

## Article

# Investigating Formation Factor–Hydraulic Conductivity Relations in Complex Geologic Environments: A Case Study in Taiwan

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**Abstract:** The development of cost-effective methods for estimating hydraulic conductivity profiles has been an ongoing effort in the field of engineering practice, which can be used to increase availability to clarify the hydrogeological complexity of fractured rock aquifers for the aid of solving groundwater-related problems. A new methodology is presented, which combines electrical well logs, fluid conductivity logs, double-packer hydraulic tests, Archie's law, and the Kozeny–Carman–Bear equation to investigate relations between formation factor (F) and hydraulic conductivity (K). Available geophysical and hydraulic test data measured from 88 boreholes in fractured rock formations in Taiwan were collected to perform the correlation studies. The correlation investigation outcomes indicate that the established F-K relations have the potential to serve as the transformation function for estimating hydraulic conductivity through the geological directly. To improve F-K relations in response to the effect of clay mineralogy, two proposed clustering techniques (the natural gamma ray threshold method and the modified Archie's law method) successfully play an important role in filtering clayed data. The prevalence of clay content in most of Taiwan's fractured rock formations has been found, which implies that careful consideration of clay-related issues in complex geologic formations is essential while applying Archie's law theory. Finally, the predictive models for estimating hydraulic conductivity have been developed for three types of lithology (sandstone, schist, and slate).



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**Keywords:** hydraulic conductivity; well logging; formation factor; fluid conductivity; resistivity

## 1. Introduction

Hydraulic conductivity plays an essential role in controlling the distribution, flow path, and storage of groundwater in the formation, especially in complex geological environments where this parameter is highly heterogeneous and, as generally recognized, may vary with spatial locations [1–4]. Therefore, if detailed and continuous hydraulic conductivity along boreholes (hydraulic conductivity profiles) can be obtained during the site investigation [5], it will be constructive to clarify the hydrogeological complexity of rock formations [6]. However, such detailed information is not easily obtained due to the limitations of budget, labor, and exploration methods. Most of the projects only take the representative data as the basis to characterize hydrogeological conditions of a site for the assistance of engineering planning and design. When the representative data cannot deal with the complexity of an engineering system, construction accidents may occur, such as large groundwater inflow accidents during tunnel construction [7]. In addition, limited access to detailed data may lead to undiscovered scientific problems related to hydrogeology, or the possible cross-disciplinary applications may be limited by insufficient observed information. Thus, there is a demand for detailed and continuous hydrogeological information for handling vertical heterogeneity in engineering practice and science.

Traditionally, direct field hydraulic tests with the fixed-interval approach can be adopted to determine the hydraulic conductivity profile along a borehole in a geologically complex formation [8]. Although this method can provide detailed information concerning hydraulic conductivity with accurate results, the method is labor-intensive, time-consuming, and costly, as mentioned above. To improve the limitation, down-hole logging tools, such as flowmeter [9–11], electrical well logging [5,12,13], the liner profiling method [14], or NMR (nuclear magnetic resonance) logging [15], have been studied to explore profiles of the hydraulic properties of formations surrounding boreholes. Although these down-hole logging tools can provide higher resolutions, not all tools have the advantage of low cost while estimating hydraulic conductivity. Additionally, geophysical data measured from these tools still need to combine transform functions to obtain hydraulic conductivity, and these studies have not yet been fully developed [5,10,12,14,15].

Inexpensive and less time-consuming methods with high resolution for estimating such a profile increase their worth in practical applications. Among these logging tools, electrical well logging meets the criteria of relatively inexpensive survey costs and high resolution. Although most of the downhole electrical logging signals are mainly used to identify the profiles of lithology, porosity, hydraulic property, cementation, strength, and water-bearing zones of a formation in a qualitative way, a few studies have attempted to utilize such data to estimate hydraulic conductivity.

Since 1951, studies have focused on exploring electrical–hydraulic relationships for groundwater exploration [16]. In the early times, previous studies utilized electrical well-logging data to calculate values of the formation factor [17], and then establish direct relationships between electrical data and hydraulic conductivity [17–20]. The later studies used a two-step approach to construct the electrical–hydraulic relationship. First, electrical well-logging data were utilized to calculate values of the formation resistivity factor and then estimate the porosity using Archie’s law [17,21]. Second, the predicted porosity is typically used in conjunction with the Kozeny–Carman model to estimate hydraulic conductivity. The abovementioned methodology has been presented in the literature [5,12,13,22,23]. These studies also pointed out that Archie’s law and Kozeny–Carman model are only validated in sandy strata. If clayed or shaley formations are present in the analysis, estimation results are inferior. To improve electrical–hydraulic relationships in response to the effect of clay mineralogy, the modification of Archie’s law was proposed by Waxman and Smits [24]. Few studies have considered the new law to improve electrical estimations from hydraulic conductivity [5,12]. In addition, electrical–hydraulic relationships developed from most of the previous studies were focused on unconsolidated formations. Such relationships are less well developed in fractured rock formations. Due to their geologic complexity, obtaining a good result on the electrical–hydraulic relationship could become challenging.

In this study, relations between hydraulic conductivity and electrical data in complex geologic environments of Taiwan, where fractured rock aquifers with diverse lithologies are commonly present, were investigated. Available geophysical and hydraulic data measured from 88 boreholes using the electrical well-logging tools and double-packer hydraulic test were collected to perform the correlation studies. The main tasks include (a) inspection of the quality of the geophysical data by comparing the existing drilling core data with the consistency of actual lithology; (b) investigation of correlations between hydraulic conductivity and geophysical parameters (spontaneous potential, short normal resistivity, long normal resistivity, point resistivity, natural gamma, and fluid conductivity); (c) classification of collected data with/without clay contents by using two proposed clustering approaches; and (d) feasibility studies for establishing the relationship between the formation factor and hydraulic conductivity over various lithologies in fractured rock formations.

## 2. Study Area and Data Sources

A twelve-year program related to groundwater resource explorations in Taiwan’s mountainous areas was initiated by the Central Geological Survey of Taiwan in 2010 [25].

The main objective of this program is to explore the potential of using groundwater extracted from fractured rock formations as alternative water resources against drought. To understand the feasibility of this concept, hydrogeologic data in regolith-bedrock aquifers over the entire Taiwan mountain areas through various hydrogeological investigation tests were collected and analyzed to support the purpose of this program. Figure 1 shows the distribution of the investigated borehole locations in the mountainous area of Taiwan for the program mentioned above from 2010 to 2021. Each investigated borehole conducted seven in situ hydrogeological tests, including electrical well logging, fluid conductivity logging, temperature logging, groundwater velocity logging, borehole imaging, double-packer hydraulic test, and pumping test. The total investigated boreholes and the depth of each borehole are 88 and 100 m, respectively.

To develop a model for determining the hydraulic conductivity of mountainous formations along a borehole, this study collected samples from a part of the above-mentioned hydrogeological tests. The analyzed data mainly aimed at survey data from the electrical well logging (spontaneous potential, short normal resistivity, long normal resistivity, point resistivity, and natural gamma), fluid conductivity logging, and double-packer hydraulic test. Data samples for each borehole were selected from the borehole sections by performing double-packer hydraulic tests (the test interval of 1.5 m). A total of 396 double-packer hydraulic test samples were collected. In addition, the electrical well logging and fluid conductivity logging have one-centimeter data sampling, which can meet this study's research goal of high resolution. Finally, each borehole's drilling core logs and image data confirmed whether the geophysical values can reflect the lithology presented.

The lithological environment covered by the collected data samples includes quartz sandstone, sandstone, sandstone interbedded with shale, silty sandstone, sandy shale, shale, alternations of sandstone and shale, mudstone, siltstone, argillaceous siltstone, andesite, volcanic agglomerate, phyllite, marble, slate, schist, gneiss, argillite, quartzite, metasandstone, and argillite interbedded with some sandstone. The number of data samples collected for each sub-lithology is shown in Table 1. Among the analyzed data, the five most abundant rock types include sandstone, slate, alternations of sandstone and shale, schist, and shale. The above data collected can construct electrical parameters to hydraulic conductivity, followed by statistical techniques to possibly develop reliable models for predicting hydraulic properties of various subsurface formations. Due to the wide range of geological environments covered by the data sources collected, the formation factor–hydraulic conductivity relation can be investigated more comprehensively.

