer is markedly improved. In addition, enhancing stress relief in nucleation and coalescence stages will reduce the edge dislocations induced by strain relaxation in the 2D growth stage. A slower precursor flow rate can promote the stress relief in nucleation and coalescence stages. By comparison, a suitable suppression of Al atoms' surface migration can decrease surface roughness, which can be realized by increasing the precursor flow rate. Eventually, we obtained a AlGaN buffer layer having both low edge dislocation density and a flat surface using a two-step growth method.

Keywords: AlGaN; stress control; aluminum atom migration length



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1. Introduction

AlGaN materials have wide-ranging applications in the ultraviolet (UV) optoelectronic field, such as UV laser diodes (UV LDs) and UV light emission diodes (UV LEDs) [1–8]. Cathodoluminescence-based AlGaN materials with carbon nanotube field emitters are also promising light sources for sterilization, disinfection, and water purification [9]. For UV LDs, when the emission wavelength is below 360 nm, a high-quality AlGaN buffer layer with Al composition higher than 15% will be needed in many nitride device applications [10–15]. Hence, the growth in the AlGaN buffer film with high crystal quality is essential. However, due to the short migration length of Al atoms and the lack of substrate with matched lattice constants, the achievement of AlGaN growth with high crystal quality is a challenge [5]. One solution is the use of patterned GaN(AlN) substrate [10–13]. However, patterned GaN(AlN) substrate will raise manufacturing costs compared to sapphire substrate. Thus, sapphire substrate is still widely used for the heterostructural growth of AlGaN films. Many studies have tried to address the lattice mismatch problem of sapphire substrate by inserting an AlN strain modulation layer [16–18]. Therefore, it is important to study and optimize the AlGaN buffer growth on the AlN strain modulation layer.

Using the AlN strain modulation layer, we grew several AlGaN samples on sapphire substrates by metal-organic chemical vapor deposition (MOCVD). The mechanisms of AlGaN growth and the optimization of growth condition are discussed.

2. Materials and Methods

In this work, we used an AIXTRON CCS 6 × 2 MOCVD device (Aixtron, Aachen, Germany) for AlGa_N sample growth. Firstly, a 500 nm AlN strain modulation layer was grown on the sapphire (001) substrates at 1120 °C for all samples. Then, AlGa_N layers were grown after the AlN strain modulation layer at 1070 °C. The structure of the samples can be seen in Figure 1. All studied AlGa_N buffer samples A, B, C, D, E, and F are about 2~3 μm thick, with Al composition of 16.1~19.0%. The Al composition was measured by X-ray diffraction (XRD) reciprocal space mapping (RSM, Rigaku, Tokyo, Japan) [19,20]. The details of Al composition measurement can be seen in the Supplementary Materials, Figure S1 and Table S1. All samples' growth parameters are shown in Tables 1 and 2. For samples C, D, E, and F, before the AlGa_N buffer growth, one additional AlGa_N film growth run has performed in the MOCVD reactor in order to create a reactor chamber environment suitable for the further AlGa_N growth. However, no such earlier AlGa_N growth run was undertaken for samples A and B. Instead, their growth occurred with an additional pre-trimethylaluminum (pre-TMAI) flow rate treatment. Two different flow rates of pre-TMAI were passed into the reactor chamber before the AlN strain modulation layer growth. The various runs were separated by a baking process that cleaned the chamber. For better quality material, back-to-back AlGa_N runs and minimizing the bakes is important. Furthermore, ensuring the chamber/susceptor and showerhead are cleaned out periodically can reduce the particle issues on the wafer. During the baking process, 20,000 sccm H₂ was passed into the reactor chamber. This process lasted 40 min at 1100 °C.

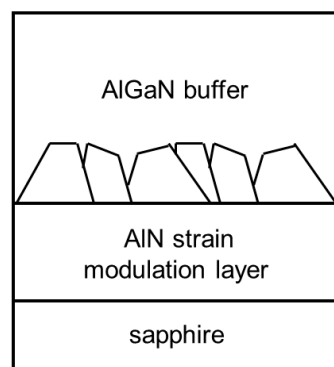


Figure 1. The schematic diagram of the sample structure in the vertical direction.

