

## Article

# A Theoretical Investigation of the Polyaddition of an $AB_2+A_2+B_4$ Monomer Mixture

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**Abstract:** Hyperbranched polymers (HBPs) are widely applied nowadays as functional materials for biomedicine needs, nonlinear optics, organic semiconductors, etc. One of the effective and promising ways to synthesize HBPs is a polyaddition of  $AB_2+A_2+B_4$  monomers that is generated in the  $A_2+CB_2$ ,  $AA'+B_3$ ,  $A_2+B'B_2$ , and  $A_2+C_2+B_3$  systems or using other approaches. It is clear that all the foundational features of HBPs that are manufactured by a polyaddition reaction are defined by the component composition of the monomer mixture. For this reason, we have designed a structural kinetic model of  $AB_2+A_2+B_4$  monomer mixture polyaddition which makes it possible to predict the impact of the monomer mixture's composition on the molecular weight characteristics of hyperbranched polymers (number average ( $DP_n$ ) and weight average ( $DP_w$ ) degree of polymerization), as well as the degree of branching (DB) and gel point ( $p_g$ ). The suggested model also considers the possibility of a positive or negative substitution effect during polyaddition. The change in the macromolecule parameters of HBPs formed by polyaddition of  $AB_2+A_2+B_4$  monomers is described as an infinite system of kinetic equations. The solution for the equation system was found using the method of generating functions. The impact of both the component's composition and the substitution effect during the polyaddition of  $AB_2+A_2+B_4$  monomers on structural and molecular weight HBP characteristics was investigated. The suggested model is fairly versatile; it makes it possible to describe every possible case of polyaddition with various monomer combinations, such as  $A_2+AB_2$ ,  $AB_2+B_4$ ,  $AB_2$ , or  $A_2+B_4$ . The influence of each monomer type on the main characteristics of hyperbranched polymers that are obtained by the polyaddition of  $AB_2+A_2+B_4$  monomers has been investigated. Based on the results obtained, an empirical formula was proposed to estimate the  $p_g = p_A$  during the polyaddition of an  $AB_2+A_2+B_4$  monomer mixture:  $p_g = p_A = (-0.53([B]_0/[A]_0)^{1/2} + 0.78)\nu AB_2 + (1/3)^{1/2}([B]_0/[A]_0)^{1/2}$ , where  $(1/3)^{1/2}([B]_0/[A]_0)^{1/2}$  is the Flory equation for the  $A_2+B_4$  polyaddition,  $[A]_0$  and  $[B]_0$  are the A and B group concentration from  $A_2$  and  $B_4$ , respectively, and  $\nu AB_2$  is the mole fraction of the  $AB_2$  monomer in the mixture. The equation obtained allows us to accurately predict the  $p_g$  value, with an  $AB_2$  monomer content of up to 80%.

**Keywords:** hyperbranched polymers; degree of branching; co-polyaddition; gel point;  $AB_2+A_2+B_4$  monomer mixture



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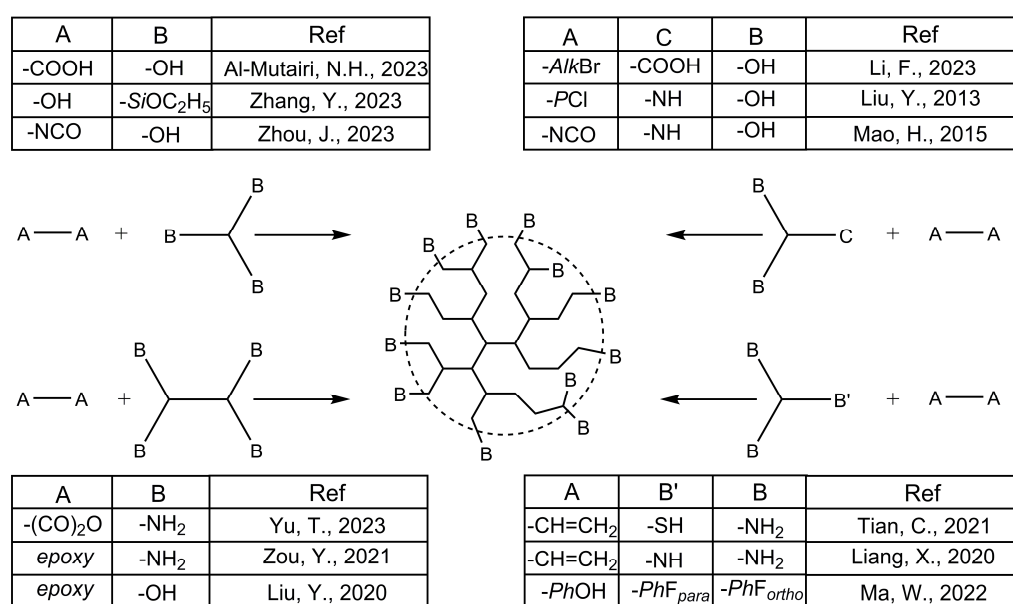
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## 1. Introduction

The synthesis and investigation of properties of hyperbranched polymers (HBPs) represents one of the most rapidly advancing areas in polymer science. They have a wide range of applications due to the number of unique features compared to the linear and cross-linked polymers, including high solubility, thermodynamic compatibility, low viscosity, high sorption capacity, and a high content of functional groups [1–3]. HBPs

are widely applied nowadays as functional materials for biomedicine needs [4,5], non-linear optics [6,7], organic semiconductors [8,9], and flame-retardant materials [10,11], among others.

One of the key ways to obtain HBP is homo-polyaddition of AB<sub>m</sub>-type monomers [12–14]. The primary advantage of polyaddition of AB<sub>m</sub>-type monomers is that it does not lead to gelation [15], allowing for a production of high-molecular-weight (MW) polymers with a degree of branching (DB) of 0.5 [16]. However, obtaining AB<sub>m</sub>-type monomers often involves a complex organic synthesis; moreover, there are some considerable complications arising in the process of isolation and purification of these monomers containing highly reactive groups [17,18]. This poses a notable barrier to the practical application of HBPs that are obtained through the aforementioned methods. For this reason, co-polyaddition of monomer mixtures of different types, for example, A<sub>2</sub>+B<sub>3</sub>, A<sub>2</sub>+B<sub>4</sub>, etc., have found wider application [19–28] (Scheme 1).



**Scheme 1.** Synthesis of HBP by polyaddition of the monomer types A<sub>2</sub>+B<sub>3</sub> [23–25], A<sub>2</sub>+B<sub>4</sub> [26–28], A<sub>2</sub>+CB<sub>2</sub> [29–31], and A<sub>2</sub>+B'B<sub>2</sub> [32–34].

The introduction of this method has enabled a significant expansion of the range of monomers that are under use and also the carrying out of polyaddition as a single-step reaction. It is a known fact that this kind of co-polyaddition eventually results in the formation of a three-dimensional structure at a specific juncture, commonly referred to as the critical gelation conversion, or gel point ( $p_g$ ). To determine the  $p_g$  value in these Flory systems, Equation (1) was offered [35].

$$\alpha = \frac{rp_A^2\rho}{1 - rp_A^2(1 - \rho)} = \frac{p_B^2\rho}{r - p_B^2(1 - \rho)} \quad (1)$$

where  $r = [A]_0/[B]_0$ ,  $\rho$  is the ratio of B (or A) groups in branched units to the total number of these groups, and  $p_A$  and  $p_B$  are the conversions of A and B groups, respectively.

In general,  $p_g = \max(p_A, p_B)$ . Hereinafter, when  $[A]_0/[B]_0 > 1$ ,  $p_g = p_B$ , because  $p_A < p_B$  in that range. Correspondingly, if  $[A]_0/[B]_0 < 1$ , then  $p_g = p_A$ , and when  $[A]_0/[B]_0 = 1$ ,  $p_A = p_B = p_g$ .

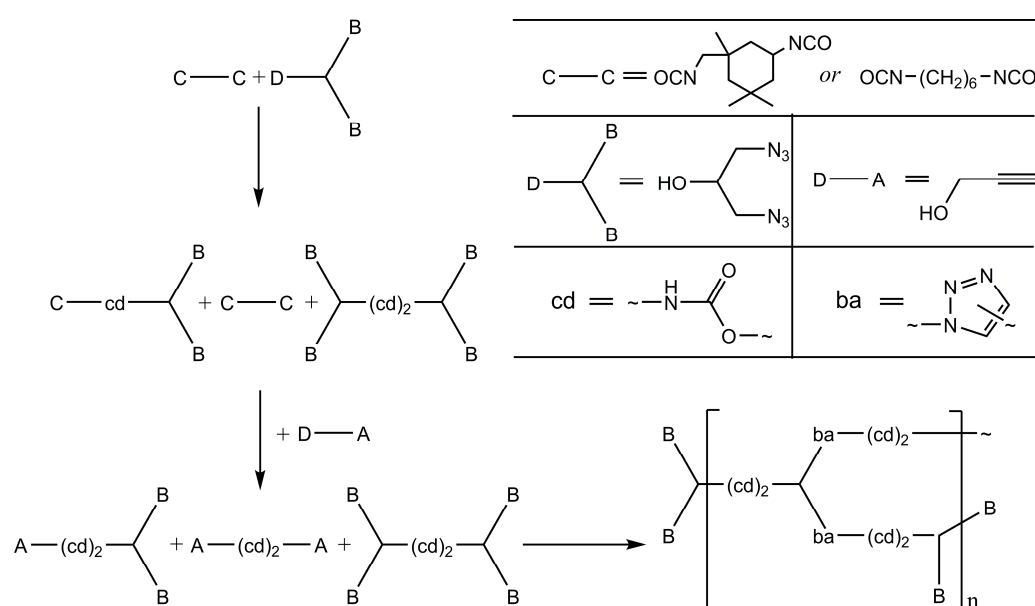
To reduce the  $p_g$  value, co-polyaddition of asymmetric monomers (A<sub>2</sub>+CB<sub>2</sub>, A<sub>2</sub>+B'B<sub>2</sub>, AA'+B<sub>3</sub>, A<sub>2</sub>+C<sub>2</sub>+B<sub>3</sub>) was introduced [29–39] (Scheme 1). These approaches made it possible to shift the gel point, since more AB<sub>2</sub> monomers were formed, and therefore, it was possible to obtain polymers with an increased MW. To describe the polyaddition of A<sub>2</sub>+CB<sub>2</sub>

monomers, a number of simulations have been developed [40,41] to predict polydispersity index (PDI) values depending on the ratio of reactants (Equation (2)).

$$\text{PDI} = \frac{\text{DP}_w}{\text{DP}_n} = \frac{(1 + 1/\lambda - 2p_A[2p_Bp_C + p_B^2 + \lambda + p_C^2/(2\lambda) + p_B^2/\lambda + 1 + 4p_B + 2p_C])}{(1 + 1/\lambda)^2(\lambda - p_B^2 - 2p_Bp_C)} \quad (2)$$

where  $\text{DP}_w$  and  $\text{DP}_n$  are the weight average and the number average degree of polymerization,  $p_A$ ,  $p_B$ ,  $p_C$  are conversions of A, B, and C groups, and  $\lambda$  is the initial ratio of  $A_2$  and  $CB_2$  monomer concentrations.