**Table 1.** Statistics of lithology for the data samples collected from the double-packer hydraulic test.

Main Lithology	Sub-Lithology	Amount
Sedimentary rock	Sandstone	93
	Shale	31
	Sandy Shale	3
	Sandstone interbedded with Argillite	2
	Mudstone	8
	Siltstone	14
	Silty Sandstone	20
	Alternations of Sandstone and Shale	44
	Argillaceous Siltstone	5
	Quartz Sandstone	6
Igneous rock	Andesite	7
Metamorphic rock	Volcanic Agglomerate	6
	Phyllite	6
	Slate	61
	Schist	41
	Marble	6
	Gneiss	5
	Argillite	18
	Metasandstone	3
	Argillite interbedded with some Sandstone	10
	Quartzite	7
	Total	396

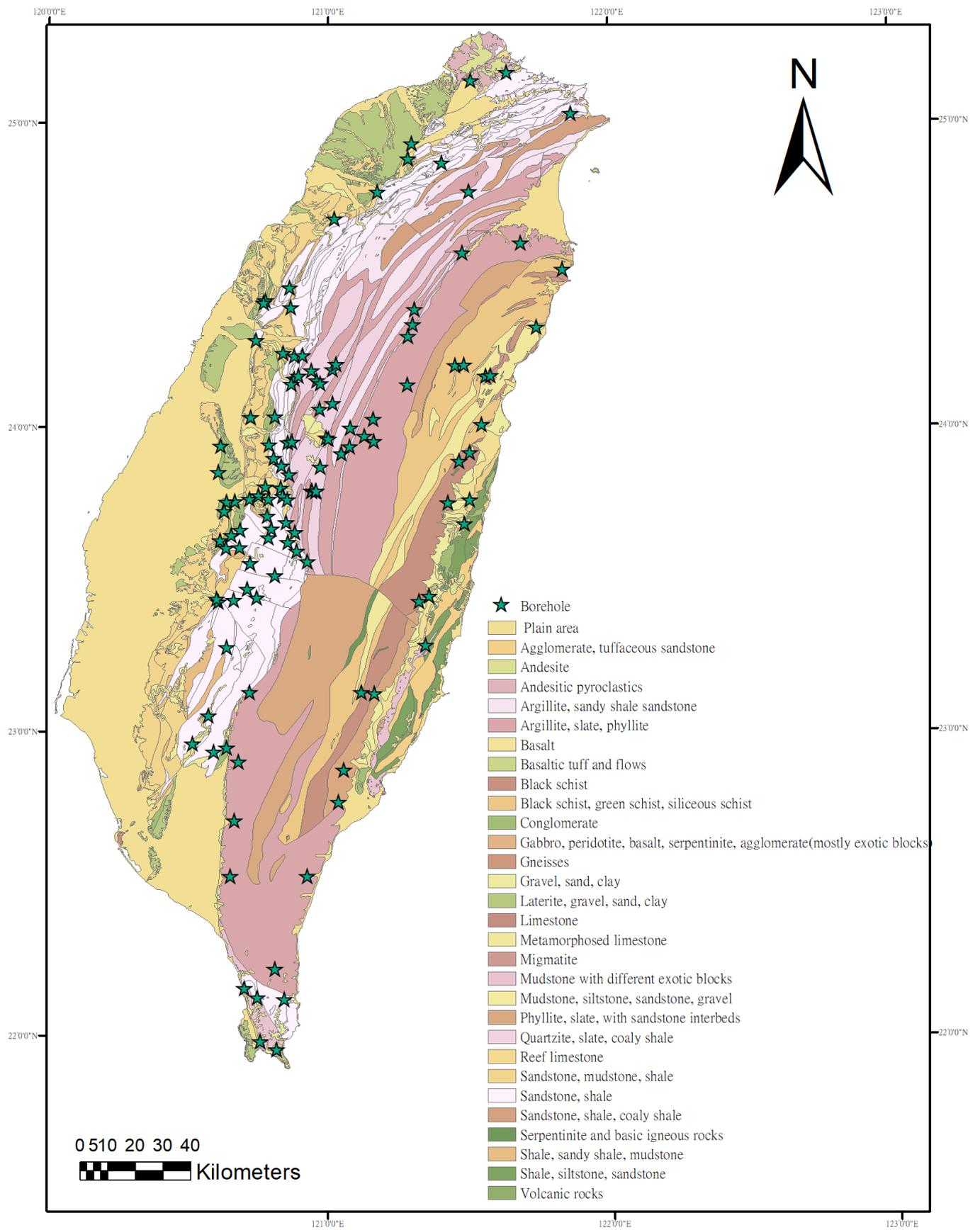
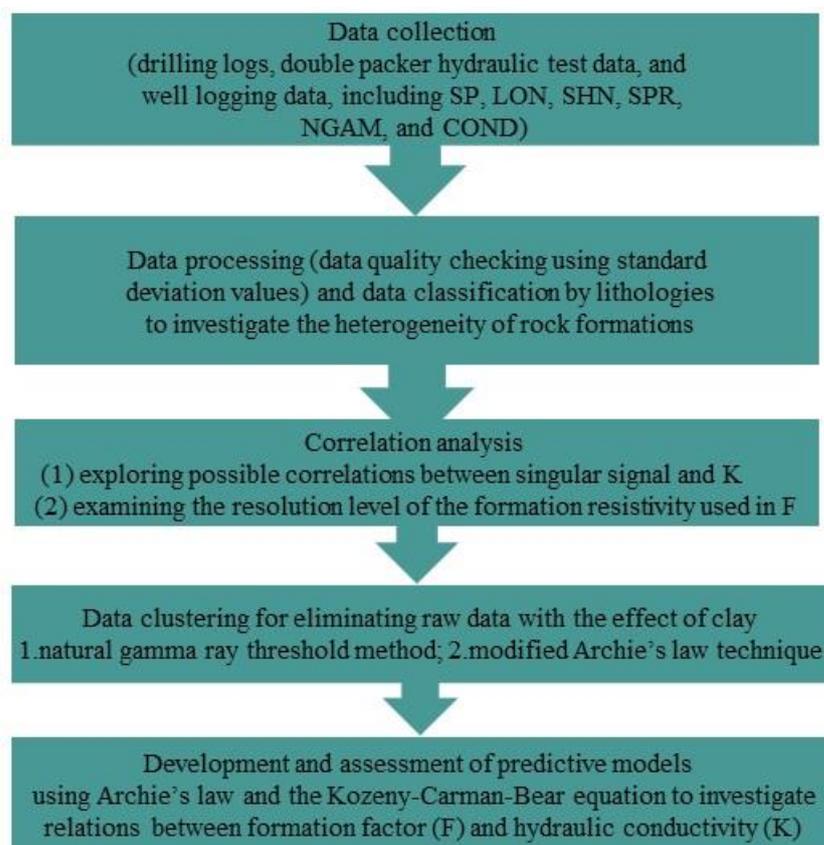


Figure 1. The study area and locations of investigated boreholes.

### 3. Methods

To provide a cost-effective approach for producing hydraulic conductivity profiles along boreholes, this study intends to explore relationships between the formation factor and hydraulic conductivity using the resistivity data of formation and fluid obtained from the most commonly used electrical well logging in drilling construction and the theory of Archie's law. A flowchart summarizing the implementation of this study for developing the estimation of hydraulic conductivity is shown in Figure 2. Five investigation stages are illustrated, including (1) collecting borehole data, including drilling logs and a variety of well-logging data (spontaneous potential, short normal resistivity, long normal resistivity, point resistivity, natural gamma, and fluid conductivity); (2) classifying the raw data by lithology as well as examining the quality of the collected data compared with the existing rock core logs; (3) performing correlation analysis by investigating relations between hydraulic conductivity and each geophysical parameter; (4) proposing two data clustering methods to eliminate raw data with the effect of clay contents; and (5) establishing the relationship between the formation factor and hydraulic conductivity according to the clustered data as well as evaluating the feasibility of the developed models.