Table 1. The growth parameters of AlGa_N samples A, B, C, D, and E.

Sample	Pre-TMAI (sccm)	TMAI (sccm)	TMGa (sccm)	NH ₃ (sccm)	An Additional AlGa _N Growth	Aluminum Composition
A	1	27.5	34.7	3000	No	18.2%
B	5	27.5	34.7	3000	No	19.0%
C	0	27.5	34.7	3000	Yes	17.6%
D	0	41.0	52.0	4500	Yes	16.5%
E	0	55.0	69.4	6000	Yes	16.1%

Table 2. The growth parameters of sample F.

Growth Stage	Flow Rate (sccm)				
	TMAI	TMGa	NH ₃		
Nucleation	27.5	34.7	3000		
Coalescence	27.5	34.7	3000		
2D Growth	41.0	52.0	4500		
Pre-TMAI (sccm)	0	An Additional AlGa _N Growth	Yes	Aluminum Composition	16.8%

It can be seen from Table 1 that samples C, D, and E have different gas precursor flow rates, thus they have various AlGaIn growth rates. Among these three samples, the flow rate of sample C is the lowest and that of sample E is the highest. The precursor flow rates of samples A and B are the same as that of sample C. In addition, sample F was grown with a so-called two-step growth method, in which the precursor flow rate of the AlGaIn layer is divided into two steps. One lower flow rate is employed in nucleation and coalescence stages, and a higher rate is used in the 2D growth stage, as shown in Table 2. The details of sample F's design and growth are discussed later. The atomic force microscope (AFM) can provide the surface information of the AlGaIn buffer, and XRD is widely used for crystal dislocation measurement. Hence, during this study, AFM and XRD tests were conducted to analyze crystalline qualities of the AlGaIn buffer layers.

3. Results

The AFM results can be seen in Figure 2 and Table 3. Sample A shows a clear surface morphology related to step bunching and trench-like roughness. These phenomena were not evident on other samples. Compared to B, samples C, D, E, and F have clearer step flow morphology. The root mean square roughness (R_q) and average roughness (R_a) information show that the surface of sample E is the flattest and that of A is the roughest. Furthermore, B is also far rougher than C, D, E, and F. According to AFM images and roughness information data, sample A has the worst surface quality, and the surface quality of B is also far lower than that of the other three samples. Sample E has the highest surface quality.

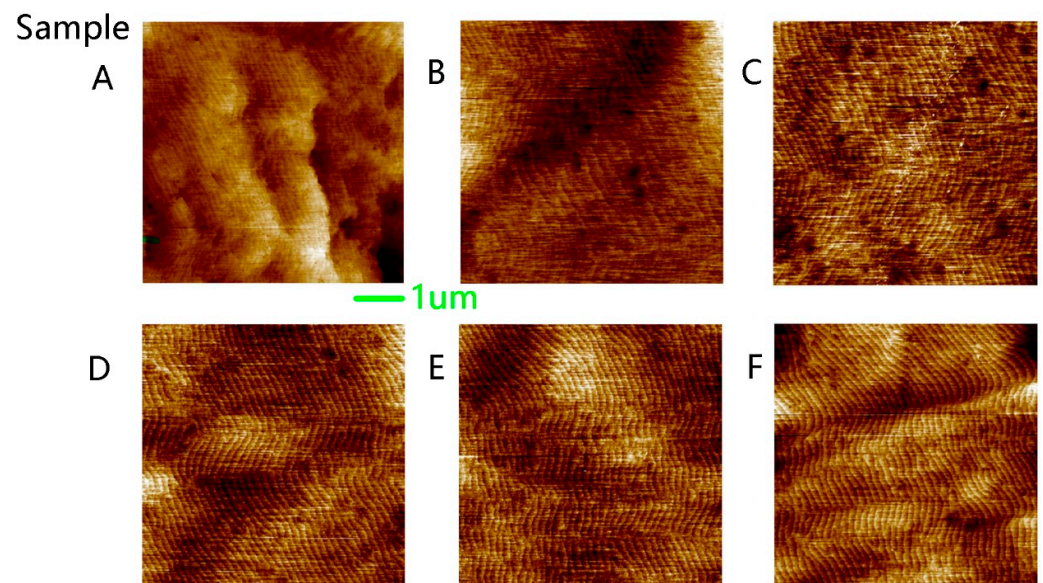


Figure 2. The $5 \times 5 \mu\text{m}$ AFM images of samples (A–F).