Previously, we successfully implemented an approach to obtain HBPs, using polyaddition of the  $AB_2+A_2+B_4$  monomer mixture with controlled contents of each constituent [42,43] (Scheme 2). That technique can also be applied to the co-polyaddition of asymmetric monomers due to the formation of  $AB_2$  monomers.



**Scheme 2.** Synthesis of HBP by polyaddition of the monomers of  $AB_2+A_2+B_4$  type [36,37], where *ba* is the product of interaction between A and B groups, *cd* is the product of interaction between C and D groups.

Despite the fact that the  $AB_2+A_2+B_4$  monomer mixture can be obtained during the polyaddition of  $A_2+CB_2$  monomers, there is a lack of current theories and ideas to adequately describe every possible combination of these monomers in the mixture. The methods described above prevent obtaining a complete picture of the impact of each constituent of the  $AB_2+A_2+B_4$  monomer mixture on HBP formation.

Moreover, positive or negative substitution effects taking place during polyaddition and described in a number of experimental papers [44–47] would significantly affect both the MW and the structural characteristics of the resulting polymers. The manifestation of a positive substitution effect, e.g., in the Friedel–Crafts aromatic substitution reaction of  $AB_2$ , leads to the production of fully branched HBPs [38]. The manifestation of a negative substitution effect, e.g., during the production of hyperbranched polyesters by copolycondensation of an  $AB_2$ -type monomer and  $B_4$ - and  $B_6$ -type polyfunctional cores, leads to a decrease in the MW of the final product [39]. There is no doubt that the substitution effect will also affect the value of  $p_g$  in cases where it may be less than 1.

The kinetic Monte Carlo method and molecular dynamics simulations are widely used nowadays to investigate the evolution of the structure of hyperbranched polymers and polymer networks [48–50]. At the same time, the conventional kinetic method that has proven itself for the investigation of HBP formation currently remains of interest [51–55].

Given all the facts above, we aim to develop a new structural kinetic model of the polyaddition of an  $AB_2+A_2+B_4$  monomer mixture, taking into account the potential manifestation of the substitution effect during polyaddition. Additionally, it would enable us to determine the impact of each system constituent on the structural and molecular weight parameters of HBPs.

## 2. Calculation Section

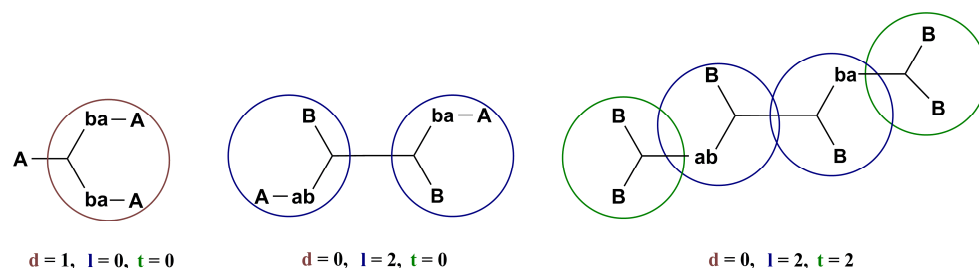
### 2.1. Design of the Kinetic–Structural Model

To describe the  $AB_2+A_2+B_4$  system, it is essential to establish certain assumptions and conditions. These will provide a framework for describing various reactions and types of resulting compounds that may emerge.

The assumptions are as follows:

- Flory assumption, i.e., function group reactivity is independent of the chain length;
- System homogeneity;
- No solvent impact.

The designed model is based on the concept of homo-polyaddition of  $AB_2$ -type monomers [55]. To describe the  $AB_2+A_2+B_4$  system properly, it is also necessary to add a new parameter to the ones that were employed in [55] (the number of linear ( $l$ ) and terminal ( $t$ ) units). That is the number of dendritic units ( $d$ ) (Figure 1).

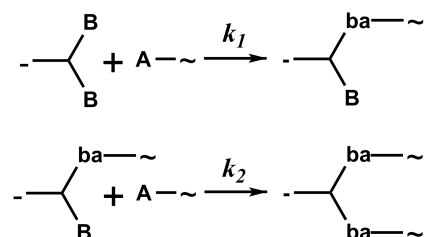


**Figure 1.** Structural units in the  $AB_2+A_2+B_4$  system, where  $ba/ab$  is the product of interaction between A and B groups.

The addition of the  $d$  unit results in the introduction of a new kind of compound,  $A_n$ , which cannot be described accurately by  $t$  and  $l$  parameters only, since the number of A groups depends on  $d$ :  $A_{\max} = d + 2$ .

The number of A groups in a macromolecule is equal to  $A_{\max}$  when  $l$  units are formed without any  $t$  ones. In case of the formation of a  $t$  unit, the number of A groups in a macromolecule is 2 less, while the number of  $d$  units is only 1 less than in the compound  $A_n$  (Figure 1). So, the amount of A groups during the  $t$  unit formation equals  $-1 \times t + A_{\max}$ , resulting in the following equation describing a real case of polyaddition as  $A = d + 2 - t$ .

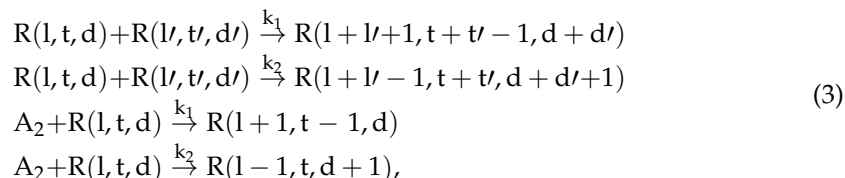
The substitution effects, occurring when the polyaddition of  $AB_2+A_2+B_4$  monomer mixture takes place, are included in the structural kinetic model (Scheme 3).



**Scheme 3.** Positive and negative substitution effects during the polyaddition of the  $AB_2+A_2+B_4$  monomer mixture, where  $ba$  is the product of interaction between A and B groups.

The reactivity of B groups belongs to  $t$  units and can be determined by the  $k_1$  rate constant, whereas one of the B groups from  $l$  units is included in the  $k_2$  rate constant. B groups can be provided by either  $AB_2$  or  $B_4$  monomers and also by the interaction products of these monomers and with an  $A_2$ -type monomer. Thus, in the case of  $k_1/k_2 < 1$ , a positive substitution effect takes place, whereas in the case of  $k_1/k_2 > 1$ , there is a negative substitution effect.

Alterations in all structural parameters during the studied reaction can be described as a set in Equation (3):



where  $R(l, t, d)$  is a concentration of macromolecules with  $l$ —linear,  $t$ —terminal, and  $d$ —dendritic units.

The introduction of additional reactions with the  $A_2$ -type monomer is necessary to describe the initial conditions properly. According to the set of reactions (3), the endless kinetic equation can be defined by the following Equation (4), with initial conditions being  $[A_2] = [A_2]_0$ ,  $R(0, 1, 0) = [AB_2]_0$ , and  $R(0, 2, 0) = [B_4]_0$ , and the other  $R(l, t, d) = 0$ :

$$\begin{aligned}
 \frac{dR(l, t, d)}{d\tau} = &-(d + 2 - t)R(l, t, d) \left\{ 2k_1 \sum_{l, t, d}^{\infty} tR(l, t, d) + k_2 \sum_{l, t, d}^{\infty} lR(l, t, d) \right\} - (2k_1 t + k_2 l)R(l, t, d) \times \\
 &\times \left\{ 2[A_2] + \sum_{l, t, d}^{\infty} (d + 2 - t)R(l, t, d) \right\} + 2k_1 \left\{ \sum_{l_1=0}^1 \sum_{t_1=0}^t \sum_{d_1=0}^d (d + 2 - t)R(l_1, t_1, d_1)(t - t_1 + 1)R(l - l_1 - 1, t - t_1 + 1, d - d_1) + \right. \\
 &+ \left. \sum_{l_1=0}^1 \sum_{t_1=0}^t \sum_{d_1=0}^d (d + 2 - t)R(l_1, t_1, d_1)(t - t_1 + 1)R(l - l_1 - 1, t - t_1 + 1, d - d_1) \right\} + \\
 &+ 2k_1 2[A_2]R(l - l_1 - 1, t - t_1 + 1, d - d_1) + \\
 &+ k_2 \left\{ \sum_{l_1=0}^1 \sum_{t_1=0}^t \sum_{d_1=0}^d (d + 2 - t)R(l_1, t_1, d_1)(l - l_1 + 1)R(l - l_1 + 1, t - t_1, d - d_1 - 1) + \right. \\
 &+ \left. \sum_{l_1=0}^1 \sum_{t_1=0}^t \sum_{d_1=0}^d (d + 2 - t)R(l_1, t_1, d_1)(l - l_1 + 1)R(l - l_1 + 1, t - t_1, d - d_1 - 1) \right\} + k_2 2[A_2]R(l - l_1 + 1, t - t_1, d - d_1 - 1)
 \end{aligned}
 \tag{4}$$

The solution to the systems containing a large number of differential equations can only be achieved through the convolution of these equations. One of the simplest ways to accomplish this is by employing generating functions:

$$\Phi \equiv \sum_{l, t, d}^{\infty} R(l, t, d) s^l p^t n^d,
 \tag{5}$$

where  $s, p$ , and  $n$  are random variables.