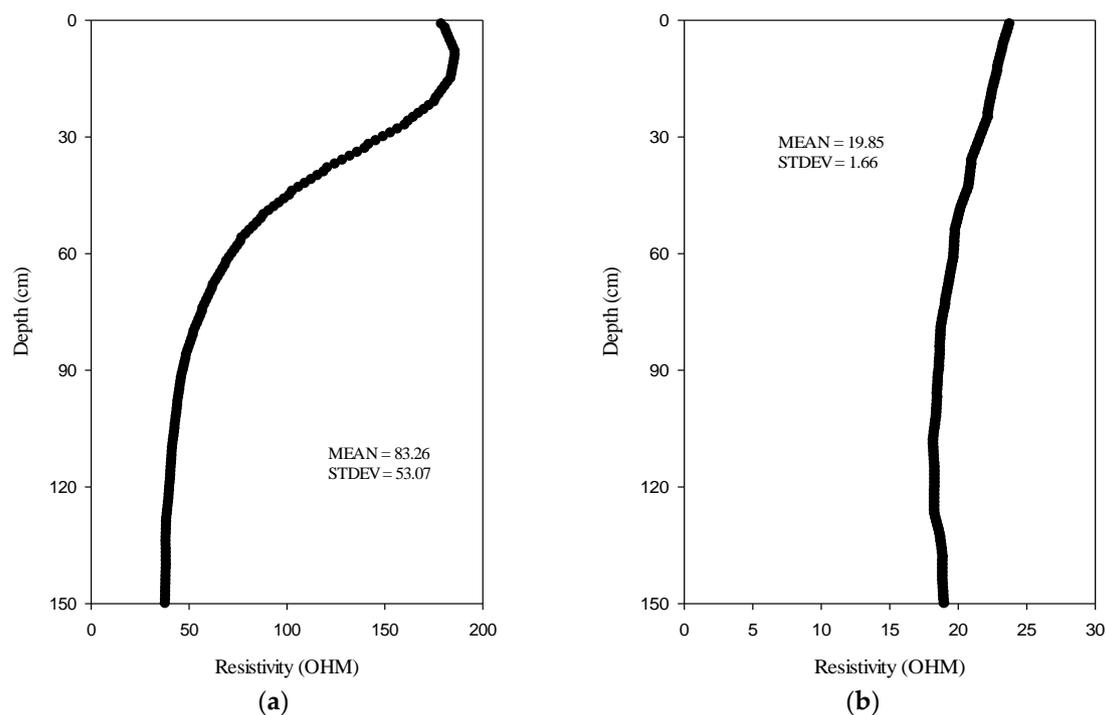
**Figure 2.** Flowchart for investigating formation factor–hydraulic conductivity relationships.

#### 3.1. Data Processing and Classification

Generally, the electrical well-logging signal data are used to infer the stratum's lithology by using geophysics principles on an indirect basis, which is different from geologists' direct visual recording of lithology. Both methods have their own advantages and disadvantages. The electrical signal data are recorded every centimeter, while the artificial core description is recorded every 20 cm, so the resolution of the latter data is much rougher than that of the former. Taking the 1.5 m test section of the double-packer hydraulic test as an example, geologists can only describe the main lithological features in the test section. Also, due to the visual identification method, it is impossible to describe the lithology for

the finer parts. However, the electrical measurement data can be used to infer the difference in lithology in a test interval through variations of the signal value.

To confirm whether numerical changes of these signals correctly reflect the actual lithology, this study collected five types of signals (including spontaneous potential (SP), long normal (LON), short normal (SHN), single-point resistivity (SPR), and natural gamma ray (NGAM)) of double-packer test sections in different boreholes with different depths. A total of 150 points were measured for each signal in the 1.5 m double-packer test interval. For each test section at a given signal, the average value and standard deviation (SD) value of all samples were calculated. For the section with a large SD value, the data were compared and verified by core logs and photos to confirm that lithology rather than artificial errors caused the greater deviation. Figure 3 shows the short normal resistivity profiles at two different double-packer intervals (1.5 m), and the geologists described the cores of both intervals as fine-grained sandstone. However, while comparing Figure 3a,b, the resistivity value of the entire vertical interval in Figure 3b has little difference (SD value is about 1.66), but the resistivity value of the whole vertical section in Figure 3a shows a larger variation (SD value is about 53.07). Thus, Figure 3b may be more in line with the result of the lithological description, so the signal quality of the double-packer interval in Figure 3a should be rechecked. In particular, the signal results obtained in a relatively complex geological environment need to be compared carefully with the existing core data to confirm the correctness of the collected signal data so that the signal values used can appropriately reflect the hydraulic conductivity value of the formation. After the quality control of the data, the confirmed data can be classified into a different group by lithology and used for subsequent statistical analysis.



**Figure 3.** The short normal resistivity profiles at two different double-packer intervals. (a) Abnormal resistivity profile. (b) Normal resistivity profile.

### 3.2. Theory of Formation Factor–Hydraulic Conductivity Relation for Clay-Free Formations

Formation factor  $F$ , or formation resistivity factor, was initially presented by Archie [17] and defined as the ratio of the resistivity of a fully water-saturated granular reservoir rock ( $R_o$ ) to the resistivity of the water saturating the pores ( $R_w$ ). Archie [17] also proposed the relation between  $F$  and porosity  $n$ . Since 1942, the  $F$ - $n$  relation has been confirmed

empirically in a variety of singular formations. The relation is commonly expressed in the following form [21].

$$F = \frac{R_o}{R_w} = an^{-m} \quad (1)$$

where  $a$  is the tortuosity constant or lithology constant, and  $m$  is the cementation factor. The values of  $m$  and  $a$  have been reported for different formations by different investigators [26]. The reported ranges for two parameters in a specific lithology are variable. The reason for such variations can be attributed to several factors, including size, packing and sorting of grains, degree of cementation, porosity, pressure, tortuosity, wettability of rock surface, and clay content. The last factor is especially significant due to violating Archie's original experimental conditions. Thus, a meaningful evaluation for Equation (1) is based on accounting for the clay content effect. Additionally, if  $a$  is equal to one, Equation (1) is called Archie's first law. While applying both equations, discussions on the difference between Equation (1) and Archie's first law can be referred to the study of Glover [27].

Based on the above relation of Equation (1),  $n$  can be theoretically obtained from  $F$ . However, valid relations between  $F$  and  $K$  generally do not exist. However, several studies have developed for the valid relations between  $K$  and  $n$ , which can be found in a textbook [5,12]. One of the famous relations comes from the Kozeny–Carman–Bear equation given by Bear [28] and Domenico and Schwartz [29].

$$K = \left[ \frac{\delta_w g}{\mu} \right] \cdot \left[ \frac{d^2}{180} \right] \cdot \left[ \frac{n^3}{(1-n)^2} \right] \quad (2)$$

where  $\delta_w$  is the dynamic viscosity;  $g$  is the acceleration gravity;  $\mu$  is the fluid density;  $d$  is the mean grain size;  $n$  is the porosity. Equation (2) is developed by the concept of the capillary tubes and often estimates the saturated  $K$  for most soils [30].

Since formation factor  $F$  and hydraulic conductivity  $K$  are both functions of porosity  $n$ , integrating Equations (1) and (2) links the two parameters  $F$  and  $K$ . The functional relationship between  $K$  and  $F$  can be assumed to be established and given as:

$$K = \text{Fucntion}(F) \quad (3)$$

In fact, such a relationship has been used in previous studies to estimate hydraulic conductivity [5,12,22,31,32]. However, the relationship was confirmed with a small size of data and a clay-free lithology. Thus, this study applied the functional relationship to investigate formation factor–hydraulic conductivity relations in various complex geologic environments.

### 3.3. Data Clustering for Eliminating Data Containing Clay Content

Since Archie's law is only applicable to the clay-free formation, the application of Equation (3) for establishing the relationship between  $F$  and  $K$  for the study area in the relatively complex geological conditions of the Taiwan mountains requires testing the data first for clustering those that are compatible with the original theory. Accordingly, this study proposes two different clustering methods to screen the data samples less affected by clay minerals to conform to the theoretical formula of Archie's law. The clustering methods and theories are detailed as follows:

#### (a) Natural Gamma Ray Threshold

The natural gamma ray (NGAM) has the characteristic of strongly distinguishing the clay mineral in a formation. Therefore, the natural gamma ray may be used to design the threshold value for recognizing clay minerals. When the average NGAM value of a formation sample is larger than the threshold value, the sample may contain clay minerals. Such a sample should be excluded in the subsequent analysis of the correlation with hydraulic conductivity. Using natural gamma ray thresholds to confirm whether a formation is affected by clay mineral effects has been investigated by Kaleris and Zioga [5] at a site in Greece. His study suggested that strata are less affected by the clay mineral effect when the

natural gamma ray value in API (American Petroleum Institute) is less than 35. According to the previous study, the design of the NGAM threshold may be the key to determining the presence of clay minerals.

The NGAM threshold can be obtained by dichotomy to group data samples into two categories, which may contain clay or non-clay content, to find a possible NGAM threshold value. Then, the correlation of F and K can be performed on the grouped data with the non-clay content. If the correlation outcome is good, it implies that Archie's law can apply to the analyzed data set. The NGAM value of splitting into two groups can be the threshold for recognizing clay content. However, this splitting method does not consider the nature of the distribution of the data itself. Thus, the frequency distribution of NGAM in the collected data set was utilized to summarize the information on the number of occurrences of class intervals in a given NGAM range. The number of class intervals can be calculated as the following equation.

$$P = 5 \times \log_{10}(N) \quad (4)$$

where  $N$  is the total amount of collected samples.  $P$  is the number of class intervals. If  $P$  is a decimal number, rounding this decimal number to the nearest whole number is needed. Based on the rounded  $P$  number, the frequency of data belonging to each class interval is plotted in a frequency distribution figure, which is also called a histogram. Each data set collected in this study was able to use this technique to obtain the frequency pattern of NGAM. The higher class interval has larger NGAM values, which may be more likely to contain clay minerals. Subsequently, a stepwise deletion process of sample data from the class interval (starting from the highest class interval) was carried out, and correlations between F and K were performed for each group of screened samples. The analyzed correlation levels were used to determine the natural gamma ray threshold value that could recognize the existence of clay minerals in the samples.

