



# *Review* **Development and Recent Progress of Hoses for Cryogenic Liquid Transportation**

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**Abstract:** Recently, the application of cryogenic hoses in the field of cryogenic media has become a hot topic, especially in the industry of offshore liquefied natural gas and aerospace field. However, the structure of cryogenic hoses is complex, and reasonable structural properties are required due to the harsh working conditions. There is still plenty of scope for further development to improve the performance in all aspects. In this paper, the current development status of cryogenic hoses for liquefied natural gas (LNG) transportation is reviewed first, including the types, manufacturers, structural forms, performance, and key technical challenges. And then, the recent progress and prospect of cryogenic hoses for cryogenic liquid transportation (such as LNG and liquid oxygen) are summarized, including structure design, low-temperature resistant polymers, liquid oxygen compatible polymers, and leakage monitoring technologies. This paper provides a comprehensive overview of the research development and application of cryogenic hoses. Moreover, future research directions have been proposed to facilitate its practical applications in aerospace.

**Keywords:** cryogenic hoses; liquefied natural gas; liquid oxygen; cryogenic liquid transportation

# **1. Introduction**

Cryogenic hoses are extensively utilized in the aerospace, maritime transportation, and other industries for the transportation and refueling systems of cryogenic liquid fuels or media. These hoses are mainly divided into two major types, including metal corrugated hoses and cryogenic composite hoses based on thermoplastic materials and metal reinforcement wires [\[1,](#page-11-0)[2\]](#page-11-1). Metal corrugated hoses possess the advantages of mature technology, low costs, and high safety, so it is widely used  $[3,4]$  $[3,4]$ . However, they have drawbacks such as heavy weight, large bending radius, low flexibility, and difficulty in aligning during pipe connections [\[5,](#page-12-1)[6\]](#page-12-2). On the other hand, cryogenic composite hoses, with their lightweight nature, small bending radius, and easy pipe connections, effectively address the challenges associated with metal hoses [\[7](#page-12-3)[,8\]](#page-12-4). However, the reliability issues due to the low-temperature embrittlement of polymer materials and compatibility problems with certain super lowtemperature media such as liquid oxygen (LOX) restrict their applications in the field of super low-temperature media like liquid hydrogen and liquid oxygen.

Currently, cryogenic composite hoses are only gradually used in offshore liquefied natural gas (LNG, -162 °C) systems [\[9\]](#page-12-5). In the field of offshore LNG, Metal corrugated hoses are only competent for offshore LNG operations in favorable sea conditions, greatly restricting operational times [\[10](#page-12-6)[,11\]](#page-12-7). In contrast, cryogenic composite hoses, known for their flexibility, corrosion resistance, lightweight, and easy operation, have been increasingly employed in offshore LNG systems [\[12–](#page-12-8)[14\]](#page-12-9). This allows for the safe completion of LNG



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transport and loading/unloading operations between ships and platforms even in harsh sea conditions [\[15–](#page-12-10)[17\]](#page-12-11).  $\frac{1}{2}$  and  $\frac{1}{2}$  and  $\frac{1}{2}$ . The possibility of  $\frac{1}{2}$  and  $\frac{1}{2}$  and  $\frac{1}{2}$  and  $\frac{1}{2}$ 

of different businesses, including the types, structural forms, structural forms, structural characteristics,

At present, many businesses and scholars have launched the research and development of cryogenic hoses. There are many models and types of cryogenic hoses and each has its own characteristic. In this paper, we provide a detailed introduction to the products of different businesses, including the types, structural forms, structural characteristics, and and advancement. key technical challenges. At the same time, we pointed out some technical challenges and also proposed corresponding solutions. In addition, we further explored the possibility of the development of cryogenic composite hoses for liquid oxygen (LOX). And, the testing of some materials that might be used in cryogenic composite hoses for LOX has been completed, which lays the foundation for further research. Finally, some suggestions are given about the particular directions for further research and advancement.

# 2. The Types of Cryogenic Hoses **primarily applied to one LNG transports**

Cryogenic hoses can be categorized according to the transported media, including LNG hoses, liquid oxygen hoses, liquid hydrogen hoses, liquid nitrogen hoses, and so on. Currently, Cryogenic hoses designed for the high-flow transport of cryogenic liquids are primarily applied to offshore LNG transport. The design and manufacturing of cryogenic hoses for LNG operations at sea are mainly guided by the BS EN ISO 20257 [\[18](#page-12-12)[,19\]](#page-12-13). This polymer braided materials wound into a multilayer wall structure called cryogenic comstandard outlines the design requirements and test criteria that LNG hoses must fulfill. The extractive the accept requirements and test entertainments and the metal correct metal corrust relationship. form: one is metal corrugated hoses and another with the wall made of polymer films and polymer braided materials wound into a multilayer wall structure called cryogenic composite hoses [7]. The metal corrugat[ed](#page-12-3) hoses are further categorized into reinforced metal corrugated hoses and high vacuum metal corrugated hoses, specifically [\[20\]](#page-12-14).

# 2.1. The Reinforced Metal Corrugated Hoses **and The anti-leakage layers**

According to the specifications of EN1474-2-2008, reinforced metal corrugated hoses are primarily composed of three anti-leakage layers, two insulation layers, an armored layer, a spiral layer, and a metal corrugated tube lining layer  $[13]$ , as shown in Figure 1. The configuration, the number of layers, and the stacking method of these layers can be  $\frac{1}{2}$ determined based on the specific working conditions. The lining layer, a thin-walled metal corrugated tube made of stainless steel solves leakage issues and provides support for the internal pressure loads. The armored layer not only bears axial loads but also provides a certain level of insulation  $[21,22]$ . The spiral layer serves to determine the position of the armored layer and offers radial support. To effectively prevent heat transfer, at least one insulation layer is needed to act as thermal protection  $[23]$ . These insulation layers are helpful to prevent the external icing of the hoses during work and ensure that the internal temperature of the hose is stabilized.

<span id="page-1-0"></span>

1, 3, 7. Anti-leakage layers, 2, 4. Insulation layers, 5. Spiral layer, 6. Armored layer, 8. Metal corrugated tube lining.

Figure 1. Typical structure of reinforced metal corrugated hose [24]. **Figure 1.** Typical structure of reinforced metal corrugated hose [\[24\]](#page-12-19).

In 2008, the French company Technip developed two forms of LNG-reinforced metal corrugated hoses, namely the floating type and the suspended type corrugated hoses as shown in Figure 2a,b, respectively, according to the actual conditions of offshore operations. The main structure includes a metal lining tube, an armored layer, an insulation layer, and an outer protective layer  $[25–28]$  $[25–28]$ . The specific structure is shown in Figure [2c](#page-2-0),d, and the layers along with their specific functions are listed in Table 1 [\[29\]](#page-12-22). The cryogenic hoses designed and produced by Technip have an inner diameter of 16 inches and an outer diameter of 17 inches, their maximum working pressure is 1.8 MPa, the medium transmission design velocity is 7 m/s, and the designed service life is up to 10 years. These transmission design velocity is 7 m/s, and the designed service life is up to 10 years. These two kinds of hoses were certified by Bureau Veritas (BV) in 2010 and 2015, respectively [\[30\]](#page-12-23). kinds of hoses were certified by Bureau Veritas (BV) in 2010 and 2015, respectively [30]. The overall flexibility of Technip's LNG hoses is slightly lower, and the minimum achievable bending radius is relatively large. However, the use of corrugated inner tubes ensures good sealing and high strength. In addition, the insulation layer provides effective thermal insulation and prevents icing on the outer wall of the hose.