Equation (4) can then be convolved with the  $\Phi$  function into a shorter one (6):

$$\frac{d\Phi}{d\tau} = -(n\Phi_n + 2\Phi - p\Phi_p)(2k_1 T + k_2 L) - (D + 2N - T + 2[A_2])(2k_1 p\Phi_p + k_2 s\Phi_s) + (n\Phi_n + 2\Phi - p\Phi_p + 2[A_2])(2k_1 s\Phi_p + k_2 n\Phi_s)
 \tag{6}$$

Consequently, we can switch from Equation (6) to the moments of the generating function  $\Phi$  (7):

$$\begin{aligned}
 \Phi(1, 1, 1) &= \sum_{l, t, d}^{\infty} R(l, t, d) \equiv N, \quad \Phi_s(1, 1, 1) = \sum_{l, t, d}^{\infty} lR(l, t, d) \equiv L, \quad \Phi_p(1, 1, 1) = \sum_{l, t, d}^{\infty} tR(l, t, d) \equiv T, \\
 \Phi_n(1, 1, 1) &= \sum_{l, t, d}^{\infty} dR(l, t, d) \equiv D, \quad \Phi_{ss} \equiv \frac{\partial^2 \Phi}{\partial s^2} = \sum_{l, t, d}^{\infty} l^2 R(l, t, d) - L, \\
 \Phi_{sp} &\equiv \frac{\partial^2 \Phi}{\partial s \partial p} = \sum_{l, t, d}^{\infty} ltR(l, t, d), \quad \Phi_{sn} \equiv \frac{\partial^2 \Phi}{\partial s \partial n} = \sum_{l, t, d}^{\infty} ldR(l, t, d), \quad \Phi_{pp} \equiv \frac{\partial^2 \Phi}{\partial p^2} = \sum_{l, t, d}^{\infty} t^2 R(l, t, d) - T, \\
 \Phi_{pn} &\equiv \frac{\partial^2 \Phi}{\partial p \partial n} = \sum_{l, t, d}^{\infty} tdR(l, t, d), \quad \Phi_{nn} \equiv \frac{\partial^2 \Phi}{\partial n^2} = \sum_{l, t, d}^{\infty} d^2 R(l, t, d) - D,
 \end{aligned}
 \tag{7}$$

and then the set of differential equations (8) for moments of the generating function  $\Phi$  can be obtained from the Equations (6) and (7):

$$\left\{ \begin{aligned} \frac{dN}{d\tau} &= -(D + 2N - T)(2k_1T + k_2L) \\ \frac{dT}{d\tau} &= -(D + 2N - T + 2[A_2])(k_2L - 2k_1T) \\ \frac{dL}{d\tau} &= -2k_1T(D + 2N - T + 2[A_2]) \\ \frac{dD}{d\tau} &= k_2L(D + 2N - T + 2[A_2]) \\ \frac{d\Phi_{ss}}{d\tau} &= -(D + 2N - T + 2[A_2])(2k_2\Phi_{ss} - 4k_1\Phi_{ps}) + (\Phi_{ns} + 2L - \Phi_{ps})(4k_1T + 4k_1\Phi_{ps} + 2k_2\Phi_{ss}) \\ \frac{d\Phi_{sp}}{d\tau} &= -(D + 2N - T + 2[A_2])(2k_1\Phi_{ps} + k_2\Phi_{ps} - 2k_1\Phi_{pp}) + (\Phi_{ns} + 2L - \Phi_{ps})(2k_1\Phi_{pp} + k_2\Phi_{ps}) + \\ &\quad + (2k_1T + 2k_1\Phi_{ps} + k_2\Phi_{ss})(\Phi_{np} + T - \Phi_{ps}) \\ \frac{d\Phi_{sn}}{d\tau} &= -(D + 2N - T + 2[A_2])(k_2\Phi_{sn} - 2k_1\Phi_{pn} - k_2\Phi_{ss}) + (\Phi_{ns} + 2L - \Phi_{ps})(k_2L + 2k_1\Phi_{pn} + k_2\Phi_{ns}) + \\ &\quad + (2k_1T + 2k_1\Phi_{ps} + k_2\Phi_{ss})(3D + \Phi_{nn} - \Phi_{pn}) \\ \frac{d\Phi_{pp}}{d\tau} &= -4k_1\Phi_{pp}(D + 2N - T + 2[A_2]) + (\Phi_{np} + T - \Phi_{ps})(4k_1\Phi_{pp} + 2k_2\Phi_{sp}) \\ \frac{d\Phi_{pn}}{d\tau} &= -(D + 2N - T + 2[A_2])(2k_1\Phi_{pn} - k_2\Phi_{sp}) + (\Phi_{np} + T - \Phi_{ps})(2k_1\Phi_{pn} + k_2L + k_2\Phi_{sn}) + \\ &\quad + (2k_1\Phi_{ps} + k_2\Phi_{sp})(3D + \Phi_{nn} - \Phi_{pn}) \\ \frac{d\Phi_{nn}}{d\tau} &= 2k_2\Phi_{sn}(D + 2N - T + 2[A_2]) + (3D + \Phi_{nn} - \Phi_{pn})(4k_1\Phi_{pn} + 2k_2\Phi_{sn} + 2k_2L) \end{aligned} \right. \quad (8)$$

with initial conditions being :

$$\left\{ \begin{aligned} N &= [AB_2]_0 + [B_4]_0 \\ T &= [AB_2]_0 + 2[B_4]_0 \\ D + 2N - T &= [AB_2]_0 \\ [A_2] &= [A_2]_0 \\ L &= 0 \\ D &= 0 \end{aligned} \right. \Rightarrow \left\{ \begin{aligned} [A_2]_0 &= [A_2] \\ [AB_2]_0 &= 2N - T \\ [B_4]_0 &= T - N \end{aligned} \right.$$

If  $R(l,t,d)$  is the content of macromolecules of the given composition, then the following set of equations can be defined (9):

$$\left\{ \begin{aligned} L_n &\equiv \frac{\sum_{l,t,d} lR(l,t,d)}{(N+[A_2])} = \frac{\Phi_s(1,1,1)}{\Phi_p(1,1,1)}, \\ T_n &\equiv \frac{\sum_{l,t,d} tR(l,t,d)}{(N+[A_2])} = \frac{\Phi_p(1,1,1)}{\Phi_n(1,1,1)}, \\ D_n &\equiv \frac{\sum_{l,t,d} dR(l,t,d)}{(N+[A_2])} = \frac{\Phi_n(1,1,1)}{\Phi_s(1,1,1)} \end{aligned} \right. \quad (9)$$

where  $L_n$ ,  $T_n$ , and  $D_n$  are equal to the values of the average content of linear, terminal, and dendritic units in a macromolecule.

We can determine the value of the average degree of polymerization ( $DP_n$ ) as  $n + 1$  amount of B groups involved in the reaction, i.e., the number of monomer units contained in a macromolecule, which is  $2d + l + 1$ . Thus,  $DP_n$  can be defined as follows (10):

$$DP_n = \frac{\sum_{l,t,d} (2d + l + 1)R(l,t,d)}{(N + [A_2])} = L_n + 2D_n + 1 \quad (10)$$

The mass average structural parameters can be determined by (11):

$$\left\{ \begin{aligned} L_w &= \frac{\sum_{l,t,d} l^2R(l,t,d)}{\sum_{l,t,d} lR(l,t,d)} = \frac{\Phi_{ss}(1,1,1)}{\Phi_s(1,1,1)} + 1, \\ T_w &= \frac{\sum_{l,t,d} t^2R(l,t,d)}{\sum_{l,t,d} tR(l,t,d)} = \frac{\Phi_{pp}(1,1,1)}{\Phi_p(1,1,1)} + 1, \\ D_w &= \frac{\sum_{l,t,d} d^2R(l,t,d)}{\sum_{l,t,d} dR(l,t,d)} = \frac{\Phi_{nn}(1,1,1)}{\Phi_n(1,1,1)} + 1, \end{aligned} \right. \quad (11)$$

where  $L_w$ ,  $T_w$ , and  $D_w$  are the weight average compositions of linear, terminal, and dendritic units in a macromolecule.

The weighted average degree of polymerization ( $DP_w$ ) can therefore be estimated by Equation (12):

$$DP_w = \frac{\sum_{l,t,d} (2d+1+1)^2 R(l,t,d)}{\sum_{l,t,d} (2d+1+1) R(l,t,d)} = \frac{4\Phi_{nm}(1,1,1) + 4\Phi_{ns}(1,1,1) + \Phi_{ss}(1,1,1) + 6\Phi_d(1,1,1) + 2\Phi_s(1,1,1)}{2\Phi_n(1,1,1) + \Phi_s(1,1,1) + N} + 1 \quad (12)$$

The condition of  $DP_w \rightarrow \infty$ , which is equivalent to  $PDI \rightarrow \infty$  (where PDI is a polydispersity index), can be considered a gelation criterion. The degree of branching is defined as the ratio of an actual number of branched units to the maximum possible number of these units in a macromolecule. Here, the branched units are dendritic, so DB can be determined by the following Equation (13) [16]:

$$DB = \frac{2D}{2D + L} \quad (13)$$

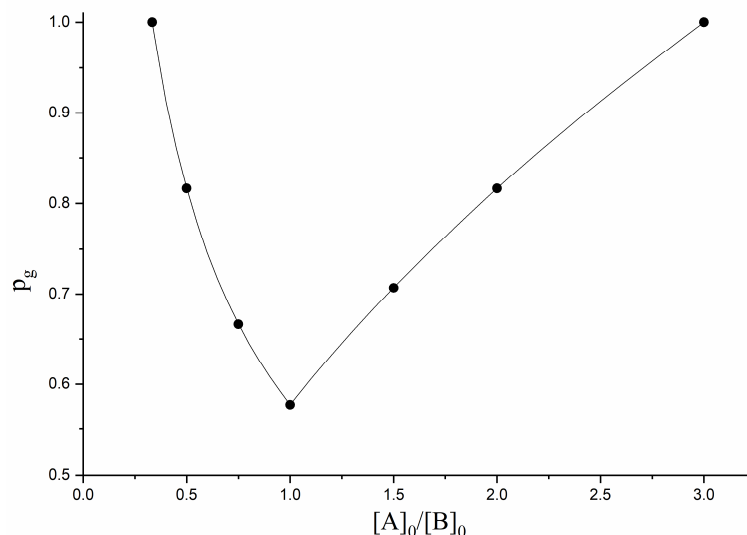
To conclude, the application of the structural kinetic model of  $AB_2+A_2+B_4$  monomer mixture polyaddition enables the study of how  $p_g$  and various structural and molecular weight characteristics are influenced by each reaction component, as well as by substitution effects, which were impossible to analyze in previous studies.