#### (b) Modified Archie's law

Initially, Archie's law does not consider the influence of clay minerals in a formation. For the geological environment where clay mineral exists, applying this theory to predict porosity generally does not work well [26]. The main reason is that clay mineral has a high degree of ion exchange and a high specific surface area [24,33]. Formations with higher clay minerals may reduce the correlation between resistivity and hydraulic conductivity. Later, some studies based on Archie's law [24,26] proposed a modified Archie's equation incorporating the effect of clay minerals, which is given below.

$$F_a = F_c \times (1 + BQ_v R_w)^{-1} \quad (5)$$

Among them,  $F_a$  is the apparent formation factor;  $F_c$  is the corrected formation factor;  $R_w$  is the resistivity of the water saturating the pores;  $Q_v$  is the cation exchange capacity; and  $B$  is the equivalent conductivity of each cation. After proper rearrangement, Equation (5) can be presented as a linear relationship between  $1/F_a$  and  $R_w$ .

$$\frac{1}{F_a} = \frac{1}{F_c} + \left( \frac{BQ_v}{F_c} \right) R_w \quad (6)$$

$BQ_v/F_c$  stands for the gradient [26]; the data of  $R_w$  (x-axis) and  $1/F_a$  (y-axis) are plotted, and then the simple linear regression formula is obtained by using regression analysis. The intercept of the regression formula is  $1/F_c$ , and its value is calculated by inversion to obtain  $F_c$ .

Afterward, a dimensionless value ( $F_a/F_c$ ) is calculated by dividing the uncorrected apparent formation factor ( $F_a$ ) and the corrected formation factor ( $F_c$ ) calculated by the correction method addressed above. A clay-free formation may be expected if  $F_a/F_c$  is greater than or equal to 0.9 [26]. The criterion indicated by Worthington [26] can be used to separate the collected samples into clay-bearing and clay-free sample groups for data clustering. The clay-free sample group can meet the original Archie's law theory hypothesis,

and the samples can be utilized to establish relations between the formation factor and hydraulic conductivity.

Therefore, data samples in complex geological environments clustered by the above two techniques (a) and (b) can be used to recognize the clay-free conditions of the samples. It may assist in improving the establishment of estimation models for predicting hydraulic conductivity through downhole resistivity data.

## 4. Results and Discussion

### 4.1. Data Processing Result

In this study, the data quality control procedures mentioned in Section 3.1 were used to eliminate the samples whose electrical signal data were inconsistent with the actual lithology, and the consistent samples were subjected to basic descriptive statistical analysis. Five data samples out of 396 were not included in the subsequent analyses. For the remaining 391 data samples, the sample data of various electrical signals in the 1.5 m double-packer hydraulic test section with different depths in different boreholes were compiled. One hundred fifty measurements in the test section were recorded for each signal sample, and each sample's mean and standard deviation were calculated. Then, all samples were classified into three group data categories: singular lithology, three major rock types, and entire data. The mean and standard deviation for each group type of data were calculated as shown in Table 2.

**Table 2.** Descriptive statistics of six well-logging signals for various rock types.

Category	Signal Type	SP (V)		NGAM (cps)		COND (ohm.m)	
	N	$\mu$	S.D.	$\mu$	S.D.	$\mu$	S.D.
All lithologic types	388	141.81	155.80	121.02	38.61	598.91	704.94
Sedimentary Rock	230	127.49	129.31	114.77	30.93	634.64	608.68
Sandstone	90	97.59	147.39	105.02	31.42	238.39	479.28
Shale	30	147.15	97.09	129.37	20.23	810.53	393.21
Sandy Shale	3	112.41	2.73	135.09	5.46	357.70	10.84
Sandstone interbedded with Argillite	10	182.97	88.13	150.42	13.17	475.71	433.32
Mudstone	8	153.16	12.01	75.20	43.42	660.81	177.84
Siltstone	14	127.85	81.40	125.69	14.60	1430.85	1018.14
Silty Sandstone	20	179.10	168.03	102.14	22.45	324.68	129.65
Alternations of Sandstone and Shale	44	135.32	104.48	124.28	27.52	468.51	374.78
Argillaceous Siltstone	5	61.72	6.04	106.40	7.05	476.60	10.33
Quartz Sandstone	6	182.97	216.57	123.38	41.24	2100.29	1459.38
Igneous Rock	13	238.67	168.08	43.35	26.55	359.45	96.49
Andesite	7	124.80	66.79	59.53	7.32	329.46	63.19
Vocanic Agglomerate	6	371.52	152.05	24.48	28.88	394.43	121.77
Metamorphic Rock	145	155.86	186.87	137.85	39.11	563.72	859.02
Phyllite	6	458.57	17.38	155.20	4.95	861.69	55.67
Slate	57	133.41	165.13	157.13	26.16	782.87	1213.49
Schist	41	155.60	202.61	119.14	35.60	375.59	120.84
Marble	6	130.69	15.25	46.27	15.65	244.82	46.86
Gneiss	5	−55.84	22.01	143.68	5.69	269.90	142.64
Argillite	18	203.31	169.42	157.10	23.74	277.10	225.91
Metasandstone	3	463.68	4.05	136.56	34.48	131.96	12.33
Argillite interbedded with some Sandstone	2	49.03	70.90	153.44	18.23	168.15	2.17
Quartzite	7	30.03	127.06	96.60	42.01	1186.50	1339.26

Table 2. Cont.

Category	Signal	SHN (ohm.m)			LON (ohm.m)		SPR (ohm.m)	
		N	$\mu$	S.D.	$\mu$	S.D.	M	S.D.
All lithologic types		388	288.70	596.58	243.23	446.49	182.30	260.95
Sedimentary Rock		230	124.45	254.45	123.47	214.02	106.12	140.89
Sandstone		90	207.92	366.58	176.30	289.81	161.32	193.35
Shale		30	35.69	33.42	56.02	48.89	40.64	28.14
Sandy Shale		3	30.40	7.35	38.85	6.28	58.89	7.84
Sandstone interbedded with Argillite		10	277.11	228.22	330.14	247.94	176.69	100.96
Mudstone		8	14.27	4.93	17.66	2.94	28.19	11.50
Siltstone		14	27.87	11.44	47.34	27.40	31.32	13.51
Silty Sandstone		20	60.82	82.72	104.34	148.53	73.49	58.88
Alternations of Sandstone and Shale		44	63.51	79.04	87.46	135.64	82.45	69.08
Argillaceous Siltstone		5	9.54	1.15	12.09	1.21	21.00	1.22
Quartz Sandstone		6	225.83	222.09	105.54	85.37	148.34	173.97
Igneous Rock		13	375.77	590.63	254.86	373.40	217.36	209.74
Andesite		7	618.32	739.84	399.87	474.51	330.52	232.63
Volcanic Agglomerate		6	92.78	43.96	85.68	25.45	85.35	42.46
Metamorphic Rock		145	541.43	846.39	433.46	627.32	300.01	352.76
Phyllite		6	523.33	120.23	513.80	79.44	190.98	42.20
Slate		57	314.15	250.56	290.28	261.60	188.74	93.86
Schist		41	379.55	417.83	289.07	305.18	238.53	139.27
Marble		6	3973.34	1417.58	2864.96	1171.03	1606.99	850.91
Gneiss		5	1329.79	327.79	1031.72	195.14	737.45	118.70
Argillite		18	315.24	316.01	226.36	171.24	291.30	186.95
Metasandstone		3	373.64	134.02	384.41	125.77	312.53	39.43
Argillite interbedded with Sandstone		2	211.48	141.82	216.72	81.60	205.53	75.00
Quartzite		7	598.84	467.85	491.71	393.95	270.94	181.78

Note: the COND in this table is the reciprocal of the original COND, which was transformed into electrical resistivity.