<span id="page-2-0"></span>

Figure 2. Two types of reinforced metal corrugated hoses by Technip [\[25\]](#page-12-20): (a) Floating type and (c) its structure; (b) Suspended type and (d) its structure (The performance of layers is listed in Tab[le](#page-2-1) 1). structure; (**b**) Suspended type and (**d**) its structure (The performance of layers is listed in Table 1).

<span id="page-2-1"></span>Table 1. Structure and Performance of reinforced metal corrugated hoses by Technip [25,29]. **Table 1.** Structure and Performance of reinforced metal corrugated hoses by Technip [\[25,](#page-12-20)[29\]](#page-12-22).



# 2.2. The High Vacuum Metal Corrugated Hoses and "pipe in pipe i  $T_{t}$  is the high vacuum type in pipe in pip

2.2. The High Vacuum Metal Corrugated Hoses

The high vacuum type metal corrugated hoses adopt a "pipe in pipe" structural form, mainly consisting of inner and outer metal thin-walled corrugated tube, anti-tensile form, manny consisting of finite and odter metal and wance corrugated the cyand tensite<br>and anti-wear protection layer, high vacuum insulation layer, vacuum port, and leak did and wear protection layer, high vacuum institution layer, vacuum port, and reak<br>detection port [\[31](#page-13-0)[,32\]](#page-13-1). The typical structure of a high vacuum-type metal corrugated hose is shown in Figure [3.](#page-3-0) The basic principle involves supporting the inner and outer metal thin-walled corrugated tubes with spacers, creating a certain annular gap. This annular gap is then evacuated to form a super-insulated vacuum layer, ensuring the hose's insulation performance. Additionally, corresponding sensors are installed in the annular gap to determine whether there is leakage by monitoring pressure or temperature changes within the gap.  $m$  in the inner and outer  $m$  of  $m$  in  $m$  is the state of  $m$  in  $m$  is the state  $n$ anti-wear protection of the metal corrugated hoses adopt a spipe in pipe structural

<span id="page-3-0"></span>

3. Outer metal thin-walled corrugated tube, 4. Inner metal thin-walled corrugated tube, 5. High vacuum insulation layer, 6. Leak detection port.

Figure 3. Typical structure of high vacuum type metal corrugated hoses [24,32]. **Figure 3.** Typical structure of high vacuum type metal corrugated hoses [\[24](#page-12-19)[,32\]](#page-13-1).

hoses in 2000, and the final product is suitable for use in relatively good sea conditions [\[33\]](#page-13-2). Its structure is shown [in](#page-3-1) Figure 4, mainly consisting of internal and external metal thinwalled corrugated tubes, annular spacers between metal corrugated tubes, an insulation layer, an armored layer, and an outer protective layer. The structure and corresponding performance of each layer are listed in Table 2. Nexans company in France started to develop LNG high vacuum metal corrugated Nexans company in France started to develop LNG high vacuum metal corrugated

<span id="page-3-1"></span>

Figure 4. The structure  $\frac{2}{3}$ . Figure 4. The structure of Nexans high vacuum metal corrugated hose [32] (The performance of **Figure 4.** The structure of Nexans high vacuum metal corrugated hose [\[32\]](#page-13-1) (The performance of layers is listed in Table 2). layers is listed in Table [2\)](#page-4-0).

This high vacuum metal corrugated hose utilizes a spiral metal corrugated tube, which During normal operation, it provides effective insulation, preventing the occurrence of ice on the outer wall of the hose. However, it lacks overall flexibility, and the achievable minimum bending radius is limited. Therefore, it is suitable for use in relatively good sea is simple to manufacture, offers excellent sealing performance, and has high strength. conditions. However, the using of high vacuum insulation comes with higher costs, and in the event of a leak, the insulation effect can be instantly compromised.

<span id="page-4-0"></span>**Table 2.** The structure and performance of Nexans high vacuum metal corrugated hose [\[32](#page-13-1)[,34\]](#page-13-3).



### *2.3. The Cryogenic Composite Hoses*

### 2.3.1. The Cryogenic Composite Hoses for Liquefied Natural Gas (LNG)

Cryogenic composite hoses are wound by multiple layers of polymer films and polymer fiber braids tightened by inner and outer helical metal wires to create a sealed tubular structure [\[12,](#page-12-8)[23\]](#page-12-18). The polymer film layers prevent leakage during medium transport, the polymer braiding layers enhance the axial and radial strength, and the inner and outer helical metal wires can provide skeletal support while enhancing the strength of the cryogenic composite hoses [\[12](#page-12-8)[,24\]](#page-12-19). The inner diameter, screw pitch, film type and thickness, number of winding layers, and the specification of inner and outer reinforcing wires of the cryogenic composite hoses should be designed according to the requirements of the actual working conditions. Depending on the liquid medium being transported, the choice of polymer films varies. The cryogenic mechanical properties, the compatibility of these films with the medium, and the barrier properties against liquid media need to be considered. At present, cryogenic composite hoses are mostly used for the transmission of LNG at sea.

The 0933 series cryogenic composite hoses manufactured by Japan Meiji Hose company (MEIJIFLEX Hose) [\[35\]](#page-13-4) located in Osaka, Japan, with a working temperature range of −200 ◦C to +80 ◦C, are designed for the transport of liquid nitrogen (−196 ◦C) and LNG ( $-162$   $\degree$ C), as shown in Figure [5.](#page-5-0) Its internal structure consists of multiple cryogenicresistant polymer films and fiber fabrics, layered and wound to meet the cryogenic mechanical performance requirements of the operating environment. The film layers primarily serve the purpose of sealing and preventing leakage, while the fiber fabrics are employed to enhance the structural strength of the cryogenic composite hoses. The manufacturing process of this kind of hose is simple and automated, leading to a low cost. Meanwhile, a heat-reflective layer is coated on the surface of film layers to enhance the thermal insulation to a certain extent. However, the thermal insulation performance with this method is limiting and needs to be further improved. The cryogenic composite hoses made by Japan Meiji are mainly used for the transportation of marine LNG, exhibiting strong adaptability to various harsh marine environments, which can significantly improve transporting efficiency.

<span id="page-5-0"></span>

1. Inner and outer metal wires, 2. Cryogenic resistant

fiber fabrics layers, 3. Cryogenic resistant polymer film

layers, 4. Impermeable film layers

Figure 5. Schematic of the structure of cryogenic composite hoses by Japan Meiji company. **Figure 5.** Schematic of the structure of cryogenic composite hoses by Japan Meiji company. Figure 5. Schematic of the structure of cryogenic composite hoses by Japan Meiji company.

cryogenic composite hoses used for LNG since 2011, which are lightweight, high-strength, and flexible [\[36\]](#page-13-5). They introduced a new cryogenic composite hose used for LNG as shown in Figure [6,](#page-5-1) which underwent various performance tests at normal and cryogenic temperatures, ultimately receiving DNV certification in 2016 [\[9\]](#page-12-5). The design form of this cryogenic composite hose offers excellent flexibility, a smaller bending radius, and can adapt to relatively harsh sea conditions. By adding the thermal insulation layers, it effectively prevents the outer surface of the hose from icing in a short period. However, the insulation layers are located inside of the pipe wall, and it poses manufacturing challenges, increasing the difficulty of processing and requiring strict control over the pre-compression force between the winding layers. The Dunlop company in the UK has been dedicated to the research and development of

<span id="page-5-1"></span>

Figure 6. The structure of composite hoses by Dunlop. **Figure 6.** The structure of composite hoses by Dunlop.