Nevertheless, at first, it is essential to provide the verification of the investigated model.

## 2.2. Verification of the Kinetic—Structural Model

The current model for  $AB_2+A_2+B_4$  monomer mixture polyaddition is quite versatile, encompassing all systems based on various combinations of the studied monomers, namely,  $A_2+AB_2$ ,  $AB_2+B_4$ ,  $AB_2$ , and  $A_2+B_4$ . This significantly expands the range of applications for the developed approach, enabling the use of well-known systems and solitary cases, such as  $A_2+B_4$ ,  $AB_2$ , and  $A_2+CB_2$ , for verification.

The  $A_2+B_4$  system is a subset of the  $A_n+B_m$  system, which was studied and described by Flory, resulting in Equation (1) [35]. Comparison of the data obtained through (1) and the data calculated using the offered approach (initial conditions are  $N = [B_4]_0$ ,  $[A_2] = [A_2]_0$ ,  $T = 2[B_4]_0$ ,  $\Phi_{pp} = 2[B_4]_0$ , others are equal to 0) is shown in Figure 2.

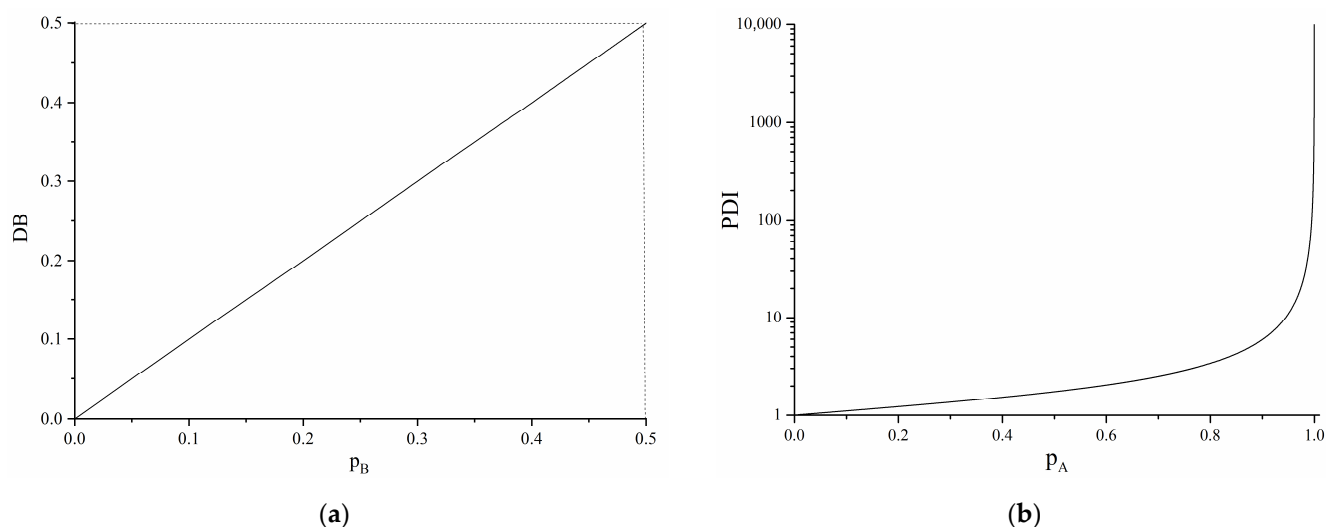


**Figure 2.** Plot of  $p_g$  as a function of  $[A]_0/[B]_0$  for  $A_2+B_4$  system. Solid line depicts the data obtained through Equation (1), and dots represent the data calculated by the offered approach ( $[AB_2]_0 = 0$ ).

As we can clearly see from Figure 2, there is a perfect correlation between data obtained through two different methods.

Another method of verification lies in reviewing well-studied systems—one of them is a solitary  $AB_2$ -type monomer. The variations in system characteristics calculated using

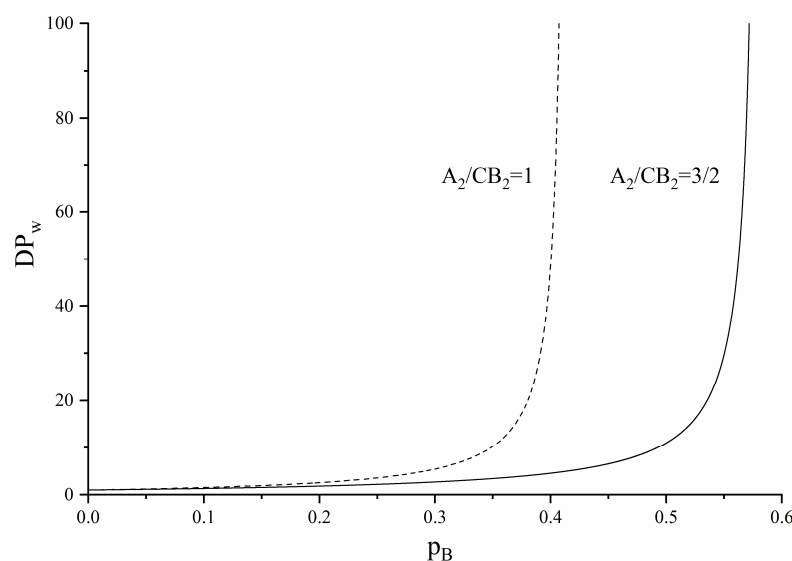
our method (with initial conditions set as  $N = [AB_2]_0$ ,  $T = [AB_2]_0$ , and the rest as zero) are illustrated in Figure 3.



**Figure 3.** Plot of DB as a function of  $p_B$  (a); plot of PDI as a function of  $p_A$  (b) in the  $AB_2$  monomer-based system ( $[AB_2]_0 = 1$ ,  $[A_2]_0 = [B_4]_0 = 0$ ).

Figure 3 shows that the maximum value of DB is 0.5 at  $p_B = 0.5$ , which corresponds to data from earlier papers [16]. Along with that, the gel point ( $PDI \rightarrow \infty$  or  $DP_w \rightarrow \infty$ ) is achieved at  $p_A \rightarrow 1$  ( $p_B \rightarrow 0.5$ ), which is the same as in a conventional Flory paper [15].

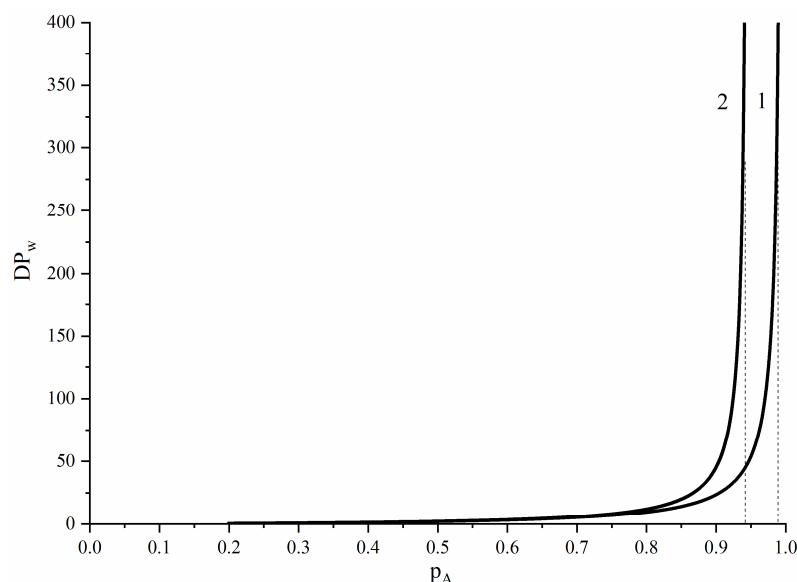
The validation of the comprehensive  $AB_2 + A_2 + B_4$  model, incorporating all constituents, involves comparing the results obtained with our model to those obtained from the following set of reactions:  $A_2 + CB_2 \rightarrow AB_2$  (rate constant  $k_c$ ) and  $AB_2 + CB_2 \rightarrow B_4$  (rate constant  $k_b$ ). For example, from [41], when  $k_c/k_b = 200$ , the  $p_g$  value equals 0.40 for the  $[A_2]_0/[CB_2]_0 = 1$  ratio and 0.56 for the  $[A_2]_0/[CB_2]_0 = 3/2$  ratio, respectively. If  $[A_2]_0/[CB_2]_0 = 1$ , the mixture of  $[AB_2]_0/[A_2]_0/[B_4]_0$  at a ratio of 2/1/1 is produced, whereas it is 4/4/1 for the  $[A_2]_0/[CB_2]_0 = 3/2$  case. The  $DP_w$  values for these mixture compositions, obtained with our suggested approach, are shown in Figure 4 and are similar to the ones specified in [41].



**Figure 4.** Plot of  $DP_w$  as a function of  $p_B$ , where the dashed line represents the  $[AB_2]_0/[A_2]_0/[B_4]_0 = 2/1/1$  ( $[A_2]_0/[CB_2]_0 = 1$ ) case, and  $[AB_2]_0/[A_2]_0/[B_4]_0 = 4/4/1$  ( $[A_2]_0/[CB_2]_0 = 3/2$ ) is for the solid line.



Experimental data confirm that the offered model describes the polyaddition of  $AB_2+A_2+B_4$  monomers properly. In [43],  $AB_2+A_2+B_4$  monomer mixtures of various compositions were synthesized, and it was determined experimentally that  $p_g$  value accounts for less than 1 in the range of  $[AB_2]_0/[A_2]_0/[B_4]_0$  ratios from 1/0.025/0.097 to 1/0.036/0.083. Figure 5 illustrates that the first case is characterized by a calculated  $p_g$  value of  $\sim 0.99$ , while for the second one, the calculated value equals  $p_g \sim 0.94$ .



**Figure 5.** Plot of  $DP_w$  vs.  $p_A$  when (1)  $[AB_2]_0/[A_2]_0/[B_4]_0 = 1/0.025/0.097$ , or (2)  $[AB_2]_0/[A_2]_0/[B_4]_0 = 1/0.036/0.083$ . Dashed lines correspond to the  $p_A$  values of 0.94 and 0.99.

Thus, the data obtained from various sources and the results of calculation using our suggestions matched perfectly. Based on that, it can be concluded that our structural kinetic model of the polyaddition of  $AB_2+A_2+B_4$  monomer mixture provides accurate results.