When comparing the standard deviations of the three categories, most of the singular lithology categories have relatively small standard deviations. A greater standard deviation means that the dispersion of the data is relatively large. If these data are used to develop a hydraulic conductivity predictive model, the prediction model's performance may not be good. Therefore, the statistical results of the underlying data imply the importance of data classification or clustering in the development of the estimation model. In addition, comparing the differences in the standard deviations of various signals, it is found that the standard deviation of the NGAM signal is smaller than other signals in each classification group. It is speculated that this signal is less susceptible to the external factors of the well (borehole size, the effect of the invasion of the mud filtrate into the formation, the heterogeneity of geologic formation, the salinity or conductivity of groundwater), while other signals are more affected by these external factors of the well. The standard deviation of the COND signal has the largest variation value, indicating that the mud may affect the fluid in the borehole. The variation of the SHN signal is larger than that of the LON signal, probably because the SHN signal reflects the resistivity value of the mud-infiltrated area and is more significantly affected by the mud. However, the LON signal reflects the formation resistivity and is less affected by mud. Therefore, the standard deviation variation can be used to understand the geology heterogeneity and the signal's degree of influence by external factors in each double-packer test section.

Furthermore, box plots were used to demonstrate the distributions of numeric signal data values and the comparisons between multiple groups. First, the selection of box plot

data is based on a single lithological group with a sample size of more than 20 and no mud or shale contents. The single lithology groups that meet these selection criteria include sandstone, slate, and schist. Then, six different signal box plots were drawn for the three single lithological groups, as shown in Figure 4. The outlier points shown in Figure 4 lie outside the 10th and 90th percentiles as black circle symbols. The number of outliers and the dispersion of the primary data points for the three lithological groups were compared from the box plots of the five signals, which were used to determine the lithology of the strata. This comparison reveals that the numerical value distribution of sandstone data is more dispersive than the other two lithologies. This result is consistent with the results of the standard deviation analysis in Table 2. However, the comparison for the signal of determining the formation's fluid conductivity reveals that the slate data points are the most scattered, followed by sandstone. This result can be used to explain how strongly the formation fluid was affected by the drilling mud fluid in the borehole at the time of the test. Therefore, for the samples with the same lithology recorded manually, the results of the box plots drawn from the downhole exploration data with higher resolution data can be used to identify whether there is geological heterogeneity in the samples, which can help the development of estimation models.

Based on the analysis results of the collected data, it can be concluded that (1) preliminary data quality control is of great importance because these signal data are susceptible to external factors; (2) these signal data can help further investigate the heterogeneity of the rock formations than the visual description data recorded by geologists; and (3) the high degree of geological heterogeneity of the study site has been found, and this result suggests that it is more appropriate to establish the hydraulic conductivity estimation model based on a single lithology type.

#### 4.2. Correlation Analysis for Various Well-logging Signals with Hydraulic Conductivity

The correlation analysis for well-logging signals was performed to (1) explore possible correlations between singular signal and hydraulic conductivity and (2) examine the resolution level of the formation resistivity used in the formation factor. This study correlated each signal with hydraulic conductivity. Normality tests for each signal were conducted to determine parametric or non-parametric statistical methods utilized to quantify the level of association between the various signals and hydraulic conductivity. The bivariate correlation analysis, then, was adopted to examine correlations between the various signals and hydraulic conductivity.

Firstly, the normal testing outcomes pointed out that the null hypothesis for a sample from a normally distributed population was rejected for most of the signals. However, most of the signals did not pass the normality test. Thus, Spearman's correlation was used to quantify the association between each signal and hydraulic conductivity. In addition, a significance level ( $p$ -value) of 0.05 with the two-tailed test was used for all correlation results in this study. If the results of significance testing show that the  $p$ -value is greater than 0.05, the correlation value is not meaningful.

Table 3 lists various signals that were analyzed for the correlation study. The correlation analysis items include hydraulic conductivity vs. SP, SHN, LON, SPR, NGAM, and COND. The analyzed data herein were selected from Table 1 for different lithological data groups, including all lithological rocks, sedimentary rock, igneous rock, metamorphic rock, sandstone, slate, and schist. In addition, Table 3 marks the correlation coefficient as a hyphen symbol if the significant testing does not pass. Based on meaningful correlation results for the all-lithologic type, the correlation results of SP and NGAM signals are insignificant among the six signal types. The possible main reason is that the formula for calculating the formation factor needs to come from the formation resistivity. Although the correlation between NGAM and K values is not meaningful, the NGAM signal is a crucial indicator for determining the presence of mud in the geological strata. Therefore, in the subsequent data clustering process, the NGAM values were used as the threshold to categorize the data samples into mud-containing and free groups for data clustering purposes.

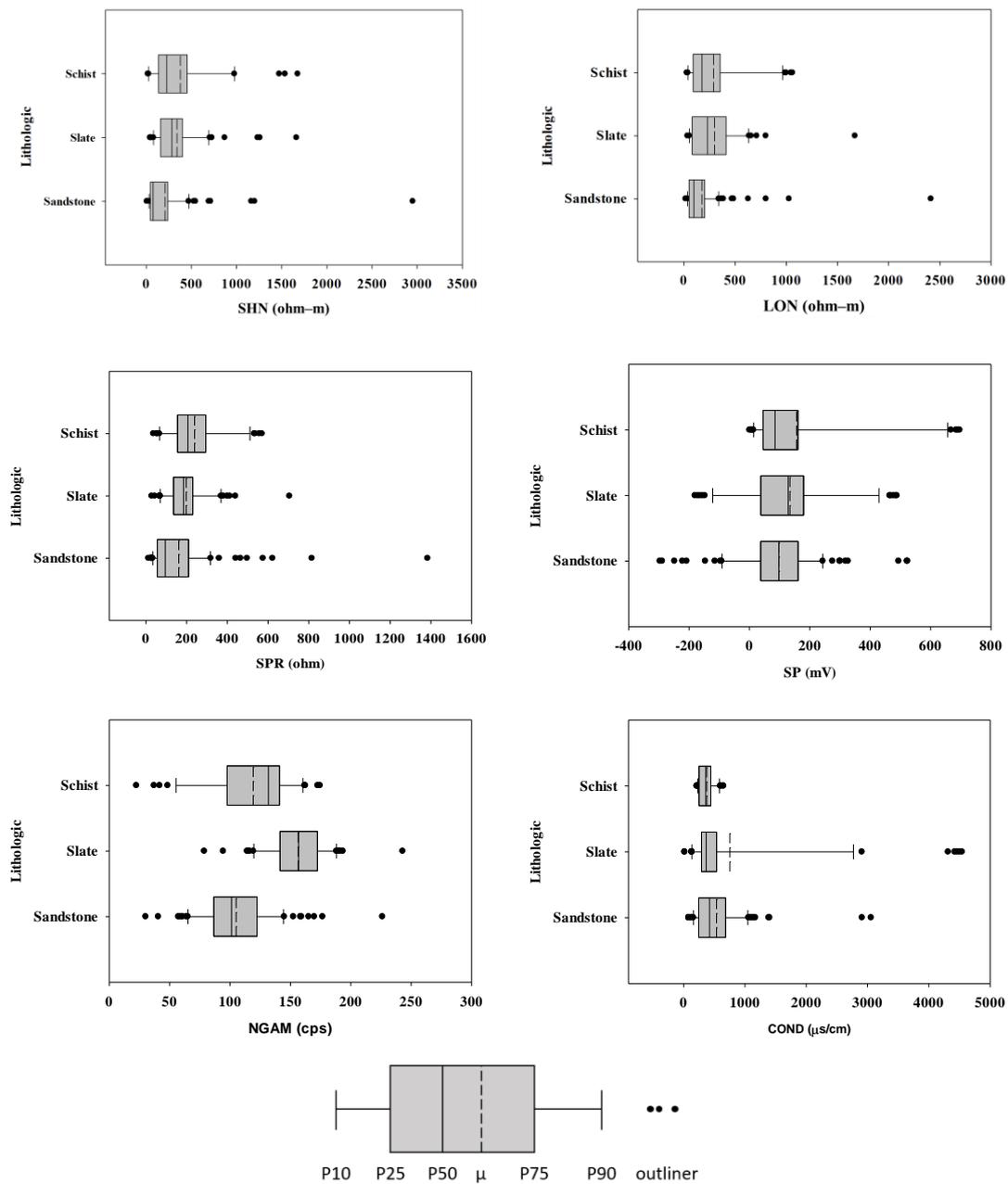


Figure 4. Box plots for demonstrating the distributions of various signals with three major lithologies.

Table 3. Correlation outcomes between k and various signal types with various lithologic groups.