During the transportation of cryogenic fluids, there is a high demand for the thermal during the transportation of cryogenic composite needs to prevent the statuent metals need additional insulation layers to prevent frosting outside of the hose and meet the insulation requirement. Sweden's Trelleborg and France's Total developed a cryogenic composite hose named Cryo-line in 2016, based on the "pipe in pipe" concept as shown in Figure [7.](#page-6-0) After static and dynamic pressure testing at normal and low temperatures, the cryogenic composite hoses successfully obtained BV certification [\[37](#page-13-6)[–39\]](#page-13-7). The composition and performance characteristics of each layer of this hose are listed in Table [3.](#page-6-1) The cryogenic composite hoses have improved insulation performance, effectively preventing the outer surface of the hose from icing. Additionally, a leak detection system, a monitoring method based on fiber optic detection technology, is embedded in the insulation layers to improve the safety of the cryogenic hoses during work. However, the presence of the insulation layers and monitoring system makes the manufacturing process complex and increases  $\sum_{i=1}^{\infty}$ During the transportation of cryogenic fluids, there is a high demand for the thermal insulation performance of cryogenic composite hoses to prevent the sudden increase of in-insulation performance of cryogenic composite hoses to prevent the sudden increase  $\frac{1}{2}$  system makes the matrix  $\frac{1}{2}$  and increases the cost. of inner pressure due to liquid vaporization. In conclusion, cryogenic composite hoses the cost.

<span id="page-6-0"></span>

Figure 7. Structure of cryo-line composite hose [38,39] (The performance of layers is listed in Ta[bl](#page-6-1)e **Figure 7.** Structure of cryo-line composite hose [\[38](#page-13-8)[,39\]](#page-13-7) (The performance of layers is listed in Table 3). 3).



<span id="page-6-1"></span>Table 3. Structure and performance features of cryo-line composite hose [38,40]. **Table 3.** Structure and performance features of cryo-line composite hose [\[38,](#page-13-8)[40\]](#page-13-9).

# 2.3.2. The Cryogenic Composite Hoses for Liquid Oxygen

Compared to the cryogenic composite hoses used for LNG, those used for liquid oxygen transportation face a more severe and extreme working environment, posing greater crucial challenges must be addressed and overcome. Firstly, the temperature of liquid oxygen (−183 °C) is lower, leading to more severe low-temperature embrittlement of polymer materials and heightened safety concerns [42]. Secondly, Due to the strong oxidizing property of liquid oxygen (LOX), most polymers possessing excellent cryogenic mechanical properties are LOX incompatible [43,44]. And, if these incompatible polymers are u[sed](#page-13-12) as the inner layer material of the hose, it probably leads to significant safety accidents such as combustion and even explosion under certain external energy stimulation [\[44](#page-13-13)[–46\]](#page-13-14).  $\,$ Therefore, the issue of material compatibility with liquid oxygen is a crucial problem that needs to be solved urgently. And, if the solved used in the solved polymers are used in the use of the use of  $\mu$ challenges in design and manufacturing [\[41\]](#page-13-10). For the safe use of liquid oxygen hoses, two

> It is found that most metals (except titanium alloys) exhibit good compatibility with liquid oxygen, including stainless steel, aluminum and its alloys, copper and its alloys, and nickel and its alloys [\[47\]](#page-13-15). Therefore, vacuum metal corrugated hoses are widely used for liquid oxygen transportation currently. However, few polymers are compatible with liquid oxygen. At present, among thermoplastic polymer materials, only some types of fluoropolymers are LOX compatible [\[48\]](#page-13-16). Research shows that some fluoropolymers, such as polytetrafluoroethylene (PTFE), polychlorotrifluoroethylene (PCTFE), and ethylene tetrafluoroethylene copolymer (ETFE), are commonly used as sealing materials for liquid oxygen pipe fittings [\[49](#page-13-17)[–52\]](#page-13-18), which indicated that these fluoropolymers are compatible with LOX. In this section, we investigated the mechanical properties of several fluoroplastic films available on the market, including perfluoroalkoxy polymers (PFA), PTFE, PCTFE, PCTFE, and ETFE. And conducted liquid oxygen impact sensitivity tests on these four fluoroplastic<br>and ETFE. And conducted liquid oxygen impact sensitivity tests on these four fluoroplastic films according to the method specified in the ASTM D2512-95 standard [\[53\]](#page-13-19). The results  $\frac{1}{2}$ show that they are all compatible with liquid oxygen. At the same time, we also tested their  $\frac{1}{2}$ mechanical properties at room temperature and liquid nitrogen temperature (−196 °C) (fol-<br>https://www.ptfe.gov.principal.org/2005/Fa1), PTFE, and liquid nitrogen temperature (−196 °C) (fol-lowing the standard ISO-527-3) [\[54\]](#page-13-20), and the tensile stress–strain curves of these four plastic

<span id="page-7-0"></span>films are shown in Figure [8.](#page-7-0) It can be seen that although the tensile strength of plastic films innis are shown in Figure 6. It can be seen that annough the tensile strength of plastic initis<br>increases at low temperatures, the elongation at break decreases exponentially, ultimately resulting in a sharp decrease in fracture strain energy, indicating that the material becomes resulting in a sharp decrease in fracture strain energy, indicating that the material becomes less ductile and more brittle at ultra-low temperatures, compared to room temperature. strength of plastic films increases at low temperatures, the elongation at break decreases

of these four plastic films are shown in Figure 8. It can be seen that although the tensile  $\mathcal{L}$ 



Figure 8. Tensile stress–strain curves of PCTFE, PFA, ETFE, and FEP plastic films under (a) room **Figure 8.** Tensile stress–strain curves of PCTFE, PFA, ETFE, and FEP plastic films under (**a**) room temperature and (b) liquid nitrogen temperature (−196 ℃). temperature and (**b**) liquid nitrogen temperature (−196 ◦C).

The values of tensile strength, elongation at break, and elastic modulus for the four The values of tensile strength, elongation at break, and elastic modulus for the four fluoropolymer films at room temperature and liquid nitrogen temperature (−196 °C) were fluoropolymer films at room temperature and liquid nitrogen temperature (−196 ◦C) were listed in Table 4. At the temperature of liquid nitrogen (−196℃), the tensile strength of listed in Table [4.](#page-7-1) At the temperature of liquid nitrogen (−196 ◦C), the tensile strength of at room temperature, respectively, and the elastic modulus is approximately 4.2, 2.9, 4.4, and 5.7 times higher, indicating a significant increase in material strength and stiffness at the cryogenic environment. Meanwhile, the elongation at break of the four types of films at −196 °C shows a reduction of orders of magnitude compared to that at room temperature. Therefore, although these four types of fluoropolymer films are liquid oxygen compatible and exhibit a certain level of strength at ultra-low temperatures, it is challenging for them to meet the pressure-resistant requirement in hoses for liquid oxygen transport. In order to the pressure of the safety and fictionity of fiquit oxygen hoses, these fidelioply filed limits fieed<br>to be combined with other low-temperature-resistant polymeric films such as polyimide, to be combined with other town temperature resistant polymeric initis such as polymeric,<br>ultra-high molecular weight polyethylene, or polyester.  $\sigma$  need to be combined with other low-temperature-resistant polymeric  $\sigma$ PCTFE, ETFE, FEP, and PFA films is approximately 7.8, 4, 6.2, and 4.8 times higher than that enhance the safety and flexibility of liquid oxygen hoses, these fluoropolymer films need