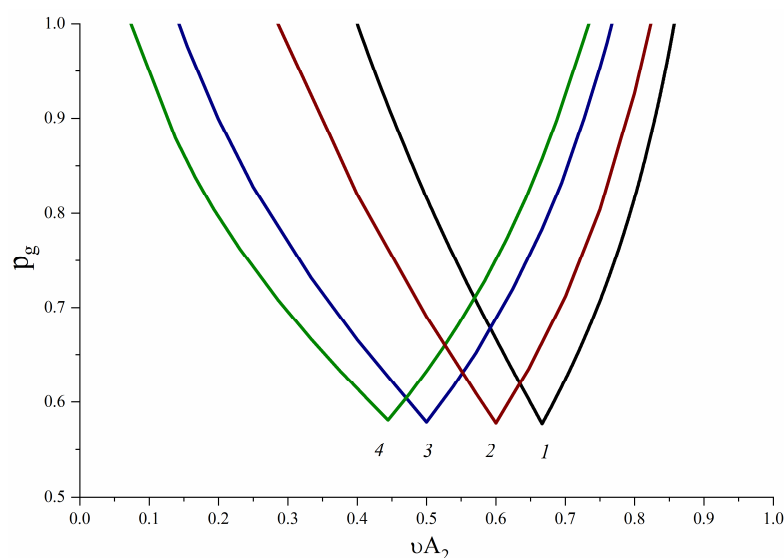
### 3. Results and Discussion

Using the proposed approach, it is possible to evaluate the effect of each constituent on both the structure and molecular weight parameters.

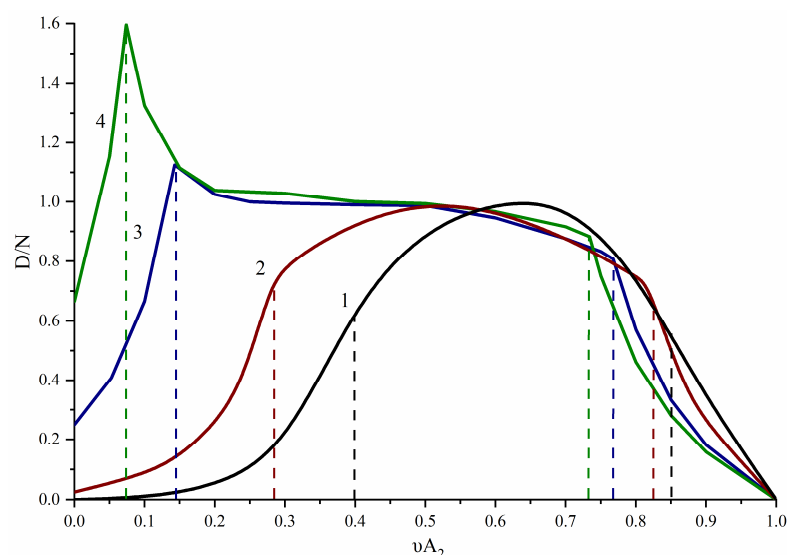
#### 3.1. $A_2$ -Type Monomer Effects

The  $p_g$  curves over the initial molar fraction of an  $A_2$ -type monomer ( $\nu A_2 = [A_2]_0 / ([AB_2]_0 + [A_2]_0 + [B_4]_0)$ ) at different  $[AB_2]_0/[B_4]_0$  ratios are shown in Figure 6.

The curves in Figure 6 reflect the conditions under which one can observe soluble systems transition to an insoluble state. Here, the condition for curve 1 is  $[AB_2]_0 = 0$ , indicating that it can be described by Equation (1). In other cases,  $[AB_2]_0 \neq 0$  (Figure 6 (2–4)), and therefore, a broadening of the Flory curve can be observed. Also, there is a distinct minimum at the  $[A]_0/[B]_0 = 1$  ratio in all the  $p_g$  vs.  $\nu A_2$  graphs. When the  $[A]_0/[B]_0$  value tends to deviate from 1 in either direction, an increase in  $p_g$  up to 1 is observed. The minimum point shifts towards lower  $\nu A_2$  values when an  $AB_2$ -type monomer is introduced into the system. At the same time, the  $p_g$  value at the minimum point is almost unaffected by changes in the  $[AB_2]_0/[B_4]_0$  ratio and remains approximately  $(1/3)^{1/2}$ . To understand the reasons for these observed patterns, it is necessary to analyze how  $\nu A_2$  affects the specific number of branches per macromolecule ( $D/N$ ) (Figure 7). Hereinafter, the values of  $p_g$  at the corresponding values of  $\nu A_2$  were used to calculate the  $D/N$ .



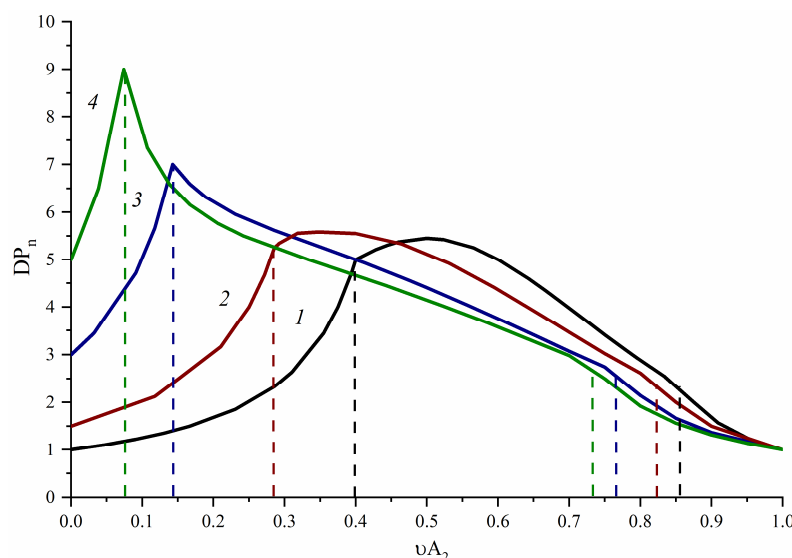
**Figure 6.** Plot of  $p_g$  as a function of  $\nu A_2$ , where (1)  $[AB_2]_0/[B_4]_0 = 0$  (a curve derived from Flory equation); (2)  $[AB_2]_0/[B_4]_0 = 0.5$ ; (3)  $[AB_2]_0/[B_4]_0 = 2$ ; and (4)  $[AB_2]_0/[B_4]_0 = 4$ .



**Figure 7.** Plot of specific number of branches per macromolecule ( $D/N$ ) at  $p_g$  vs.  $\nu A_2$  when (1)  $[AB_2]_0/[B_4]_0 = 0$  (Flory curve); (2)  $[AB_2]_0/[B_4]_0 = 0.5$ ; (3)  $[AB_2]_0/[B_4]_0 = 2$ ; and (4)  $[AB_2]_0/[B_4]_0 = 4$ . Dashed lines correspond to the points where  $p_g \leq 1$ .

It can be observed in Figure 7 (1) that for the polyaddition of  $A_2+B_4$  monomers, the specific number of branches per macromolecule increases with the growth of  $\nu A_2$  until it reaches 1, corresponding to a minimum of the  $p_g$  vs.  $\nu A_2$  function (Figure 6). As expected, it then begins to decrease. Thus, the minimum  $p_g$  value is reached when  $D/N = 1$ .

The Introduction of the  $AB_2$ -type monomer into the system leads to an increase in the  $D/N$  growth rate over  $\nu A_2$ . The maximum  $D/N$  value possible is 1 when  $[AB_2]_0/[B_4]_0 < 1$  (Figure 7 (2)), whereas it exceeds 1 at  $[AB_2]_0/[B_4]_0 > 1$  (Figure 7 (3,4)). Furthermore, the function reaches its maximum when  $p_g \leq 1$ . However, the introduction of the  $AB_2$ -type monomer does not affect the condition under which  $p_g$  reaches its minimum at  $\sim(1/3)^{1/2}$ , which is observed at  $D/N = 1$ . Thus, introducing the  $AB_2$ -type monomer into the  $A_2+B_4$  system results in an increase in the  $D/N$  of the homo-polyaddition of the  $AB_2$ -type monomer and its interaction with the  $B_4$ -type monomer. The mentioned process does not lead to the crosslinking of macromolecules and contributes only to an increase in the degree of polymerization, as indicated by the  $DP_n$  vs.  $\nu A_2$  plots shown in Figure 8.



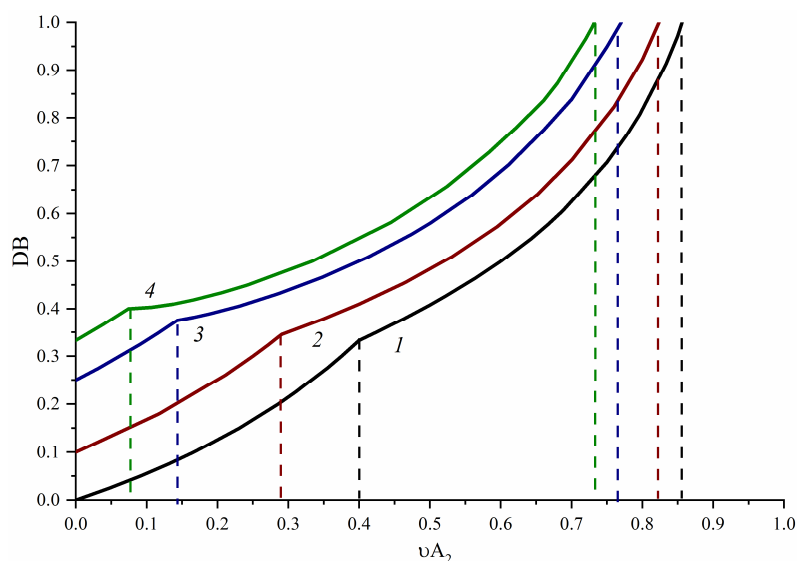
**Figure 8.** Plot of  $DP_n$  at  $p_g$  as a function of  $\nu A_2$ : (1)  $[AB_2]_0/[B_4]_0 = 0$  (Flory curve); (2)  $[AB_2]_0/[B_4]_0 = 0.5$ ; (3)  $[AB_2]_0/[B_4]_0 = 2$ ; and (4)  $[AB_2]_0/[B_4]_0 = 4$ . Dashed lines correspond to the points where  $p_g \leq 1$ .