Signal Type	All Lithologic Type	Sedimentary Rock	Igneous Rock	Metamorphic Rock	Sandstone	Slate	Schist
Sample quantity	391	230	13	148	90	60	41
SP	-	-	-0.613	-	-	-	-
SHN	0.343	0.575	0.732	-	0.442	-	-
LON	-0.277	0.480	-	-	0.397	-	-
SPR	-0.378	0.549	0.765	0.245	0.490	-	-
NGAM	-	-	-	-	-	-	-
COND	-0.308	-0.281	-	-0.355	-0.338	-	0.345

Note: “-” stands for “the significant testing fails”.

In addition, the meaningful correlation coefficients shown in Table 3 exist in SHN, LON, SPR, and COND signals. According to Cohen's guideline [34] for interpreting the level of correlation from Spearman's coefficient, the strength of the relation for SHN, SPR, and COND reaches the medium strength (0.3–0.5). The strength of the relation for LON belongs to the low strength (0.3–0.1). While looking at other data groups for specific lithology, the strength of the relation for these meaningful signals may increase. The increased correlation strength, which is up to the level of the strong strength, depends on the lithology. The correlation analysis results regarding the three electrical resistivity signals (SPR, SHN, and LON) show that the strength of their associations, from best to worst, is in the order of SPR, SHN, and LON. The electrical resistivity value is commonly used as an essential parameter for estimating the formation factor (F) of formation. Based on the correlation strength of electrical resistivity results, theoretically, F should be calculated using the best-correlated signal, SPR. However, the electrical well-logging data from SPR is typically used only as a supplementary tool to determine the presence of fractures and groundwater flow in rock formations. The electrical resistivity values for lithological characterization are usually determined by SHN and LON signals. Therefore, the SHN signal was adopted in this study, which showed a stronger correlation with K for estimating the F values. The correlation of SHN that is better than that of LON was also confirmed by previous studies [5,13]. For estimating the formation factor, SHN is utilized as it assures a greater resolution of the formation than LON.

Finally, the correlation between COND and K revealed a certain degree of negative correlation. The connection between these two parameters was not expected, as the COND values were initially intended to understand the water quality around a drilling well. However, a plausible explanation for this connection is that higher COND values indicate relatively more polluted water quality, possibly due to the poor permeability of the strata, resulting in the groundwater flowing poorly in the stratum. As a result, the analysis shows a negative correlation where higher COND values correspond to smaller K values. Although COND may correlate with K, COND is not directly used to estimate K. Instead, the reciprocal of COND was transformed into electrical resistivity, which is used as the resistivity of the water saturating the pores ( $R_w$ ), as shown in Equation (1). It is then combined with SHN to calculate F.

#### 4.3. Data Clustering Results

To address the influence of clay minerals on the correlation between F and K, this study first utilized the findings from Section 4.2, which showed a higher correlation between single lithological well-logging data and hydraulic conductivity as the basis for data samples classification. Furthermore, two data clustering methods from Section 3.3 were employed to progressively eliminate data samples containing clay minerals from each single lithological group. The remaining samples can be the basis for constructing models to estimate K from F. The detailed outcomes of the two data clustering methods are summarized below.

##### 4.3.1. Outcomes from the Natural Gamma Threshold Method

This study classified the data population based on individual lithological data (Table 2). Three individual lithological groups were selected among these data groups, namely sandstone, slate, and schist. The selected criteria were based on the data group with a sample size of more than 20 and did not contain clay minerals in lithological compositions. These filtered groups were subjected to the NGAM threshold clustering analysis. Using Equation (4), the frequency distribution figure of NGAM for each single lithology type was plotted in Figure 5. Based on each histogram, the higher class interval was supported to have a greater NGAM value that may contain clay minerals. A relatively better correlation can gradually be found by deleting clay-contained data samples from the highest-class interval with performing correlation analysis between F and K for each filtered data group. Tables 4–6 show the process of correlation variations with different data groups for

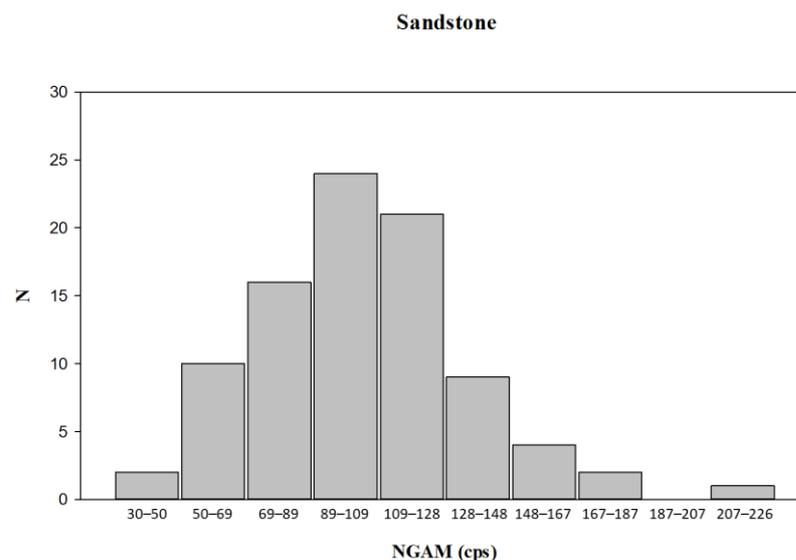
sandstone, slate, and schist, respectively. As seen in Table 4, the correlation coefficient of Spearman between F and K gradually increased by deleting samples with higher NGAM values. When the NGAM value of the data is between 30 and 90, Spearman’s coefficient is greater than 0.5, which reaches the minimum lower limit of the strong strength according to Cohen’s guideline [34]. The Spearman’s correlation coefficient increased from 0.159 (all data samples) to 0.572 ([30,89] data samples), and the maximum correlation coefficient value is statistically significant (the *p*-value is less than 0.05). Therefore, in this case, NGAM equal to 89 is used as the threshold value for sandstone clustering. Values above this threshold indicate intervals containing mud, while values below suggest intervals with very low mud content or being clean. However, the correlation coefficient between F and K shows a positive relationship, meaning that as F increases, K also increases. This contradicts the theory of Archie’s law and Kozeny–Carman–Bear equation, implying that the samples selected using NGAM equal to 89 as the threshold might still contain some muddy samples or incomplete data of clean sand, which may include some quantities of mud. However, such an empirical relationship requires more data to be proved.

**Table 4.** Correlation variations with various filtered data sets for the lithological group of sandstone.

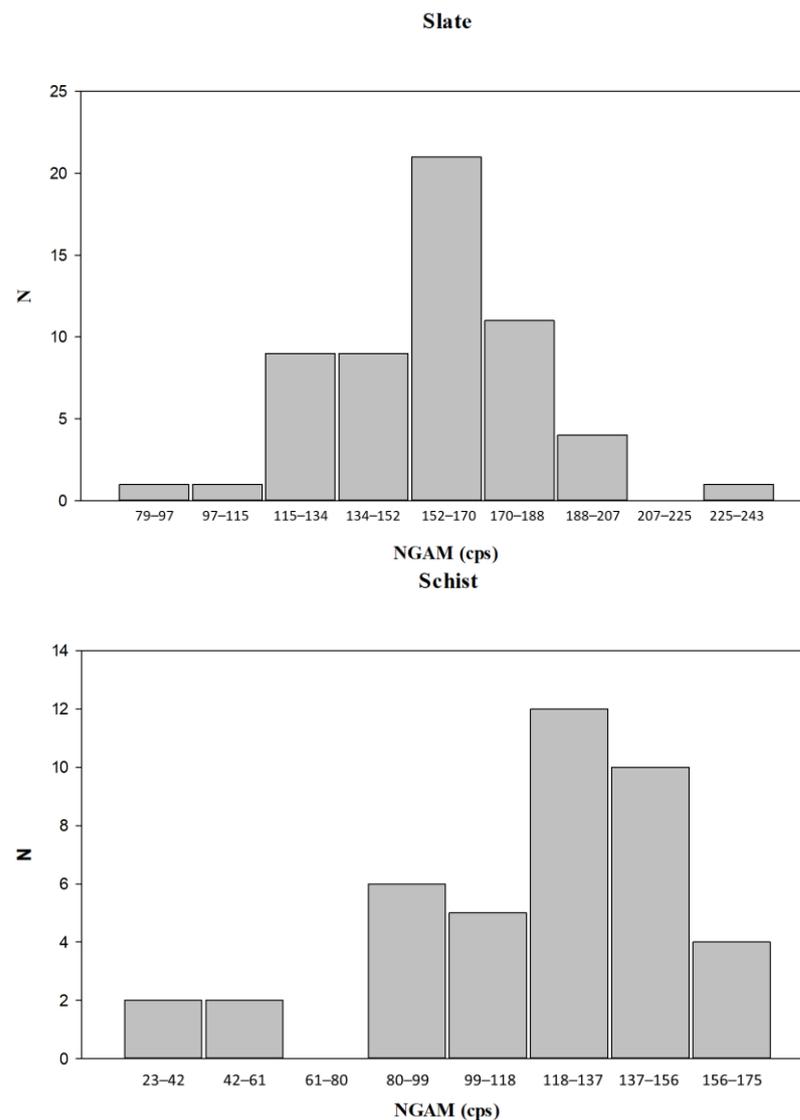
		F-Sandstone						
	Data Sets	All Data	[30–187]	[30–167]	[30–148]	[30–128]	[30–109]	[30–89]
K	r	0.180	0.180	0.213	0.217	0.254	0.377	0.554
	Sig.	0.089	0.094	0.049	0.050	0.030	0.006	0.002
	N	90	88	86	82	73	52	28