Material	Performance	Tensile Strength/MPa		<b>Elongation at Break/%</b>		Elastic Modulus/GPa	
		$20^{\circ}$ C	$-196 °C$	20 °C	$-196$ °C	$20^{\circ}$ C	$-196$ °C
	<b>PCTFE</b>	$16.32 \pm 1.02$	$127.78 \pm 8.91$	$193.53 + 9.01$	$4.01 \pm 0.66$	$1.35 \pm 0.10$	$5.65 \pm 0.16$
	<b>ETFE</b>	$25.04 \pm 1.61$	$100.16 + 5.03$	$386.71 + 7.93$	$4.31 + 0.26$	$1.69 + 0.08$	$4.85 \pm 0.21$
	FEP	$11.52 + 1.22$	$71.08 + 4.87$	$379.04 + 8.83$	$6.37 \pm 0.19$	$0.59 + 0.05$	$2.98 \pm 0.20$
	PFA	$16.85 \pm 1.33$	$80.79 \pm 8.43$	$478.89 \pm 7.68$	$6.32 \pm 0.29$	$0.58 \pm 0.04$	$3.28 \pm 0.27$

<span id="page-7-1"></span>Table 4. The mechanical performance of four fluoropolymer at ambient and cryogenic temperatures.

# 2.3.3. The Manufacturing Process of Cryogenic Composite Hose

The properties of the medium conveyed by the cryogenic composite hoses determine be processed and manufactured according to the designed structural form and structural<br>be processed and manufactured according to the designed structural form and structural is completed on a rotating mechanical shaft, as shown in Figure 9. The diameter of the mechanical shaft determines the inner diameter of the cryogenic composite hoses. The specific manufacturing process is summarized as follows: the use of materials. After the material is determined, the cryogenic composite hoses can parameters. The entire manufacturing process of the wall of cryogenic composite hose

understand.

<span id="page-8-0"></span>

Figure 9. The schematic diagram of the manufacturing process. **Figure 9.** The schematic diagram of the manufacturing process.

size of the cryogenic composite hoses. Then, each film, fabric, and other thermal insulation material is wrapped around the wire according to the designed angle in the lay-up sequence. Finally, all layers are laid, the outer wire is wrapped around the outside at the same pitch, and half a screw pitch apart from the inner wire to form a self-locking structure. After the completion of the body of the cryogenic composite hose is removed from the rotary shaft, intercepting the valid section and installing the connectors. The above is the simplified manufacturing process of cryogenic composite hose, only for the reader to understand. First, the inner wire is wound onto the mechanical shaft according to the screw pitch

# fluid medium exhibits strong oxidizing or corrosive properties, the material selection of **3. The Key Technical Challenges of Cryogenic Composite Hoses**<br>2. The Key Technical Challenges of Cryogenic Composite Hoses

# 3.1. The Material Selection for Cryogenic Composite Hoses

The selection of the material for cryogenic hoses is one of the crucial factors determining hose safety, fatigue resistance, and lifespan. For metal corrugated hoses, 316 L stainless steel exhibits good low-temperature toughness and corrosion resistance [\[31,](#page-13-0)[55\]](#page-13-21), it is suitable as the material used in metal corrugated hoses for the transportation of most low-temperature media. As for cryogenic composite hoses, when the low-temperature fluid medium exhibits strong oxidizing or corrosive properties, the material selection of the conveying hose is critical. Especially in the selection of the inner layer material in direct contact with the medium, the material must not only consider the mechanical properties (strength, flexibility, mechanical fatigue performance, etc.) [\[44](#page-13-13)[,56](#page-13-22)[,57\]](#page-13-23) but also consider the barrier, oxidation resistance, and corrosion resistance under the corresponding medium.

Due to the small molecular weight of some media (such as liquid hydrogen), for a period of time, it will permeate out of the container wall, making the hydrogen content of the air increase, which is prone to accidents [\[58](#page-13-24)[–60\]](#page-14-0). Therefore, it is necessary to perform a penetration test on the materials used for this medium. In addition, there are some media with strong oxidation and corrosion (such as liquid oxygen), and some polymer materials will oxidize in liquid oxygen for a long time, thereby reducing their own mechanical properties. Therefore, the corresponding material needs to be soaked in liquid oxygen test, and then the mechanical properties of the soaked material are tested. Therefore, there are two methods for material selection: First, material performance tests need to be completed according to the actual situation based on the existing materials, and then applied to the cryogenic composite hoses after meeting the requirements. Second, combined with the performance characteristics of existing materials, the synthesis of high-performance new materials that meet the requirements, and then through various performance tests to ensure that they can meet the requirements of cryogenic composite hoses.

### *3.2. The Structure Design and Numerical Simulation of Cryogenic Composite Hose*

Due to the harsh operating conditions of cryogenic hoses, the structural design must consider the impact of temperature, internal pressure, bending, and torsion on its mechanical properties [\[1,](#page-11-0)[13](#page-12-15)[,55\]](#page-13-21). Additionally, factors such as thermal insulation performance, sealing performance, flexibility, strength, and weight must be taken into account [\[14\]](#page-12-9). The design of the hose aims to ensure safety and reliability while obtaining reasonable structural forms, interlayer thicknesses, and stacking methods for each layer. Furthermore, the structural analysis of cryogenic composite hoses involves winding structure analysis, modeling analysis of multilayer non-bonded composite structures, and modeling analysis of braided structures [\[61\]](#page-14-1). These include numerical simulations of structural and thermal-solid coupling, addressing challenges in unit analysis, interlayer contact analysis, nonlinear problem analysis, and constraints on boundary conditions [\[31,](#page-13-0)[62\]](#page-14-2). In summary, the structural design and modeling analysis of cryogenic hoses need to consider the mechanical response characteristics under different conditions and balance various performance parameters for optimal structural design. The validation process involves structural numerical simulations, nonlinear analysis of interlayer structures, fluid–solid coupling calculations, and heat transfer calculations to obtain a low-temperature hose structure suitable for specific operating conditions [\[7\]](#page-12-3). The future research aim is to overcome the above problems to obtain lightweight, high-strength, high-toughness, and large-size cryogenic composite hoses that meet various working conditions.

#### *3.3. The Insulation Measures of Cryogenic Composite Hoses*

There are three heat transfer styles, conduction, convection, and radiation. It is a challenge to achieve absolute insulation within limited thickness within the millimeter or centimeter scale range [\[63](#page-14-3)[,64\]](#page-14-4). For cryogenic hoses, two methods are usually used to achieve thermal insulation, by vacuum interlayer between inner and outer walls or by insulation materials. The former provides excellent insulation performance but is associated with poor flexibility and higher overall costs. Additionally, Once the vacuum layer is damaged, the insulation performance will be immediately lost resulting in the failure of the entire hose structure. The insulation layers of composite hoses need to meet high requirements, such as lightweight, excellent flexibility, and longer service life. There are many kinds of traditional insulation materials, including glass wool, foam asbestos, aluminum silicate fiber felt, and polyurethane. They are usually used in the form of pads or plates for insulation protection outside vessels or buildings [\[65–](#page-14-5)[67\]](#page-14-6). Flexible aerogel is a new type of insulation material, the biggest advantage is that it has flexibility, and can be used for insulation measures of different curvature surfaces [\[68](#page-14-7)[,69\]](#page-14-8).