In the case of polyaddition, the molecular weight of the product depends heavily on the ratio of the groups that are involved in the reaction, and also, the highest molecular weight polymer can only be obtained under equimolar conditions. Another factor affecting the molecular weight is the conversion of functional groups. The effect of conversion on the MW is often complex in nature. In any case, it is obvious that the degree of reaction completion is essential to obtaining a high-molecular-weight polymer.

Where the polyaddition of a binary mixture of  $A_2+B_4$  monomers is concerned, there is a correlation between achieving equimolar conditions, a functional group conversion, and the molecular weight of the final product. Due to this, a broad peak is present on the graph of the degree of polymerization as a function of  $\nu A_2$  (Figure 8 (1)). The introduction of an  $AB_2$ -type monomer into the system results in shifting the peak (Figure 8 (2)) towards the  $[A]_0/[B]_0 < 1$  area. A further increase in this part of the  $AB_2$ -type monomer in the system causes the highest MW to be achieved only when the conversion approaches 1, thereby sharpening the peak (Figure 8 (3,4)). Thus, the increase in  $\nu AB_2$  in the  $AB_2+A_2+B_4$  system significantly enhanced the  $DP_n$  of the final polymer from 5 to 9, with  $[AB_2]_0/[B_4]$  changing from 0 to 4; also,  $\nu AB_2 \rightarrow 1$ , and  $DP_n \rightarrow \infty$ .

As expected, a monotonic increase in DB is observed in the curves illustrating its variation over  $\nu A_2$ , as depicted in Figure 9, up to  $p_g \leq 1$ . The inflection point indicates the gelation onset. Figure 9 shows that the introduction of  $AB_2$ -type monomer facilitates the DB growth.

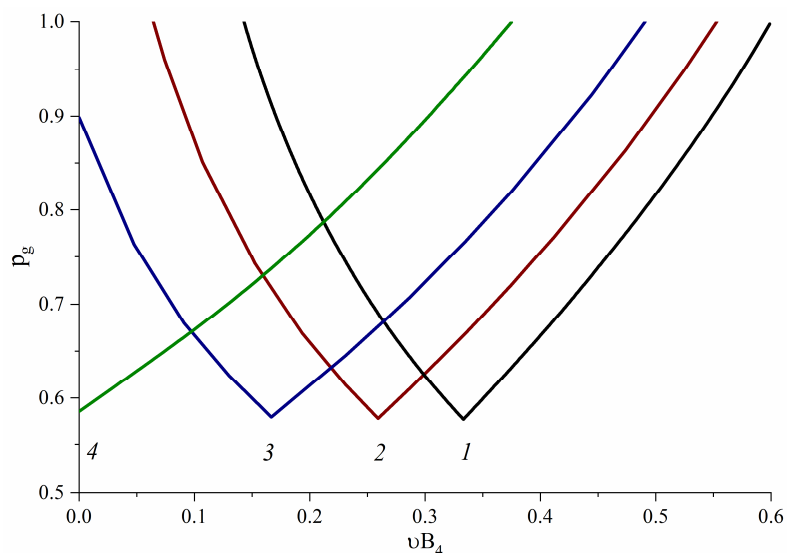
Generally, hyperbranched polymers exhibit a  $DB \geq 0.4$ . This value can be reached with all the ratios used within this work. However, when  $[AB_2]_0/[B_4]_0 < 4$  (Figure 9 (1–3)), the DB value reaches 0.4 beyond the inflection point, that is, when  $p_g < 1$  (and when  $DP_n$  reaches its highest values). On the other hand, at  $[AB_2]_0/[B_4]_0 \geq 4$ , fully soluble hyperbranched polymers with  $DB = 0.4$  can be obtained (Figure 9 (4)). The highest DB that is possible for the polyaddition of an  $AB_2$ -type monomer is 0.5. However, HBPs with  $DB > 0.5$  can be obtained using a mixture of  $AB_2+A_2+B_4$  monomers. The point is that the application of the monomer mixtures that can potentially help reach  $DB \geq 0.4$  results in a decrease in the molecular weight characteristics of the final product compared to the polyaddition of an  $AB_2$ -type monomer.



**Figure 9.** Plot of DB at  $p_g$  as a function of  $\nu A_2$ : (1)  $[AB_2]_0/[B_4]_0 = 0$ ; (2)  $[AB_2]_0/[B_4]_0 = 0.5$ ; (3)  $[AB_2]_0/[B_4]_0 = 2$ ; and (4)  $[AB_2]_0/[B_4]_0 = 4$ . Dashed lines correspond to the points where  $p_g \leq 1$ .

### 3.2. $B_4$ -Type Monomer Effects

The next important stage involves investigating how a  $B_4$ -type monomer affects the formation of hyperbranched polymers during the polyaddition of the  $AB_2+A_2+B_4$  monomer mixture. Figure 10 shows that, as in the previous case, the curves of  $p_g$  over the initial molar fraction of a  $B_4$ -type monomer ( $\nu B_4 = [B_4]_0/([AB_2]_0 + [A_2]_0 + [B_4]_0)$ ) tend to broaden when the  $AB_2$ -type monomer is introduced into the system. Also, a distinctive minimum is observed on each curve at  $[A]_0/[B]_0 = 1$  for all  $[AB_2]_0/[A_2]_0$  ratios (Figure 10).



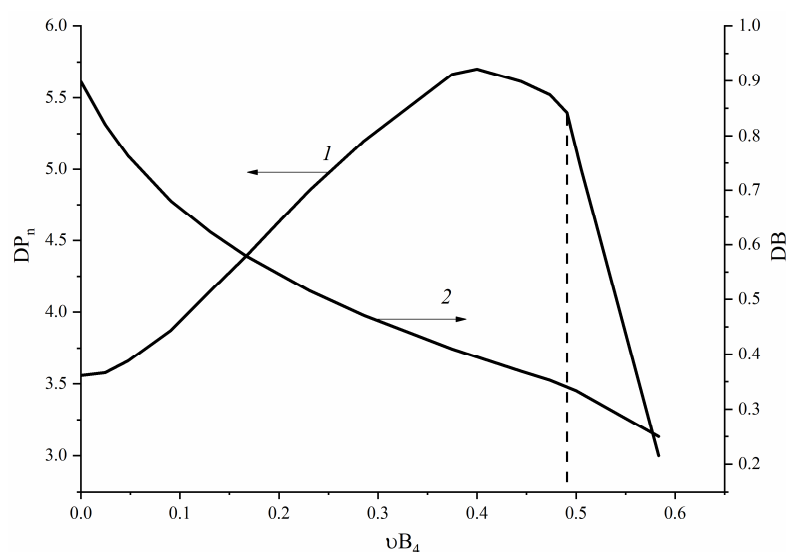
**Figure 10.** Graph of  $p_g$  as a function of  $\nu B_4$ , when (1)  $[AB_2]_0/[A_2]_0 = 0$  (Flory curve); (2)  $[AB_2]_0/[A_2]_0 = 1/4$ ; (3)  $[AB_2]_0/[A_2]_0 = 2/3$ ; and (4)  $[AB_2]_0/[A_2]_0 = 2$ .

When the polyaddition of the  $AB_2+A_2+B_4$  monomer mixture takes place, a  $B_4$ -type monomer can be introduced into a macromolecule as a linear (when two B-groups in the monomer have reacted) or tri- (when three B-groups in the monomer have reacted) or tetrafunctional (when four B-groups in the monomer have reacted) branching unit. Figure 10 demonstrates that an increase in  $\nu B_4$  results in a decrease in  $p_g$  when  $[A]_0/[B]_0 > 1$ .

This can be explained by an excess of A groups in the system within this range. Here, a B<sub>4</sub>-type monomer is introduced to a macromolecule mainly as a polyfunctional branching unit.

Same as the A<sub>2</sub>-type monomer does, it leads to an increase in the number of branches per macromolecule. A further increase in  $\nu B_4$  causes a decrease in both the absolute and specific number of branches per macromolecule, which is associated with the growth of a free B group amount. As a result, the possibility of forming a three-dimensional grid is significantly diminished. The decrease in the number of branches per macromolecule is related to a decrease in the number of reactive A groups. The latter causes an increase in the number of macromolecules, resulting in the trend for short-chain linear polymers to form.

Thus, subject to  $[A]_0/[B]_0 > 1$ , a B<sub>4</sub>-type monomer is introduced to a chain mainly as a polyfunctional branching unit; in other words, it acts as a core for a macromolecule to form and grow. Meanwhile, at  $[A]_0/[B]_0 < 1$ , the monomer is introduced primarily as a linear unit and, eventually, terminates the growing polymer chain (Figure 11).



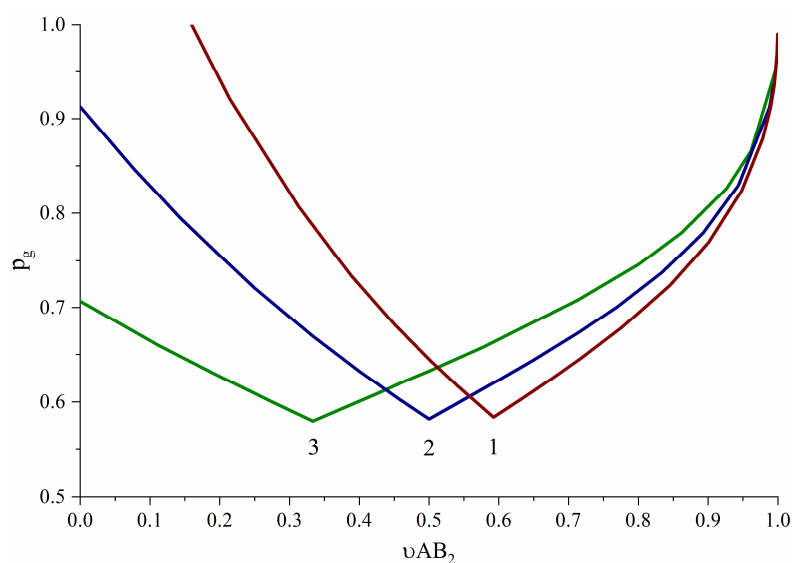
**Figure 11.** Plot of  $DP_n-1$  and  $DB-2$  vs.  $\nu B_4$ , with  $[AB_2]_0/[A_2]_0 = 2/3$ , and conversion is equal to  $p_g$ . Dashed line corresponds to the point where  $p_g \leq 1$ .