Table 3. The crystalline quality indexes of 6 AlGaIn samples.

Sample	AFM Roughness (nm)		AlGaIn XRD FWHM (arcsec)		
	R_q	R_a	(002)	(102)	(100)
A	0.622	0.478	148	945	1373
B	0.414	0.317	152	594	854
C	0.282	0.216	206	315	405
D	0.244	0.194	149	381	534
E	0.236	0.188	153	549	786
F	0.239	0.188	207	297	374

Table 3 and Figure 3 also show the XRD results of AlGa_N buffer layers. The full width of half maximum (FWHM) values of (002) ($\beta_{(002)}$) and (102) ($\beta_{(102)}$) were directly measured by rocking curves. FWHM of (100) ($\beta_{(100)}$) are calculated from the formula:

$$\beta_{(100)} = \sqrt{\frac{\beta_{(102)}^2 - \cos^2 \theta \cdot \beta_{(002)}^2}{\sin^2 \theta}} \quad (1)$$

where θ is the angle between (002) and (102). The normal direction of (002) is in the vertical direction because the AlGa_N is grown in the <002> direction. During the (102) XRD rocking curve tests, the sample stage was tilted until the normal direction of (102) was in the vertical direction. This process can be calibrated by the XRD diffraction intensity during the test. In this case, θ is equal to the tilt angle of sample stage, which is near 43°. It is known that the values of $\beta_{(002)}$ and $\beta_{(100)}$ are proportional to the screw and edge dislocation densities in the samples, respectively [21].

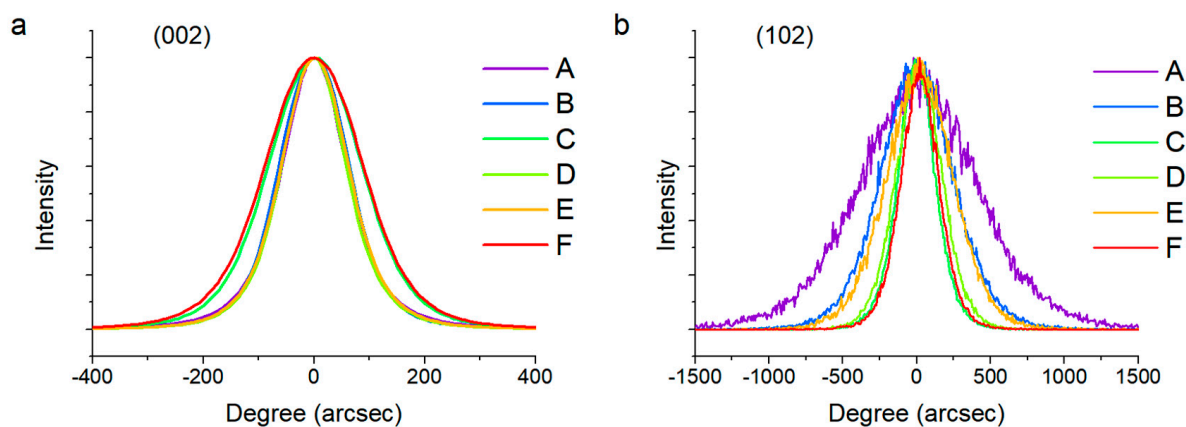


Figure 3. The (002) (a) and (102) (b) ω scan of samples A, B, C, D, E, and F.

Samples A, B, and C have the same precursor flow rate. In all these samples, A has the largest AlGa_N $\beta_{(100)}$ whereas C has the smallest. Among the four samples having additional AlGa_N growth, samples C and F have relatively smaller AlGa_N $\beta_{(100)}$, but sample E has far larger $\beta_{(100)}$ than the other three samples.