The insulation performance of common insulation materials is listed in Table [5.](#page-10-0) At present, aerogel possesses a promising prospect in cryogenic composite hoses, due to its lightweight, excellent, and stable insulation performance, low-temperature resistance, and long insulation life [\[70\]](#page-14-9). As early as the late 1980s, researchers in the Lawrence Livermore National Laboratory (LLNL) prepared the lightest silica aerogel with a density of 0.003  $g/cm<sup>3</sup>$  and only three times than air. At room temperature and pressure, its thermal conductivity ranges between 0.011  $W/(m \cdot K)$  and 0.016  $W/(m \cdot K)$  [\[71\]](#page-14-10). If aerogel is used as insulation material for cryogenic composite hoses, it can effectively reduce the wall thickness and overall weight. The reinforced metal corrugated hose developed by Technip in France uses aerogel as the insulation material, achieving excellent insulation performance

and effectively preventing the outer wall from icing during the working process [\[16\]](#page-12-24). Thermal insulation performance is one of the important indexes of cryogenic composite hoses. Previous studies have shown that aerogel is an excellent insulation material, However, further research is needed to realize its application in cryogenic composite hoses, especially how to reasonably apply it to the structure of cryogenic composite hose and ensure its fault tolerance.



<span id="page-10-0"></span>**Table 5.** Performance comparison of common insulation materials [\[65](#page-14-5)[,72](#page-14-11)[–76\]](#page-14-12).

#### *3.4. The Leak Monitoring System of Cryogenic Composite Hoses*

In the working process, the real-time monitoring of the positions prone to leakage and fatigue in cryogenic hoses can provide more effective safety assurance throughout the entire operation. Fiber optic sensing systems offer advantages such as resistance to electromagnetic interference, high insulation, and reliable sensitivity, they can provide real-time monitoring during the working of cryogenic hoses so that leaks can be detected timely to prevent accidents [\[25,](#page-12-20)[77](#page-14-13)[,78\]](#page-14-14). The leak detection system for cryogenic hoses based on fiber optics is illustrated in Figure [10.](#page-10-1) The challenges of the application of fiber optic monitoring systems in cryogenic hoses are mainly the distribution of fiber optic systems, service life, and bending flexibility with the complex working conditions of cryogenic hoses. Reasonable optical fiber arrangement can realize all-round monitoring, improve the fault tolerance rate of optical fiber monitoring systems can greatly improve the service life of cryogenic composite hoses, and indirectly reduce the production cost.

<span id="page-10-1"></span>

1. Protective layer, 2. Insulation layer, 3. Insulation layer, 4. Armor layer 5. Sealing layer, 6. Inner corrugated tube, 7. Fiber optic for leakage monitoring

Figure 10. The cryogenic composite hoses with an optical fiber monitoring system [25]. Fi**gure 10.** The cryogenic composite hoses with an optical fiber monitoring system [\[25\]](#page-12-20).<br>
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#### **4. Summary and Perspectives**

Compared to metal corrugated hoses, flexible composite hoses based on thermoplastic polymers have the advantages of being lightweight, good flexibility, simple operation, and easy connection. With the continuous development of the offshore LNG bunkering market, the superiority of flexible composite hose bunkering methods has become increasingly prominent. These hoses can be operated in bad and extreme sea conditions, breaking the limitation of traditional ones which can only be used in good sea conditions, significantly reducing the operational risk and improving working efficiency. Additionally, with the continuous development in various industries, there is a substantial potential demand for the transport and bunkering systems of low-temperature media such as liquid oxygen, liquid hydrogen, and LNG. Therefore, there is a wide prospect for cryogenic composite hoses applied in LNG transport and ship bunkering systems, liquid oxygen or liquid hydrogen bunkering systems for rockets, as well as commercial cryogenic media transfer and bunkering systems.

Due to the extreme working conditions, such as ultra-low temperature and high pressure, there are high requirements for the weight, cryogenic mechanical properties, chemical stability, leak resistance, thermal fatigue resistance, and thermal insulation performance of cryogenic composite hoses. It makes material selection, structural design, manufacture, safety monitoring, and testing of cryogenic composite hoses face many challenges. First of all, materials are fundamental to the manufacture of cryogenic composite hoses. cryogenic and corrosion-resistant polymer materials are the key to limiting the further development of cryogenic composite hoses. In addition, the reasonable structural design can improve the service life and working strength of the low-temperature composite hose, it also reduces the weight and improves the toughness as much as possible under the premise of ensuring sufficient strength. Finally, reliable monitoring technology can avoid risks in advance to ensure the safe operation of the cryogenic composite hose. The further development of cryogenic composite hoses first requires efforts in the research and development of high-performance materials. Then, combined with accurate numerical simulation, the interface mechanism between different layers should be considered comprehensively, and reasonable winding Angle, layering sequence, pitch, wave height, and wave width need to be optimized, and finally the structure form with excellent performance is obtained. Finally, in order to ensure the safety and reliability of cryogenic composite hoses, the application of detection technology also needs further research. Overcoming the above challenges will break the shackles of cryogenic composite hoses and further improve the efficiency of offshore natural gas development and aerospace cryogenic propellant filling.

In the future, the technical developments in structure/function integrated materials, optimization methods and software for hose structures, intelligent manufacturing technology, novel sealing connection structures, and health monitoring technology will lead the continuous development of cryogenic composite hoses towards directions of lightweight, high flexibility and safety, long life, large size, and self-monitor.