The graph of  $DP_n$  and  $DB$  vs.  $\nu B_4$  is illustrated in Figure 11. As with the A<sub>2</sub>-type monomer, the  $DP_n$  curve goes through a maximum. However, for the  $[AB_2]_0/[A_2]_0 = 2/3$  ratio, we can see a broad peak that is related to the area where the gelation is observed. The  $DB$  decreases with an increasing  $\nu B_4$  due to a decline in the number of cross-linked units. Thus, when no gelation occurs, hyperbranched polymers with B end groups can be obtained, with  $DB = 0.34$  and  $DP_n = 5.4$ . These characteristic values are not much higher compared to the polyaddition of the A<sub>2</sub>+B<sub>4</sub> monomer mixture ( $DB = 0.33$  and  $DP_n = 5.0$ ).

### 3.3. AB<sub>2</sub>-Type Monomer Effects

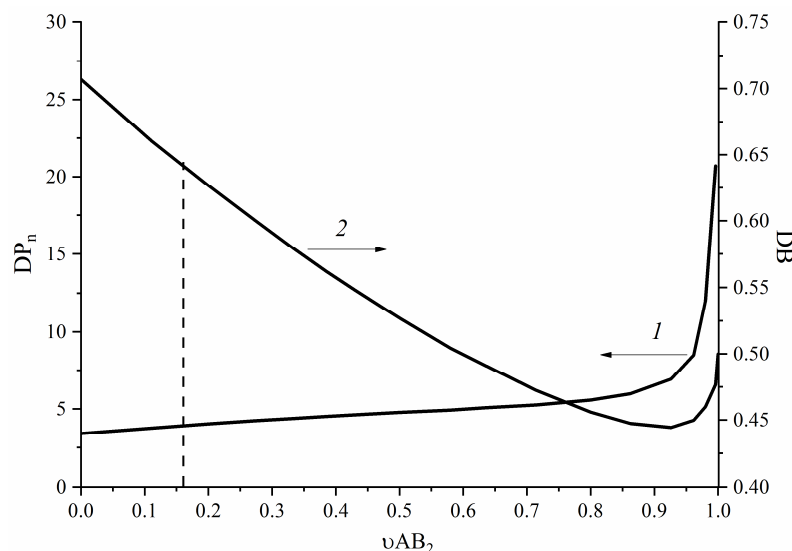
The plot of  $p_g$  over the initial molar fraction of the AB<sub>2</sub>-type monomer ( $\nu AB_2 = [AB_2]_0/([AB_2]_0 + [A_2]_0 + [B_4]_0)$ ) is of particular interest (Figure 12). In contrast to the two cases above, there are no distinctive points at which gelation would not be observed, when  $[A]_0/[B]_0 > 1$ . The  $p_g \rightarrow 1$  only when  $\nu AB_2 \rightarrow 1$ , which corresponds to the data from [15]. The minimum of the function is also observed at  $[A]_0/[B]_0 = 1$ , and shifting from equimolar conditions results in an increase in  $p_g$ . The  $p_g$  value decreases with an increase in  $\nu AB_2$  when  $[A]_0/[B]_0 > 1$ . The reason lies in the fact that under these conditions, an AB<sub>2</sub>-type monomer can be introduced into the chain mainly as a trifunctional unit, thereby increasing the number of these units per macromolecule and causing a decrease in  $p_g$ . On the other hand, with an excess of B groups ( $[A]_0/[B]_0 < 1$ ), an increase in the AB<sub>2</sub> monomer content promotes an increase in the number of terminal and linear units in

a macromolecule. Thus, an AB<sub>2</sub>-type monomer can be introduced in a growing polymer chain both as a trifunctional and as a linear unit.



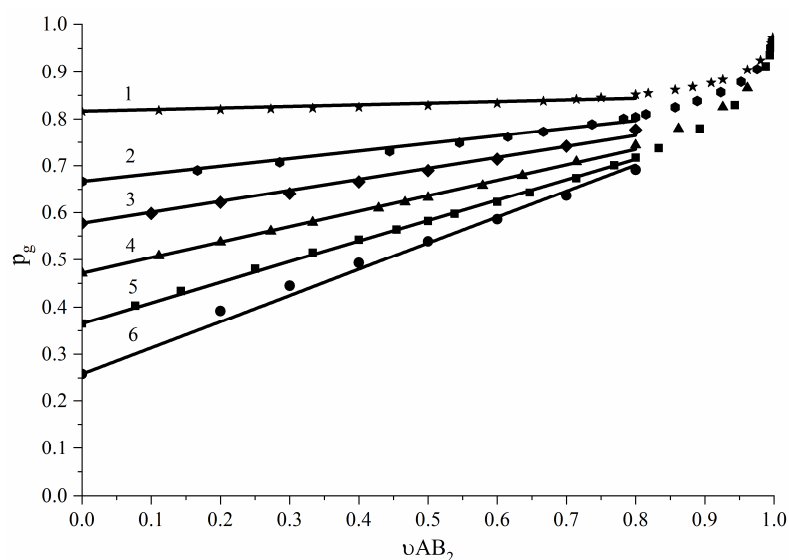
**Figure 12.** Plot of  $p_g$  vs.  $\nu AB_2$  at (1)— $[A_2]_0/[B_4]_0 = 3$ ; (2)  $[A_2]_0/[B_4]_0 = 5$ ; and (3)  $[A_2]_0/[B_4]_0 = 10$ .

The plots of  $DP_n$  and  $DB$  vs.  $\nu AB_2$  are shown in Figure 13. In contrast to all of the aforementioned options, a monotonic increase in  $DP_n$  is observed with an increase in  $\nu AB_2$  over the entire range. Moreover, the curves appear to be almost linear up to  $\nu AB_2 \sim 0.90$  due to the contribution of each component of the  $AB_2 + A_2 + B_4$  monomer mixture to the polyaddition process. Nevertheless, a further increase in  $\nu AB_2$  leads to an exponential increase in  $DP_n$ , associated with a negligible contribution of  $A_2$ - and  $B_4$ -type monomers compared to the  $AB_2$  type. The  $DB$  graph reaches its lowest value and then tends to grow at  $\nu AB_2 \sim 0.90$  for the exact same reasons.



**Figure 13.** Plot of  $DP_n-1$  and  $DB-2$  vs.  $\nu AB_2$  with  $[A_2]_0/[B_4]_0 = 3$ ; conversion is equal  $p_g$ . Dashed line corresponds to the point where  $p_g \leq 1$ .

As indicated above, the Flory Equation (1) for  $p_g$  determination is relevant solely for the polyaddition of  $A_n + B_m$  monomers, without taking the  $AB_2$ -type monomer effect into account. To figure out how  $p_g = p_A$  can be influenced by the composition of the  $AB_2 + A_2 + B_4$  monomer mixture, the curves of  $p_g = p_A$  vs.  $\nu AB_2$  were plotted for a range of the  $[A_2]_0/[B_4]_0$  ratio of 1–10 (Figure 14).



**Figure 14.** Plot of  $p_g = p_A$  as a function of  $vAB_2$  at  $[A_2]_0/[B_4]_0$  ratio equal to (1) 1; (2) 3/2; (3) 2; (4) 3; (5) 5; and (6) 10.

Figure 14 demonstrates that each graph here can be accurately described by the linear equation  $p_g = p_A = a \times vAB_2 + b$ , where  $vAB_2$  ranges between 0 and 0.8.

The constant term ( $b$ ) can be determined using the Flory Equation (1) at  $vAB_2 = 0$ . Due to the fact that the parameters  $\alpha$  and  $\rho$  are constants for every single case of polyaddition, the correlation between  $p_g = p_A$  and the parameter  $r = [A]_0/[B]_0$  will appear as (14). Therefore, the curve of the constant term ( $b$ ) vs.  $([B]_0/[A]_0)^{1/2}$  should be linear (see Figure S1a in Supporting Information). Here,  $[A]_0$  and  $[B]_0$  represent A and B groups from  $A_2$  and  $B_4$ , respectively.

$$p_g = p_A = \sqrt{\frac{\alpha}{r(\rho + \alpha(1 - \rho))}} \sim \sqrt{\frac{1}{r}} \sim \sqrt{\frac{[B]_0}{[A]_0}} \quad (14)$$

The slope coefficient ( $a$ ) appears to be influenced by an  $AB_2$ -type monomer introduction; however, the relationship between  $a$  and  $([B]_0/[A]_0)^{1/2}$  also exhibits linearity (see Figure S1b in Supporting Information).

Thus, we can estimate the  $p_g = p_A$  value during the polyaddition of the  $AB_2 + A_2 + B_4$  monomer mixture through the following Equation (15):

$$p_g = p_A = (-0.53([B]_0/[A]_0)^{1/2} + 0.78)vAB_2 + (1/3)^{1/2}([B]_0/[A]_0)^{1/2} \quad (15)$$

where  $(1/3)^{1/2} \times ([B]_0/[A]_0)^{1/2}$  is Equation (1) for the polyaddition of the  $A_2 + B_4$  monomer mixture,  $[A]_0$  and  $[B]_0$  represent the content of A and B groups from  $A_2$  and  $B_4$ , respectively. The equation allows for the accurate calculation of the  $p_g = p_A$  value when  $vAB_2$  is up to 80%.

One of the most significant advantages of the invented model is an opportunity to calculate structural and molecular weight properties while considering substitution effects (Scheme 3).

### 3.4. Substitution Effects

Let us simulate the case of a monomer mixture polyaddition when  $[AB_2]_0/[A_2]_0/[B_4]_0 = 0.63/0.060/0.31$ , based on  $A_2 + B'B_2$  and  $A_2 + CB_2$  polyaddition cases. The impact of the  $k_2/k_1$  ratio on the structural and molecular weight parameters of the hyperbranched polymers that are obtained under these conditions is illustrated in Figures S2 and S3 (Supporting Information), respectively.

As we can see from Figure S2 (Supporting Information), the negative substitution effect leads to  $DB \rightarrow 0$ . That is, the topological mechanism of the macromolecule formation changes drastically, resulting in the formation of weakly branched polymers with numerous side-chained B groups. It seems nearly impossible to obtain hyperbranched polymers under these conditions. On the contrary, when  $k_2/k_1 > 1$ , the possibility of forming knots increases the same way that the ratio does, causing an increase in the DB.