4. Discussion

4.1. Restrain of Gallium Residues

GaN-based materials are sensitive to MOCVD reactor chamber environment condition [22]. Therefore, environment treatment is very important for the epitaxy growth of the AlGa_N buffer. Firstly, we studied the influence of reactor chamber residues on AlGa_N growth quality by samples A and B. Two different pre-TMAI flow rates of 1 and 5 sccm for A and B, respectively, were passed in the reactor before the growth of the AlN strain modulation layer. Regardless of the surface topography, roughness, or the value of AlGa_N $\beta_{(100)}$, the crystalline quality of sample B was far better than that of A, which suggests that a higher Pre-TMAI flow rate can lead to better AlGa_N quality. One reasonable explanation is that an Al-rich environment is beneficial to AlN's nucleation and growth, which will improve the quality of the AlN strain modulation layer and the AlGa_N film grown above it. Our MOCVD reactor is used not only for growing AlGa_N, but also for GaN. Therefore, residual GaN in the reactor chamber may decompose during the temperature lifting process because the growth temperature of AlN is higher than the decomposition temperature of GaN. Then Ga atoms may participate in the chemical deposit reaction and form AlGa_N, which hinders the growth of the AlN strain modulation layer [23]. Hence, a pre-TMAI flow rate can alleviate the unwanted problem of deposition of gallium and indium, enabling the AlN layer to have a higher crystalline quality [23]. Eventually, this leads to better AlGa_N buffer quality.

To verify the above hypothesis, the $\beta_{(002)}$ and $\beta_{(102)}$ of AlN for these samples were measured. The AlN $\beta_{(002)}$ of sample A was 220 arcsec and its $\beta_{(102)}$ is 1512 arcsec. However, sample B had a lower AlN $\beta_{(002)}$ (174 arcsec) and $\beta_{(102)}$ (1152 arcsec). This supports our assumption that increasing the pre-TMAI flow rate can improve the crystalline quality of the AlN strain modulation layer.

By comparison, the gallium residue problem can be also solved if the MOCVD has just undertaken additional AlGaN growth. Sample C used the same AlGaN growth parameters as those of A and B but yielded a better surface topography and a lower AlGaN $\beta_{(100)}$ than the samples without earlier AlGaN growth. This suggests that additional AlGaN growth created an environment that is beneficial to the subsequent AlGaN growth. Restraining gallium residues can reduce AlGaN dislocations and improve its surface.

4.2. Mismatch Stress Relief

The growth model of AlGaN on the AlN strain modulation layer can be described by three stages: (i) nucleation; (ii) coalescence; and (iii) two-dimensional growth (2D growth); these are shown in Figure 4a [24,25]. Due to the large mismatch strain between AlN and AlGaN, deposited AlGaN will not form a flat surface, but first form a large number of small grains, which is called the nucleation stage [24]. The surface becomes rougher and rougher during stress relief through nucleation and grain growth. The in situ reflectance curve shows a drop at the nucleation stage. Then, at the coalescence stage, grains continue to grow and start to coalesce. Furthermore, the surface becomes smoother and the optical reflectance rises. Finally, the reflectance stops increasing and 2D growth of the AlGaN begins. If the mismatch strain is released adequately at the nucleation and coalescence stages, AlGaN will be relaxed in the beginning of 2D growth stage. Otherwise, the remaining stress will be released at the 2D growth stage by forming new dislocations, specifically, threading edge dislocations [26]. Strain relaxation will mainly cause the twist of (100) faces, which can be detected by the broadening of $\beta_{(100)}$ [27].