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### **References**

- <span id="page-11-0"></span>1. Mallon, N.; van der Weijde, G. Influence of Hysteresis on the Dynamics of Cryogenic LNG Composite Hoses. In Proceedings of the ASME 2011 30th International Conference on Ocean, Offshore and Arctic Engineering, Rotterdam, The Netherlands, 19–24 June 2011; pp. 199–208.
- <span id="page-11-1"></span>2. Queau, J.P.; Torre, G.E. COOL™ Hose Qualification Process of the First EN1474−2 Lng Floating Hose. In Proceedings of the ASME 2011 30th International Conference on Ocean, Offshore and Arctic Engineering, Rotterdam, The Netherlands, 19–24 June 2011.
- <span id="page-11-2"></span>3. Hao, Z.; Luo, J.; Jin, Y.; Wei, W.; Liu, L. Failure analysis of corrugated metal hose under ultimate repeated bending process. *Eng. Fail. Anal.* **2020**, *109*, 104295. [\[CrossRef\]](https://doi.org/10.1016/j.engfailanal.2019.104295)
- <span id="page-12-0"></span>4. Huang, D.; Zhang, J. Research on the Tensile Mechanical Properties of a Braided Corrugated Hose and Its Axial Stiffness Model. *J. Mar. Sci. Eng.* **2021**, *9*, 1029. [\[CrossRef\]](https://doi.org/10.3390/jmse9091029)
- <span id="page-12-1"></span>5. Huang, D.; Zhang, J. Numerical Simulation and Experimental Study on Axial Stiffness and Stress Deformation of the Braided Corrugated Hose. *Appl. Sci.* **2021**, *11*, 4709. [\[CrossRef\]](https://doi.org/10.3390/app11104709)
- <span id="page-12-2"></span>6. Yuan, B.; Mao, L.; Dong, R.; Zhang, T.; Zhang, R.; Liu, G.; Wei, W. Failure analysis of metal corrugated hose in space station. In Proceedings of the International Conference on Intelligent and Human-Computer Interaction Technology (IHCIT 2022), Zhuhai, China, 22–24 July 2022.
- <span id="page-12-3"></span>7. Hu, H.; Yang, Z.; Yan, J.; Yang, L.; Zhou, B.; Fan, J. Thermal and mechanical coupled analysis of marine composite cryogenic pipeline. In Proceedings of the ASME 2019 38th International Conference on Ocean, Offshore and Arctic Engineering, Glasgow, UK, 9–14 June 2019.
- <span id="page-12-4"></span>8. Twerda, D.A.; Netherlands, D.T. Integrity and Efficiency in LNG Transfer Operations with Flexibles. In Proceedings of the International Petroleum Technology Conference, Doha, Qatar, 20–22 January 2014.
- <span id="page-12-5"></span>9. Witz, J.A.; Ridolfi, M.V.; Hall, G.A. Offshore LNG transfer—A new flexible cryogenic hose for dynamic service. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 3–6 May 2004.
- <span id="page-12-6"></span>10. Wu, C.; Liu, J.; Zhang, J. Transient thermal analysis on pre-cooling process of LNG cryogenic corrugated hose. *Geoenergy Sci. Eng.* **2024**, *232*, 212434. [\[CrossRef\]](https://doi.org/10.1016/j.geoen.2023.212434)
- <span id="page-12-7"></span>11. Liu, M.E.; Yang, L.; Li, F.; Lu, Z.; Yan, J. Thermophysical properties of the corrugated cryogenic hose precooling process. *J. Pipeline Sci. Eng.* **2023**, *3*, 100110. [\[CrossRef\]](https://doi.org/10.1016/j.jpse.2023.100110)
- <span id="page-12-8"></span>12. Ston, J.B.; Ehrhardt, M.E.; Johnston, A.B.; Rischmüller, P.; Nusser, S. Offshore LNG Loading Problem Solved. Gastech 2000. Available online: [https://www.impac.de/fileadmin/content/Downloads/15\\_Offshore\\_LNG\\_gastech\\_2003.pdf](https://www.impac.de/fileadmin/content/Downloads/15_Offshore_LNG_gastech_2003.pdf) (accessed on 17 March 2024).
- <span id="page-12-15"></span>13. Francois, C.B.; Huang, T.; Mohan, K. Structural analysis of cryogenic flexible hose. In Proceedings of the ASME 2011 30th International Conference on Ocean, Offshore and Arctic Engineering, Rotterdam, The Netherlands, 19–24 June 2011; pp. 593–606.
- <span id="page-12-9"></span>14. Weijde, G.V.D.; Putten, S.V.D. Assessing Integrity and Reliability of Multicomposite LNG Transfer Hoses. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 30 April–3 May 2012.
- <span id="page-12-10"></span>15. Cox, P.J.C.; Gerez, J.M.; Biaggi, J.P. Cryogenic Flexible for Offshore LNG Transfer. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2003.
- <span id="page-12-24"></span>16. Tan, D.; Case, M.; Sheldrake, T. Higher order effects on bending of helical armor wire inside an unbounded flexible pipe. In Proceedings of the 24th International Conference on Offshore Mechanics and Arctic Engineering, Halkidiki, Greece, 12–17 June 2005.
- <span id="page-12-11"></span>17. Buitrago, J.; Slocum, S.T. Cryogenic Structural Performance of Corrugated Pipe. In Proceedings of the ASME 2010 29th International Conference on Ocean, Offshore and Arctic Engineering, Shanghai, China, 6–11 June 2010.
- <span id="page-12-12"></span>18. *ISO/20257-1*; Installation and Equipment for Liquefied Natural Gas—Design of Floating LNG Installations—Part 1: General Requirements. ISO: Geneva, Switzerland, 2020.
- <span id="page-12-13"></span>19. *ISO/20257-2*; Installation and Equipment for Liquefied Natural Gas—Design and Testing of Marine Transfer Systems—Part 2 Design of Floating LNG Installations—Part 2: Specific FSRU issues. ISO: Geneva, Switzerland, 2021.
- <span id="page-12-14"></span>20. Yang, Z.; Yan, J.; Chen, J.; Lu, Q.; Yue, Q. Multi-Objective Shape Optimization Design for Liquefied Natural Gas Cryogenic Helical Corrugated Steel Pipe. *J. Offshore Mech. Arct. Eng.* **2017**, *139*, 051703. [\[CrossRef\]](https://doi.org/10.1115/1.4036372)
- <span id="page-12-16"></span>21. Huang, G.; Wu, W. Armored steel wire stress monitoring strategy of a flexible hose in LNG tandem offloading operation. *Ocean Eng.* **2023**, *281*, 114775. [\[CrossRef\]](https://doi.org/10.1016/j.oceaneng.2023.114775)
- <span id="page-12-17"></span>22. Wang, H.; Yang, Z.; Yan, J.; Wang, G.; Shi, D.; Zhou, B.; Li, Y. Prediction Method and Validation Study of Tensile Performance of Reinforced Armor Layer in Marine Flexible Pipe/Cables. *J. Mar. Sci. Eng.* **2022**, *10*, 642. [\[CrossRef\]](https://doi.org/10.3390/jmse10050642)
- <span id="page-12-18"></span>23. Frohne, D.C.; Harten, F.; Schippl, K.; Steen, K.E.; Haakonsen, R. Innovative Pipe System for Offshore LNG Transfer. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2008.
- <span id="page-12-19"></span>24. *ISO 16904-2*; Installation and Equipment for Liquefied Natural Gas—Design and Testing of Marine Transfer Systems—Part 2: Design and Testing of Transfer Hoses. ISO: Geneva, Switzerland, 2024.
- <span id="page-12-20"></span>25. Abbasi, T.; Hults, J.E.; Mesnage, O.; Subsea, F.; Genesis, V.S.; Gerez, J.; Hardiman, R.; Vlekken, J.; Roosbroeck, J. LNG flexible integrated with fiber optic distributed leak system enhancing safety, integrity monitoring and life assessments. In Proceedings of the Offshore Technology Conference, Kuala Lumpur, Malaysia, 22–25 March 2016.