**Table 5.** Correlation variations with various filtered data sets for the lithological group of slate.

		F-Slate						
	Data Sets	All Data	[94–210]	[94–193]	[94–177]	[94–160]	[94–144]	[94–127]
K	r	−0.125	−0.089	−0.101	−0.161	−0.283	−0.321	−0.455
	Sig.	0.392	0.546	0.501	0.327	0.161	0.285	0.365
	N	49	48	47	39	26	13	6



**Figure 5.** Cont.



**Figure 5.** Histogram of NGAM for three lithologies (sandstone, slate, and schist, respectively).

**Table 6.** Correlation variations with various filtered data sets for the lithological group of schist.

		F-Schist			
Data Sets		All Data	[23–156]	[23–137]	[23–118]
K	r	−0.102	−0.102	−0.461	−0.643
	Sig.	0.526	0.550	0.015	0.01
	N	41	37	27	15

Table 5 shows the correlation variations with various filtered data sets for the slate group. Spearman’s correlation coefficients between F and K gradually increased by deleting samples with higher NGAM values. When the NGAM value of the data is between 94 and 127, Spearman’s coefficient is −0.455, which is the maximum value and belongs to the medium strength according to Cohen’s guideline [34]. Spearman’s correlation coefficient increased from −0.125 (all data samples) to −0.455 ([94,127] data samples). However, the maximum correlation coefficient value is not statistically significant (the *p*-value is greater than 0.05). The insignificant result of F vs. K is that the sample size may not be sufficient. The applicability of this clustering method to the slate group needs further confirmation

with more data. Finally, Table 6 shows the correlation variations with various filtered data sets for the schist group. Spearman's correlation coefficients between F and K gradually increased by deleting samples with higher NGAM values. When the NGAM value of the data is between 23 and 118, Spearman's coefficient is  $-0.643$ , which is the maximum value and belongs to the strong strength according to Cohen's guideline [34]. Spearman's correlation coefficient increased from  $-0.102$  (all data samples) to  $-0.643$  ([23,118] data samples), and the maximum correlation coefficient value is statistically significant (the  $p$ -value is less than 0.05). Therefore, in this case, NGAM equal to 118 is used as the threshold value for schist clustering. Values above this threshold indicate intervals containing mud, while values below suggest intervals with very low mud content or being clean.

#### 4.3.2. Outcomes from the Modified Archie's Law Method

To understand the mud content within the specific interval of a formation, this study establishes an alternative clustering approach different from directly using the NGAM signal to classify intervals into muddy/clean zones based on a threshold value. Instead, this study first constructed the apparent formation factor ( $F_a$ ) using formation resistivity ( $R_o$ ) and the inverse of formation fluid conductivity ( $R_w$ ). Then, the modified formation factor ( $F_c$ ) was computed employing Equations (5) and (6) in Section 3.3. The  $F_a$  and  $F_c$  values are divided to obtain a dimensionless parameter  $F_a/F_c$ , and data samples where the  $F_a/F_c$  value falls in the [0.9,1.0] interval as the clean segments [26]. Finally, conducting a correlation analysis between the corrected formation factor ( $F_c$ ) and hydraulic conductivity (K) within the clean zones allows this study to understand the benefits of the improved correlation between  $F_c$  and K resulting after being corrected by this clustering approach.

To obtain  $F_c$  values for each sample under a single lithologic classification using the techniques described in Section 3.3, a scatter plot with  $1/F_a$  and  $R_w$  values was created using 150 downhole signal data points for each sample section (1.5 m double-packer test interval). Furthermore, simple linear regression analysis was applied to determine the regression equation's intercept (representing  $F_c$ ) and slope. However, if the obtained intercept or slope from the data points is negative, it would contradict the theoretical expectations. Such samples from the analysis will be excluded from the subsequent correlation analysis between  $F_c$  and K. Based on the analysis as mentioned above criteria, each sample's ( $F_a$ ,  $F_c$ ) data was obtained for each individual lithological type. Simultaneously, the  $F_a/F_c$  ratio was calculated for each sample. The correlation between  $F_c$  and K was then analyzed for different ranges of the  $F_a/F_c$  ratio. This analysis aimed to investigate the relationship between the ratio and the correlation of  $F_c$  vs. K. Theoretically, as the  $F_a/F_c$  ratio increases, the sample's mud content decreases, aligning better with Archie's law's theoretical assumptions.

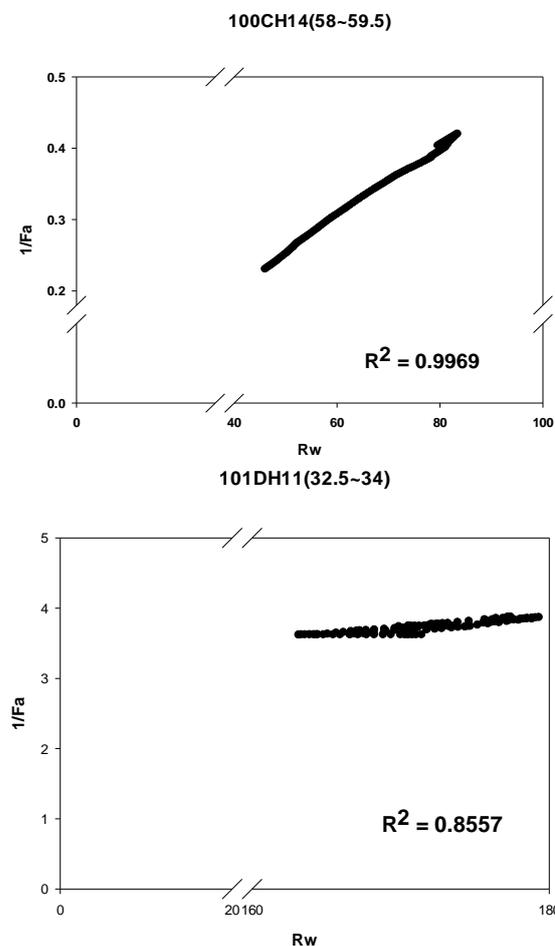
Table 7 shows the correlation analysis between modified formation factor ( $F_c$ ) and hydraulic conductivity (K) for different lithological types. According to the study by Worthington [26], the  $F_a/F_c$  value of the clean and mud-free formation interval should be greater than 0.9. However, the analysis results in the table show that very few samples of different lithological types meet the criterion of  $F_a/F_c$  greater than 0.9. Only a few sandstone samples can exceed this 0.9 threshold. Using this approach to separate samples from muddy and clean sections of the formation, it is clear that relatively few lithological samples in the Taiwan region meet the requirements of Archie's law well.

In addition, the smaller the  $F_a/F_c$  ratio, the higher the probability of containing mud. Table 7 also shows sample groups for different ranges of  $F_a/F_c$  ratios along with the correlation analysis results between  $F_c$  and K. Taking sandstone as an example, the correlation between  $F_c$  and K improves as the  $F_a/F_c$  ratio increases. Similar trends were observed for most other lithological types. However, upon comparing these trends with the results of the correlation coefficient trends for each lithological type, this clustering approach suggests that sedimentary rock types have a better chance of yielding mud-free samples. On the other hand, slates in metamorphic rocks are more challenging to screen for mud-free samples. This conclusion aligns with the findings in the analysis of Section 4.3.1.

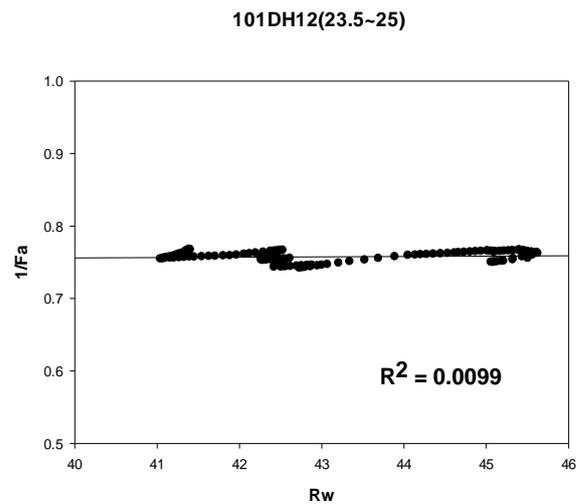
**Table 7.** Correlation analysis of corrected formation factor ( $F_c$ ) and hydraulic conductivity ( $K$ ) of different lithologies under different  $F_a/F_c$  ratio ranges.