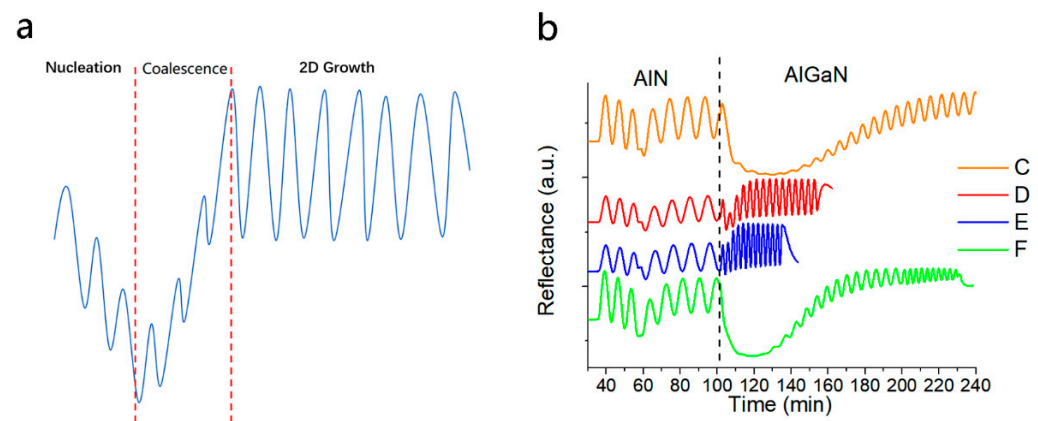


Figure 4. (a) The schematic diagram of an in situ reflectance curve divided in 3 parts in the initial stage of AlGaN growth. (b) The in situ 633 nm reflectance curves of samples C, D, E, and F.

It is noted that the growth conditions of samples C, D, and E in Table 1, i.e., their source gas flow rates, are different. The XRD results of samples C, D, and E are different, as shown by Table 3. This indicates that the source gas flow rate can influence AlGaN's $\beta_{(100)}$ of XRD. Among these three samples, sample C's precursor flow rate is the lowest and that of E is the highest. When the flow rate is too high, the mismatch strain between AlN and AlGaN is unable to be released adequately during the nucleation and coalescence stages. As shown in Figure 4b, compared to sample C, the nucleation and coalescence stages of sample E are much shorter. The duration of the nucleation and coalescence stages of sample E is less than 20 min, whereas the duration of C is over 80 min. Moreover, sample E's reflectance decrease during the nucleation stage is also less, which means that the mismatch strain relief may be not adequate at these stages. The remaining stress will be released at the 2D

growth stage by the generation of a higher density of edge dislocations, which results in the highest AlGaN $\beta_{(100)}$ value of sample E among the three samples. Therefore, it is assumed that enhancing stress relief in nucleation and coalescence stages can decrease the density of AlGaN edge dislocations.

4.3. Control of Aluminum Atom Migration Length

Another important quality index of AlGaN buffer is the surface roughness [28,29]. A smooth surface will actively contribute to the growth of the subsequent layer structure. This study found that appropriate restraint of the Al atom migration length improved the AlGaN surface. According to the AFM image results of samples C, D, and E, a higher precursor flow rate can yield a better surface. The roughness results also show that sample E has the flattest surface. A low source gas flow rate leads to a low AlGaN growth rate at the 2D growth stage. The growth rates for samples C, D, and E at the 2D growth stage were 1.45, 2.52, and 3.35 $\mu\text{m}/\text{h}$, respectively. Generally, a slower growth rate can increase the Al atom migration length and thus induce a flatter surface. An Al atom migration length that is too short will hinder step flow growth. However, even sample E, which has the faster growth rate among samples C, D, and E, had a clear step flow morphology. This indicates the Al atom migration length was enough for a good step flow growth mode in our study. In this case, increasing the Al atom migration length may no longer result in a flatter surface. Conversely, when the growth rate is too low, the migration distance of Al atoms on the surface will be too large, so the Al atom migration distance may be much higher than the separation between steps [30,31]. A step edge on the grown surface will be much more likely to interact with more atoms, which may be heterogeneously accumulated and induce a rougher surface [30]. Hence, reducing Al atom migration length appropriately may contribute to a smoother AlGaN surface.

4.4. Two-Step Growth Method

To acquire an AlGaN buffer layer with high crystalline quality, three aspects need to be address, as discussed. Firstly, an additional AlGaN growth step is necessary in order to restrain the influence of gallium residues. Moreover, according to the discussions above, a low precursor flow rate can improve the stress relief in nucleation and coalescence stages, whereas a higher growth rate will reduce Al atom migration length. Hence, precursor flow rate plays an extremely important role in AlGaN quality, which can be clearly seen from Figure 5.