- 26. Ferreira, A.L.F.; Morooka, C.K. Evaluation of response of a floating cryogenic hose in offloading operation between FLNG unit and carrier in tandem. In Proceedings of the ASME 2015 34th International Conference on Ocean, Offshore and Arctic Engineering, St. John's, NL, Canada, 31 May–5 June 2015.
- 27. Cox, P.; Blair, C.; Adkins, D. Integration of Insulated Rigid and Flexible Cryogenic Pipes in Marine LNG Transfer. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 1–4 May 2006.
- <span id="page-12-21"></span>28. Eurodim, B.D.; Technip-Coflexip, P.C.; Claude Garrigues, J. Key Cryogenic Components for Dynamic Marine LNG Transfer at Sea- Development and tests completed. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2003.
- <span id="page-12-22"></span>29. Cox, P.; O'Sullivan, J.; Lehning, V. Results of New LNG Transfer Technology Developments and What Possibilities They Foretell. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 30 April–3 May 2007.
- <span id="page-12-23"></span>30. Rombaut, G.; Peigne, A.; Loisel, P.; Cloirec, A.; Machouat, F.; Maocec, D. LNG Trials of a New 16" Flexible Hose Based LNG Transfer System In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2008.
- <span id="page-13-0"></span>31. Yang, Z.; Yan, J.; Chen, J.; Wang, C.; Lu, Q.; Wu, S.; Yue, Q. Multi-objective shape optimization design for lng cryogenic. In Proceedings of the ASME 2016 35th International Conference on Ocean, Offshore and Arctic Engineering, Busan, Republic of Korea, 19–24 June 2016.
- <span id="page-13-1"></span>32. OneSubsea, J.E.; Haakonsen, R.; Aker Pusnes, T.V.O.; Nexans, C.F. offshore tandem loading of LNG-from idea to system approval. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2014.
- <span id="page-13-2"></span>33. Hoog, S.; Koch, H.; Huhn, R.; Frohne, C.; Homann, J.; Clauss, G.; Sprenger, F.; Testa, D. LNG transfer in harsh environmentsintroduction of a new concept. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 4–7 May 2009.
- <span id="page-13-3"></span>34. Eide, J.; Bernson, M.; Haakonsen, R.; Frohne, C. Challenges and solutions in the development of a flexible cryogenic pipe for offshore LNG transfer. In Proceedings of the Offshore Technology Conference, Rio de Janeiro, Brazil, 4–6 October 2011.
- <span id="page-13-4"></span>35. Corporation, M. Flexible Composite Hose Group. Available online: <http://www.meiji-rubber.co.jp/product/fh/index.html> (accessed on 18 March 2024).
- <span id="page-13-5"></span>36. Humphreys, V.; Jones, N. Offshore LNG transfer, a practical system based on proven oil transfer principles. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 3–6 May 2004.
- <span id="page-13-6"></span>37. Giacosa, A.; Mauries, B.; Lagarrigue, V. joining forces to unlock LNG tandem offloading using 20" LNG floating hose—An example of industrial collaboratin. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 2–5 May 2016.
- <span id="page-13-8"></span>38. Lagarrigue, V.; Hermary, J. Trelleborg. Re-shaaping LNG transfer. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 30 April–3 May 2018.
- <span id="page-13-7"></span>39. Lagarrigue, V.; Trelleborg, J.H.; Saipem, B.M. Qualification of A Cryogenic Floating Flexible Hose Enabling Safe And Reliable Offshore LNG Transfer For Tandem FLNG Offloading Systems. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2014.
- <span id="page-13-9"></span>40. Saipem, B.M.; Saipem, F.B.; Saipem, F.L.; Trelleborg, V.L. Development of an LNG Tandem Offloading System Using Floating Cryogenic Hoses-Breaking the Boundaries of LNG Transfer in Open Seas. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 5–8 May 2014.
- <span id="page-13-10"></span>41. Wehr-Aukland, A.K.; White, J.E.; Cook, K.M. Failure Analysis of an Oxygen Transfer Hose Flash Fire. In *Flammability and Sensitivity of Materials in Oxygen-Enriched Atmospheres: 15th Volume*; ASTM International: West Conshohocken, PA, USA, 2021; pp. 207–219. [\[CrossRef\]](https://doi.org/10.1520/stp162620200014)
- <span id="page-13-11"></span>42. Chen, D.; Li, J.; Yuan, Y.; Gao, C.; Cui, Y.; Li, S.; Liu, X.; Wang, H.; Peng, C.; Wu, Z. A Review of the Polymer for Cryogenic Application: Methods, Mechanisms and Perspectives. *Polymers* **2021**, *13*, 320. [\[CrossRef\]](https://doi.org/10.3390/polym13030320)
- <span id="page-13-12"></span>43. Ren, M.; Wang, L.; Li, T.; Wei, B. Molecular investigation on the compatibility of epoxy resin with liquid oxygen. *Theor. Appl. Mech. Lett.* **2020**, *10*, 38–45. [\[CrossRef\]](https://doi.org/10.1016/j.taml.2019.06.010)
- <span id="page-13-13"></span>44. Li, S.; Li, J.; Cui, Y.; Ye, J.; Chen, D.; Yuan, Y.; Liu, X.; Liu, M.; Peng, C.; Wu, Z. Liquid oxygen compatibility of epoxy matrix and carbon fiber reinforced epoxy composite. *Composites Part A* **2022**, *154*, 106771. [\[CrossRef\]](https://doi.org/10.1016/j.compositesa.2021.106771)
- 45. Wu, Z.; Li, C.; Liu, M. Study on liquid oxygen compatibility of bromine-containing epoxy resins for the application in liquid oxygen tank. *Polym. Adv. Technol.* **2016**, *27*, 98–108. [\[CrossRef\]](https://doi.org/10.1002/pat.3604)
- <span id="page-13-14"></span>46. Wang, G.; Li, X.; Yan, R.; Xing, S. The study on compatibility of polymer matrix resins with liquid oxygen. *Mater. Sci. Eng. B* **2006**, *132*, 70–73. [\[CrossRef\]](https://doi.org/10.1016/j.mseb.2006.02.028)
- <span id="page-13-15"></span>47. Kevin Rivers, H. Cyclic Cryogenic Thermal-Mechanical Testing of an X-33-RLV Liquid Oxygen Tank Concept. In Proceedings of the NASA/TM-1999, NASA Center for AeroSpace Information, Florence, Italy, 5–10 September 1999.
- <span id="page-13-16"></span>48. DeLong, D.; Greason, J. Thermoplastic Fluoropolymer Composite Material for Lightweight, Long-life, Nonflammable Tanks and Structures. In Proceedings of the 48th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference, Honolulu, HI, USA, 23–26 April 2007.
- <span id="page-13-17"></span>49. Teng, H.X. Overview of the Development of the Fluoropolymer Industry. *Appl. Sci.* **2012**, *2*, 496–512. [\[CrossRef\]](https://doi.org/10.3390/app2020496)
- 50. Zou, J.J.; Zhang, M.C.; Huang, M.Q.; Zhao, D.; Dai, Y. Structure, Properties, and Modification of Polytrifluorochloroethylene: A Review. *Front. Mater* **2022**, *9*, 824155. [\[CrossRef\]](https://doi.org/10.3389/fmats.2022.824155)
- 51. Snyder, C.E.; Gschwender, L.J. Fluoropolymers in Fluid and Lubricant Applications. *Ind. Eng. Chem. Prod. Res. Dev* **1983**, *22*, 383–386. [\[CrossRef\]](https://doi.org/10.1021/i300011a001)
- <span id="page-13-18"></span>52. Ameduri, B. Fluoropolymers: The Right Material for the Right Applications. *Chemistry* **2018**, *24*, 18830–18841. [\[CrossRef\]](https://doi.org/10.1002/chem.201802708)
- <span id="page-13-19"></span>53. *ASTM D2512-95*; Standard Test Method for Compatibility of Materials with Liquid Oxygen (Impact Sensitivity Threshold and Pass-Fail Techniques). ASTM: West Conshohocken, PA, USA, 1995.