As we expected,  $DP_n$  is unaffected by the presence of the substitution effect (see Figure S3 in Supporting Information). It is evident that, when no gelation occurs, the  $k_2/k_1$  ratio has no impact on the completion of the process. We can conclude that  $DP_n$  is indifferent to the unequal reactivity of groups, unlike  $DP_w$ . As the  $k_2/k_1$  ratio grows, an increase in the possibility of generating dendritic units can be observed. Thus, there is a higher chance of obtaining high-molecular-weight macromolecules, causing  $DP_w$  to increase.

The derived regularities are expected for any values of the  $[A_2]_0/[AB_2]_0/[B_4]_0$  ratio. However, each component of the system has a different impact on the forming of hyperbranched polymers.

A joint influence of the substitution effect and  $\nu A_2$  on  $p_g$ , when  $[AB_2]_0/[B_4]_0 = 2$ , is shown in Figure 15. It illustrates that the positive substitution effect, i.e., when  $k_2/k_1 > 1$ , leads to a decrease in  $p_g$  compared to the statistical polyaddition of an  $AB_2+A_2+B_4$  monomer mixture. For instance, if  $\nu A_2 = 0.14$  and  $k_2/k_1 = 1$ ,  $p_g$  takes a value of 1, whereas it reaches 0.86 when  $k_2/k_1 = 10$ . Both positive and negative substitution effects modify the topological mechanism of macromolecule formation. At the initial stage of the polyaddition of an  $AB_2+A_2+B_4$  monomer mixture, when  $k_2/k_1 > 1$ , macromolecules with numerous dendritic units are mainly formed. These macromolecules are characterized by an enhanced content of B groups, which act as cross-linking centers, causing them to form a three-dimensional mesh. In contrast, when the negative substitution effect ( $k_2/k_1 < 1$ ) takes place, the formation of polymers with numerous linear units is primarily observed during the entire process. This is attributed to the lower reactivity of B groups within linear fragments that is characteristic of this specific case. Therefore, the cross-linked polymer is less likely to form compared to the statistical polyaddition of the  $AB_2+A_2+B_4$  monomer mixture.

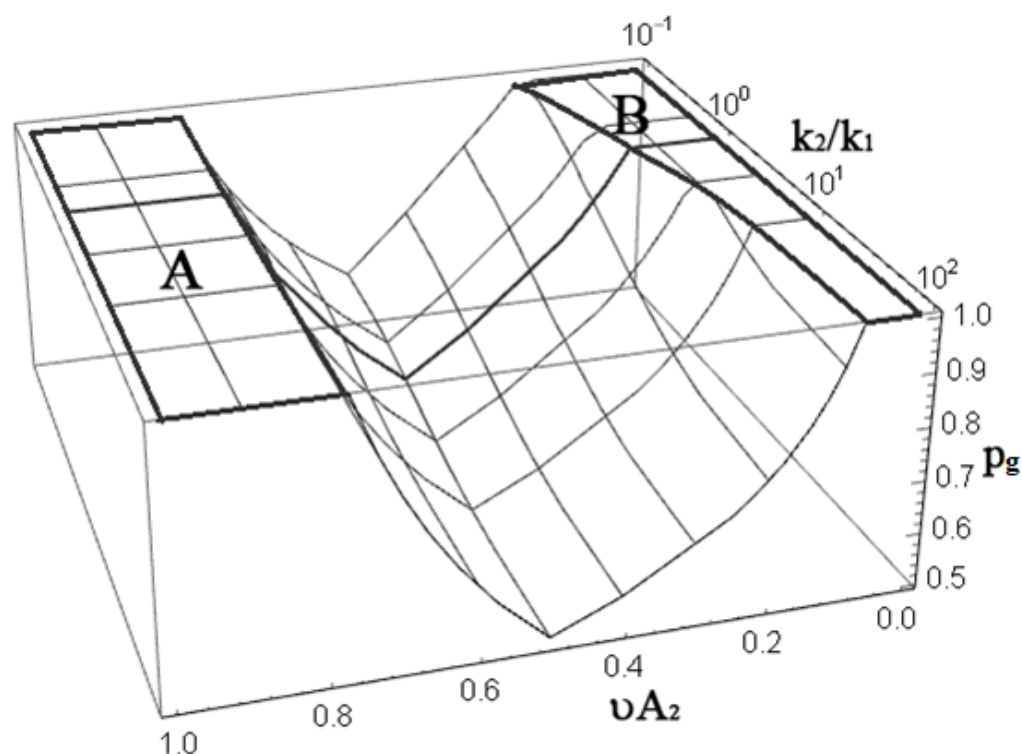


Figure 15. Plot of  $p_g$  vs.  $\nu A_2$  and  $k_2/k_1$  if  $[AB_2]_0/[B_4]_0 = 2$ .



When  $p_g$  reaches 1, an inflection appears in the surface of the graph due to the cessation of changes in  $p_g$ . Thus, we can define an area in the graph that is depicted in Figure 15, which is limited by inflection points where  $\nu A_2$  and  $k_2/k_1$  can be adjusted freely, named the ‘sustainability area’. There are no restrictions imposed on the polyaddition of the  $AB_2+A_2+B_4$  monomer mixture and associated with the gelation process in the so-called ‘sustainability area’, since the formation of a three-dimensional spatial network here is impossible. With  $\nu A_2$  values being high, fully branched polymers with terminal A groups and relatively low  $DP_n$  values can be produced, as indicated by the relations derived above. On the other hand, for lower  $\nu A_2$  values, we can obtain hyperbranched polymers with terminal B groups, exhibiting a DB close to or exceeding 0.5 and a relatively high molecular weight. Similar plots can be derived for each monomer in the  $AB_2+A_2+B_4$  ternary system. Thus, by varying the component composition and/or  $k_2/k_1$ , it is possible to define a range of the system parameter values where soluble products with predefined structural and molecular weight parameters are formed consistently.

#### 4. Conclusions

A new structural kinetic model of the polyaddition of an  $AB_2+A_2+B_4$  monomer mixture was designed within this work in order to predict the impact of the composition of the monomer mixture on the structural (DB) and molecular weight ( $DP_n$ ,  $DP_w$ ) characteristics of HBP, as well as  $p_g$ . The suggested model also considers a positive or negative substitution effect to occur during the polyaddition. The relevance of the polyaddition description for the  $AB_2+A_2+B_4$  system was verified by the interaction of well-defined systems, like  $A_2+B_4$ ,  $AB_2$ , and  $A_2+CB_2$ . Furthermore,  $p_g$  values obtained using the proposed model are in agreement with the experimental data that are derived from the scientific sources that are dedicated to the polyaddition of  $AB_2+A_2+B_4$  monomers.

Using the suggested model, the influence of both the component’s composition and the substitution effect during the polyaddition of  $AB_2+A_2+B_4$  monomers on the structural and molecular weight characteristics of hyperbranched polymers was investigated.

It was shown that with an increase in the  $A_2$ -type monomer content in the ternary system under study, the value of  $p_g$  decreases. This is also accompanied by an increase in  $DP_n$  and DB as a result of the cross-linking of macromolecules formed at the initial stages, containing B groups in terminal and linear units. The introduction of a  $B_4$ -type monomer into the  $AB_2+A_2$  monomer system also leads to a decrease in the  $p_g$  value, accompanied by an increase in  $DP_n$  and a decrease in DB, as a result of the cross-linking of macromolecules that are also formed at the initial stages, containing terminal A groups. In both cases, the maximum values of  $DP_n$  and DB belong to the area where  $[A]_0/[B]_0 < 1$ . It should be noted that the effect of the monomers of the  $A_2$  and  $B_4$  type on  $DP_n$  is extreme. However, when an  $AB_2$ -type monomer is introduced into the  $A_2+B_4$  system, the  $DP_n$  value increases over the entire concentration scale. On the contrary, the DB value decreases to a certain limit when the  $AB_2$  monomer concentration approaches 90%, after which it begins to increase. Thus, when the amount of  $AB_2$ -type monomers is less than 90%, the contribution of each constituent of the  $AB_2+A_2+B_4$  system to polyaddition is comparable. In contrast, with an  $AB_2$  monomer content exceeding 90%, the contribution of the  $A_2$  and  $B_4$  types of monomers becomes negligible.

Based on our results, an empirical formula has been proposed for estimating  $p_g$  for the polyaddition of an  $AB_2+A_2+B_4$  monomer mixture:  $p_g = p_A (-0.53([B]_0/[A]_0)^{1/2} + 0.78)\nu AB_2 + (1/3)^{1/2}([B]_0/[A]_0)^{1/2}$ , where  $(1/3)^{1/2}([B]_0/[A]_0)^{1/2}$  represents a Flory equation for the case of  $A_2+B_4$  polyaddition;  $[A]_0$  and  $[B]_0$  are concentrations of groups A and B from  $A_2$  and  $B_4$ , respectively; and  $\nu AB_2$  represents the mole fraction of  $AB_2$ -type monomers in the mixture. The resulting equation is able to predict precisely the  $p_g$  value at  $AB_2$  monomer contents up to 80%.

The presence of ‘sustainability areas’ is shown, where it is possible to freely vary all the system variables and to obtain soluble hyperbranched polymers with various sets of the functional end groups.

It is revealed that the range of initial monomer ratios, where soluble products of the highest molecular weight possible can be obtained, increases in case of a negative substitution effect. Moreover, linear polymers with side-chained B groups tend to form. As the negative effect of substitution increases, the degree of branching approaches 0. In contrast, the positive substitution effect is accompanied by the trend to form polymers with more functional groups in terminal units, with the degree of branching approaching 1. In this case, however, a narrowing of the ‘sustainability area’ occurs.

**Supplementary Materials:** The following supporting information can be downloaded at <https://www.mdpi.com/article/10.3390/polym16030426/s1>: Figure S1: Plot of the constant term  $b$  (a) and the slope coefficient  $a$  (b) as a function of  $([B_0]/[A_0])^{1/2}$ . Figure S2: Plot of DB vs.  $k_2/k_1$ ; the ratio of monomer mixture polyaddition  $[AB_2]_0/[A_2]_0/[B_4]_0 = 0.63/0.060/0.31$ . Figure S3: Plot of  $DP_n-1$  and  $DP_w-2$  vs.  $k_2/k_1$  ratio during the polyaddition of the monomer mixture  $[AB_2]_0/[A_2]_0/[B_4]_0 = 0.63/0.060/0.31$ .

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