Rock Types	Sandstone		Slate		Schist	
	$r$	No. of samples	$r$	No. of samples	$r$	No. of samples
0–1	−0.1	41	0.168	32	−0.085	16
0.2–1	0.003	21	−0.115	22	−0.297	10
0.4–1	0.245	12	−0.291	13	0.353	6
0.6–1	0.406	10	−0.066	8	0.936	3
0.8–1	−0.800	4		3	N.A.	1
0.9–1	−1.000	3	N.A.	2	N.A.	1

Finally, concerning the proposed method for calculating  $F_c$  in this study, the estimated quality of  $F_c$  data deserves discussion, as it determines the reliability of the correlation analysis results between  $F_c$  and  $K$ . Figure 6 displays scatter plots and regression curves for three different sample sets of  $1/F_a$  against  $R_w$ . The corresponding regression coefficients ( $R^2$ ) for the three sample sets are 0.9969, 0.8557, and 0.0099, respectively. The first sample set exhibits the highest  $R^2$  value and a concentrated point distribution, indicating a strong matching degree and concentrated point set. The estimated  $F_c$  value from this kind of well-matching and concentrated point distribution samples may belong to higher-quality data. Conversely, the point distribution in the last sample set is more scattered, suggesting lower-quality data for the estimated  $F_c$  value. Thus, the quality of  $F_c$  estimation has a specific impact on the quality of subsequent correlation analysis results between  $F_c$  and  $K$ . Therefore, there is room for improvement in the feasibility of this clustering method for determining mud-containing intervals.



**Figure 6.** Cont.



**Figure 6.** Demonstration of the quality of estimated  $F_c$  values for three types of levels.

#### 4.4. Establishment of Hydraulic Conductivity Estimation Models

Using the two clustering methods outlined in Section 4.3, a preliminary selection of potential mud-free samples conforming to Archie's law theory has been conducted based on the collected sample data. This serves as a foundation for further establishing estimation formulas for predicting hydraulic conductivity based on the formation factor. Regarding the outcomes of the natural gamma ray threshold clustering method, the analysis primarily focuses on results from three individual lithological types: sandstone, schist, and slate. Initially, an examination was performed to check for anomalies in short normal resistivity and fluid conductivity values within each set of individual lithological samples. These anomalies were verified against expected short normal resistivity and fluid conductivity values based on the hydraulic conductivity value. Theoretically, both short normal resistivity and fluid conductivity values should be small for samples with high permeability. Conversely, for low permeability samples, both values should be larger. When the raw data signals were rechecked for anomalies, these abnormal data samples were considered an outlier within that set. Finally, regression analysis between hydraulic conductivity and formation factors and the construction of hydraulic conductivity estimation models were performed exclusively for samples with signals conforming to the theoretical values.

During the process of model establishment, it was observed that each lithological type had outliers after data quality checking. Simultaneously, the  $R^2$  values of regression analyses between original data points and checked data points showed significant differences between the two sets of analysis results. The accuracy of hydraulic conductivity estimation models can be greatly enhanced by re-evaluating the rationality of data signals. Regression analysis results with the removal of outliers revealed  $R^2$  values of 0.63, 0.60, and 0.83 for sandstone, schist, and slate regression models, respectively. For these three lithological types, the hydraulic conductivity estimation models best matched the power law model. Equations (7)–(9) show the estimation equations for sandstone, schist, and slate, respectively. Through the established estimation models, the steps for estimating hydraulic conductivity are (1) selecting the appropriate lithological estimation model; (2) collecting short normal resistivity and fluid conductivity data from borehole electrical logging; (3) obtaining the formation factor ( $F$ ) using Archie's law theory; and (4) estimating hydraulic conductivity using the calculated  $F$  value and Equations (7)–(9).

$$K = 7 \times 10^{-8} F^{1.3033} \quad (7)$$

$$K = 6 \times 10^{-4} F^{-2.422} \quad (8)$$

$$K = 2 \times 10^{-6} F^{-3.055} \quad (9)$$

Although this study utilized the statistical method in Section 3.3 to rapidly screen for valid data samples, there were still some samples for which abnormal signals could not be entirely screened out. However, further scrutiny of well-logging signals allowed the selection of ultimately analyzable samples. Improvements can be made to the screening method in Section 3.3 in the future.

Regarding the outcomes of the modified Archie's law screening method, only the single lithological type of sandstone can reach the criterion of  $F_a/F_c \geq 0.9$  after clustering. This clustering method is relatively stringent and theoretically grounded for identifying mud-containing formation intervals. After undergoing this clustering process, the sample count was reduced from 41 to only 3 that met the clustering criterion. Finally, regression analysis between  $K$  and  $F_c$  and the establishment of hydraulic conductivity estimation models was performed for samples conforming to theoretical signal values. The regression analysis results for sandstone indicated that this lithological type's hydraulic conductivity estimation model exhibited the best match with the power law model, with an  $R^2$  value of 0.98. Equation (10) presents the estimation equation for sandstone.

$$K = 4 \times 10^{-6} F^{-7.591} \quad (10)$$

In summary, after establishing estimation models of hydraulic conductivity based on the data collected from 88 boreholes in Taiwan's mountainous areas, Equations (7)–(10) with electrical well-logging data of a given borehole can be used to easily generate hydraulic conductivity profiles of this borehole. With such data information, possible applications include the disclosure of hydrogeological complexity for engineering design and planning, exploring the potential of using groundwater extracted from fractured rock formations as alternative water resources against drought, giving information about a drilling depth for maximizing profits concerning the water supplies availability, finding potential slip surface locations at landslide-prone sites, and so on.

## 5. Conclusions

Given the need for information on the continuous hydraulic conductivity of rock mass vertically required for scientific questions or the development planning of rock engineering, this study performs a feasibility investigation for estimating hydraulic properties of rock formations in complex geologic environments using downhole electrical signals. Summarizing the various research findings of this study, the following conclusions can be drawn, along with potential research recommendations for future efforts.

1. For results concerning data processing and classification, statistical analysis showed a high degree of geological heterogeneity in the study site has been found. While developing hydraulic conductivity estimation models, well-logging signals were suggested to be categorized by lithological types to establish effective relationships with hydraulic conductivity.
2. For results regarding correlation analysis for various single well-logging signals with hydraulic conductivity, the three types of resistivity (LON, SHN, and SPR) and fluid conductivity (COND) signals with hydraulic conductivity for most of the lithological cases had better correlation performance than SP and NGAM signals. This better performance confirmed that the resistivity and fluid conductivity parameters were required to be composed of the formation factor ( $F$ ). Nevertheless, a single signal alone is insufficient for constructing a model to estimate hydraulic conductivity.
3. To improve electrical–hydraulic relationships in response to the effect of clay mineralogy, the natural gamma ray threshold clustering and modified Archie's law clustering methods successfully play an important role in filtering clayed data. However, to satisfy Archie's law's theoretical requirements, many data entries for various rock types needed to be removed, indicating that Taiwan's mountainous rock formations

are complex and often contain significant clay content. Therefore, careful consideration of clay-related issues in formation layers is essential in practical engineering applications in mountainous regions.

4. With the assistance of two mud clustering techniques, this study has successfully established four permeability estimation models for three rock types (sandstone, schist, and slate). The  $R^2$  values are at least 0.6. However, the issue of limited data during model development is worth noting.
5. During the exploration of electrical well-logging data, it was found that the clay effect is present in most rock formations in Taiwan. To enhance the utilization of a mathematical model for estimating hydrogeological parameters of individual rock types using single resistivity signals, more data collection is required to ensure the reliability of the model. Furthermore, for hydrogeological parameter estimation models applicable to multiple rock types, it is recommended to consider recombining the collected signals. This approach could yield novel signal indicators, enabling the construction of new relationships between indicators and different hydrogeological parameters.

**Author Contributions:** S.-M.H. developed the conceptualization, processed the data, and wrote the manuscript; G.-Y.L. worked on the correlation studies; M.-C.D. worked on data clustering; Y.-F.L. analyzed the well-logging data and the data curation; J.-S.L. worked on well-logging data preparation. All authors have read and agreed to the published version of the manuscript.

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