- <span id="page-13-20"></span>54. *ISO-527-3*; Plastics-Determination of Tensile Properties-Part 3—Test Conditions for Films and Sheets. ISO: Geneva, Switzerland, 2018.
- <span id="page-13-21"></span>55. Srivastava, V.; Buitrago, J.; Slocum, S.T. Stress analysis of a cryogenic corrugated pipe. In Proceedings of the ASME 2011 30th International Conference on Ocean, Offshore and Arctic Engineering, Rotterdam, The Netherlands, 19–24 June 2011.
- <span id="page-13-22"></span>56. Key, C.F.; Riehl, W.A. *Compatibility of Materials with Liquid Oxygen*; NASA TM X-985; NASA: Washington, DC, USA, 1964. Available online: <https://ntrs.nasa.gov/api/citations/19750065862/downloads/19750065862.pdf> (accessed on 18 March 2024).
- <span id="page-13-23"></span>57. Nakayama, Y.; Takahagi, T.; Soeda, F.; Ishitani, A. A Study of XPS 01s Spectrum of Poly(ethylene Terephthalate). *J. Polym. Sci. Part A Polym. Chem.* **1990**, *28*, 1813–1821. [\[CrossRef\]](https://doi.org/10.1002/pola.1990.080280713)
- <span id="page-13-24"></span>58. Li, X.; Huang, Q.; Liu, Y.; Zhao, B.; Li, J. Review of the Hydrogen Permeation Test of the Polymer Liner Material of Type IV On-Board Hydrogen Storage Cylinders. *Materials* **2023**, *16*, 5366. [\[CrossRef\]](https://doi.org/10.3390/ma16155366)
- 59. Qiu, Y.; Yang, H.; Tong, L.; Wang, L. Research Progress of Cryogenic Materials for Storage and Transportation of Liquid Hydrogen. *Metals* **2021**, *11*, 1101. [\[CrossRef\]](https://doi.org/10.3390/met11071101)
- <span id="page-14-0"></span>60. Aziz, M. Liquid Hydrogen: A Review on Liquefaction, Storage, Transportation, and Safety. *Energies* **2021**, *14*, 5917. [\[CrossRef\]](https://doi.org/10.3390/en14185917)
- <span id="page-14-1"></span>61. Yang, L.; Liu, M.; Liu, Y.; Li, F.; Fan, J.; Liu, F.; Lu, Z.; Yang, J.; Yan, J. Thermal—Fluid—Structure Coupling Analysis of Flexible Corrugated Cryogenic Hose. *China Ocean Eng.* **2022**, *36*, 658–665. [\[CrossRef\]](https://doi.org/10.1007/s13344-022-0058-z)
- <span id="page-14-2"></span>62. Jaiman, R.K.; Oakley, J.O.H.; Adkins, J.D. CFD modeling of corrugated flexible pipe. In Proceedings of the ASME 2010 29th International Conference on Ocean, Offshore and Arctic Engineering, Shanghai, China, 6–11 June 2010.
- <span id="page-14-3"></span>63. Hung Anh, L.D.; Pásztory, Z. An overview of factors influencing thermal conductivity of building insulation materials. *J. Build. Eng.* **2021**, *44*, 102604. [\[CrossRef\]](https://doi.org/10.1016/j.jobe.2021.102604)
- <span id="page-14-4"></span>64. Kalhor, K.; Emaminejad, N. Qualitative and quantitative optimization of thermal insulation materials: Insights from the market and energy codes. *J. Build. Eng.* **2020**, *30*, 101275. [\[CrossRef\]](https://doi.org/10.1016/j.jobe.2020.101275)
- <span id="page-14-5"></span>65. Probert, S.D.; Gian, S. Thermal Insulants. *Appl. Energy* **1976**, *2*, 83–116. [\[CrossRef\]](https://doi.org/10.1016/0306-2619(76)90030-1)
- 66. Villasmil, W.; Fischer, L.J.; Worlitschek, J. A review and evaluation of thermal insulation materials and methods for thermal energy storage systems. *Renew. Sustain. Energy Rev.* **2019**, *103*, 71–84. [\[CrossRef\]](https://doi.org/10.1016/j.rser.2018.12.040)
- <span id="page-14-6"></span>67. Papadopoulos, A.M. State of the art in thermal insulation materials and aims for future developments. *Energy Build.* **2005**, *37*, 77–86. [\[CrossRef\]](https://doi.org/10.1016/j.enbuild.2004.05.006)
- <span id="page-14-7"></span>68. Lucchi, E.; Becherini, F.; Di Tuccio, M.C.; Troi, A.; Frick, J.; Roberti, F.; Hermann, C.; Fairnington, I.; Mezzasalma, G.; Pockelé, L.; et al. Thermal performance evaluation and comfort assessment of advanced aerogel as blown-in insulation for historic buildings. *Build. Environ.* **2017**, *122*, 258–268. [\[CrossRef\]](https://doi.org/10.1016/j.buildenv.2017.06.019)
- <span id="page-14-8"></span>69. He, Y.-L.; Xie, T. Advances of thermal conductivity models of nanoscale silica aerogel insulation material. *Appl. Therm. Eng.* **2015**, *81*, 28–50. [\[CrossRef\]](https://doi.org/10.1016/j.applthermaleng.2015.02.013)
- <span id="page-14-9"></span>70. Li, C.; Chen, Z.; Dong, W.; Lin, L.; Zhu, X.; Liu, Q.; Zhang, Y.; Zhai, N.; Zhou, Z.; Wang, Y.; et al. A review of silicon-based aerogel thermal insulation materials: Performance optimization through composition and microstructure. *J. Non-Cryst. Solids* **2021**, *553*. [\[CrossRef\]](https://doi.org/10.1016/j.jnoncrysol.2020.120517)
- <span id="page-14-10"></span>71. Gurav, J.L.; Jung, I.K.; Park, H.H.; Kang, E.S.; Nadargi, D.Y. Silica Aerogel: Synthesis and Applications. *J. Nanomater.* **2010**, *2010*, 409310. [\[CrossRef\]](https://doi.org/10.1155/2010/409310)
- <span id="page-14-11"></span>72. Choqueuse, D.; Chomard, A.; Bucherie, C. Insulation Materials for Ultra deep sea Flow Assurance—Evaluation of the Material proerties. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 6–9 May 2002.
- 73. Bouchonneau, N.; Sauvant-Moynot, V.; Grosjean, F.; Choqueuse, D.; Poncet, E.; Perreux, D. Thermal Insulation Material for Subsea Pipelines-Benefits of Instrumented Full-Scale Testing To Predict the Long-Term Thermomechanical Behaviour. In Proceedings of the Offshore Technology Conference, Houston, TX, USA, 30 April–3 May 2007.
- 74. Kumar, D.; Alam, M.; Zou, P.X.W.; Sanjayan, J.G.; Memon, R.A. Comparative analysis of building insulation material properties and performance. *Renew. Sustain. Energy Rev.* **2020**, *131*, 110038. [\[CrossRef\]](https://doi.org/10.1016/j.rser.2020.110038)
- 75. Wiprächtiger, M.; Haupt, M.; Heeren, N.; Waser, E.; Hellweg, S. A framework for sustainable and circular system design: Development and application on thermal insulation materials. *Resour. Conserv. Recycl.* **2020**, *154*, 104631. [\[CrossRef\]](https://doi.org/10.1016/j.resconrec.2019.104631)
- <span id="page-14-12"></span>76. Zhao, J.; Wang, X.; Li, S.; Li, Y. Polypropylene fiber reinforced alkali-activated ultra-light foam insulation material: Performance study and mechanism analysis. *Constr. Build. Mater.* **2023**, *405*, 133241. [\[CrossRef\]](https://doi.org/10.1016/j.conbuildmat.2023.133241)
- <span id="page-14-13"></span>77. Ashraf Virk, M.; Mysorewala, M.F.; Cheded, L.; Aliyu, A.R. Review of energy harvesting techniques in wireless sensor-based pipeline monitoring networks. *Renew. Sustain. Energy Rev.* **2022**, *157*, 112046. [\[CrossRef\]](https://doi.org/10.1016/j.rser.2021.112046)
- <span id="page-14-14"></span>78. Wang, J.; Ren, L.; Jia, Z.; Jiang, T.; Wang, G. Pipeline leak detection and corrosion monitoring based on a novel FBG pipe-fixture sensor. *Struct. Health Monit.* **2021**, *21*, 4. [\[CrossRef\]](https://doi.org/10.1177/14759217211044966)

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