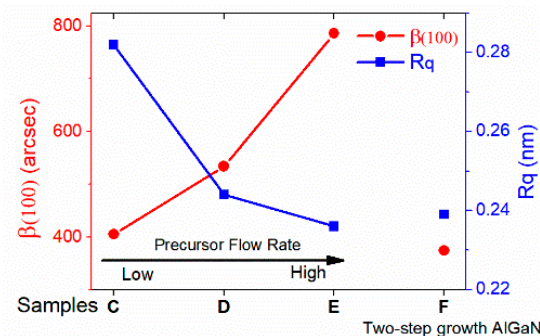


Figure 5. The relationship between precursor flow rate and AlGaN crystalline qualities.

In order to simultaneously acquire both a low edge dislocation density and a flat surface, a two-step AlGaN growth method was designed and tested. As shown in Table 2, this method uses a low precursor flow rate in the nucleation and combination stages, and a higher flow rate in its 2D growth stage. At the beginning of AlGaN growth, a lower precursor flow rate causes longer nucleation and combination stages. The reflectance of sample F drops abruptly and then rises slowly, as shown in Figure 4b. The mismatch stress between the AlN strain modulation layer and the AlGaN buffer layer is adequately released. Then, a higher precursor flow rate is applied at the 2D growth stage. A higher

growth rate can reduce the Al atom migration length and thus lead to a better AlGaIn surface. The sample F's XRD $\beta_{(002)}$ was 207 arcsec, its $\beta_{(102)}$ was 297 arcsec, and its $\beta_{(100)}$ was 374 arcsec. This result was also better than typical qualities for AlGaIn layers grown on sapphire (366 arcsec for $\beta_{(002)}$ and 1023 arcsec for $\beta_{(102)}$) [32]. These data of the XRD result are close to those of the AlGaIn grown using a low gas precursor flow rate (sample C), representing low values of the dislocation densities. By comparison, sample F's R_q was 0.239 nm and its R_a was 0.188 nm. These values are also relatively low, which means it has a surface quality similar to that of AlGaIn layers grown using a high growth rate (such as samples D and E). Based on the two-step growth method, a AlGaIn device buffer layer was grown having a low density of edge dislocations and a flat surface.

5. Conclusions

The mechanisms of AlGaIn growth and the methods of crystalline quality improvement were studied. Gallium residues left in the MOCVD reactor chamber may influence the quality of the grown AlN strain modulation layer and the AlGaIn device buffer layer. Passing TMAI in the reactor chamber during the temperature lifting process can reduce the influence of gallium residues. Furthermore, the problem can be also solved in another manner: by growing an additional AlGaIn layer in the MOCVD reactor before the AlGaIn buffer growth. In the paper, the effects of the stress relief and Al atom migration length on the AlGaIn buffer are discussed. The stress relief in nucleation and coalescence stages can efficiently decrease the density of edge dislocations induced by strain relaxation in the 2D growth stage. By comparison, an appropriate restraint of Al atoms' surface migration can improve the AlGaIn surface. By adjusting the precursor flow rate, the stress relief process and Al atom migration length can be controlled. Hence, a two-step growth method is proposed, in which a low precursor flow rate is applied in nucleation and coalescence stages, and a higher flow rate is applied in the 2D growth stage. Using this two-step growth method, we acquired a high-quality AlGaIn buffer layer having both a lower edge dislocation density and a flatter surface.

Supplementary Materials: The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/cryst12081131/s1>, Figure S1: The (105) RSM of samples A, B, C, D, E, and F; Table S1: The reciprocal space coordinates of AlGaIn (105) RSM and the Al composition for the six samples.

Author Contributions: Conceptualization, B.W. and J.Y.; methodology, B.W. and J.Y.; software, Z.L.; validation, Y.Z. and Z.Z.; formal analysis, F.L.; investigation, P.C.; resources, D.Z.; data curation, B.W.; writing—original draft preparation, B.W.; writing—review and editing, B.W.; visualization, Z.L.; supervision, D.Z. and J.Y.; project administration, D.Z. and J.Y.; funding acquisition, D.Z. All authors have read and agreed to the published version of the manuscript.

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