

Article

Using Process Mineralogy as a Tool to Investigate Blending Potential of the Pentlandite-Bearing Ores at the Nkomati Ni Mine in South Africa

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Abstract: The mineralogy and texture of Ni-sulfide ores at the Nkomati nickel mine are highly variable, and this results in often erratic nickel recovery at the mine. The variability of the ore presents an opportunity to study the influence of grind size on the flotation-based recovery of Ni in highly heterogeneous sulfide ores, which would be applicable to this ore type at many other mines worldwide. In view of this, a process mineralogy investigation was conducted on thirteen mineralogically and texturally different nickel-sulfide ores from the Nkomati Nickel Mine, with a view on the influence of grind size on the flotation performance of pentlandite. Ore types presented include medium- and high-grade variants of the bleb, disseminated, massive, semi-massive, and net-textured sulfide ores of the Main Mineralized Zone (MMZ), as well as disseminated chromite-rich nickel sulfide ore and massive chromitite ore of the Peridotitic Chromitite Mineralized Zone (PCMZ). Laboratory scale metallurgical test work, comprising of sequential grinding and bench-top flotation testing of the ores, was conducted in combination with quantitative mineralogical investigation of the flotation feed and associated flotation products, using a FEI 600F Mineral Liberation Analyzer. The ore types under consideration require a variety of grind sizes (i.e., milling times) in order to attain optimal recovery of nickel through flotation. This is predominantly controlled by ore texture, and also partly by the abundance of the major constituent minerals in the ore, being pyroxenes, base metal sulfides, and chromite. Liberation of pentlandite is directly correlated with grind size (milling time), which is also positively correlated with the level of nickel recovery through flotation. A grind size of P80 at 75 µm results in the highest concentrate nickel grades of 7.5-8.1% in the PCMZ ores' types which is the current grind for the PCMZ ores at Nkomati. A grind size of P77 at 75 µm yields the best overall pentlandite liberation, Ni recoveries of 84–88% and grades of 5.3–5.6% in the MMZ ores. This holds the potential to produce the best overall pentlandite liberation, nickel grades, recoveries from blending the MMZ and PCMZ ore types, and milling the composite ore at a target grind of P80 at 75 µm.

Keywords: ore texture; grind sizes; milling; liberation analysis; pentlandite; flotation; flotation kinetics; recovery

1. Introduction

Nickel is a ferromagnetic transition metal, markedly resistant to oxidation and corrosion. It is malleable, ductile, and has superior strength and corrosion resistance even at high temperatures and it provides an excellent base for developing specialized alloys, such as stainless steel. Nickel and nickel alloys are non-ferrous metals with high strength and toughness, excellent corrosion resistance, and superior elevated temperature properties.

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This makes nickel a highly versatile material that alloys with most metals for a wide variety of industries, such as aircraft gas turbines, steam turbines in power plants, and is used intensively in the energy and nuclear power industries [\[1\]](#page-22-0).

Economically important ore types hosting nickel are limonite (Fe-hydroxide) and garnierite (Ni-laterite) type ores, as well as the sulfide minerals, pentlandite ((Ni, Fe) $_9$ S₈), and pyrrhotite (ranging in composition from FeS to Fe₇S₈, and in which some of the iron may be replaced by nickel). Magmatic sulfide deposits such as Norilsk in Russia [\[2\]](#page-22-1), Sudbury in Canada [\[3,](#page-22-2)[4\]](#page-22-3), and Kambalda in Australia [\[5\]](#page-22-4)), as well as laterite deposits (e.g., those occurring in Cuba, New Caledonia, and Indonesia [\[6](#page-22-5)[,7\]](#page-22-6)), account for the bulk of nickel production world-wide. Magmatic sulfide deposits host about 40% of the global nickel resource, and currently are the source of more than 50% of the world's nickel supply, while laterite deposits are host to approximately 70% of the world's nickel resource [\[8\]](#page-22-7).

Pentlandite is generally found within the lower margins of mineralized layered intrusions, for example, in the troctolite of the Voisey's Bay intrusive complex in Canada, and in the gabbro of the Duluth Complex of North America and the Bushveld Igneous Complex in South Africa [\[3](#page-22-2)[,9](#page-22-8)[–11\]](#page-22-9). The nickel sulfide deposits (and minerals) often also contain cobalt, copper, and platinum-group metals. Increasing demand for nickel in the stainless-steel manufacturing industry and the continuous depletion of nickel resources, compounded by high processing costs, have resulted in substantial increases in the price of nickel, and this has precipitated much interest in the optimization of the nickel recovery processes [\[12\]](#page-23-0).

This paper focuses on pentlandite in ore from the Nkomati Nickel Mine, which is located in the Uitkomst Complex in South Africa [\[11](#page-22-9)[,13–](#page-23-1)[17\]](#page-23-2). Nkomati is the only primary nickel producing mine in South Africa, with pentlandite being the main nickel-bearing mineral. Two ore horizons are being mined for nickel, these being the Main Mineralized Zone (MMZ) as well as the Peridotitic Mineralized Zone (PCMZ), with each of these characterized by a variety of ore textures and mineralogy [\[11](#page-22-9)[,18](#page-23-3)[,19\]](#page-23-4). The ore types of the MMZ ores are comprised of: high- and medium-grade bleb (Bleb_HG and Bleb_MG); disseminated (Dis_HG and Dis_MG); massive (MS_HG and MS_MG); semi-massive (SMS_HG and SMS_MG); and net-textured (Net_HG and Net_MG) varieties. In contrast, the ore types of the PCMZ consist of high- and medium-grade variants of disseminated chromite-rich nickel sulfide ores (PCMZ_HG and PCMZ_MG), as well as massive chromitite ore (MCHR). Accepted practice at Nkomati is to mill the MMZ sulfide ores at a grind of 67% passing 75 micron (i.e., P67 at 75 µm) and P80 at 75 µm (PCMZ ore horizon), followed by a separate bulk sulfide flotation of the two ore types.

The liberation of sulfides through milling, and their efficient recovery through bulk sulfide flotation concentration, are closely related to the ore mineralogy and ore texture, which often pose processing problems for complex ore types [\[20\]](#page-23-5). Textural analysis of the ore minerals provides predictive liberation information and also acts as a basis for an economic evaluation of a technological scheme for mineral processing [\[21](#page-23-6)[,22\]](#page-23-7). Therefore, the optimum liberation and recovery of valuable minerals in texturally complex ores require varying degrees of grinding to optimize mineral liberation and energy consumption of the mining operation. This is achieved by having the ore milled not finer than the optimum liberation required; and to ensure that the liberated minerals are not ground finer than absolutely necessary, as that overgrinding will further inhibit their recovery during flotation [\[10](#page-22-10)[,23\]](#page-23-8).

The processing philosophy at the Nkomati mine is to blend the different sulfide ore textural varieties from each ore horizon into a 'required' run-of-mine mill feed, which is then processed further to ultimately obtain a bulk flotation concentrate [\[24\]](#page-23-9). However, ore blending could lead to synergistic and antagonistic effects from the individual ore types, of varying mineralogy and texture, during mineral processing, while the overall contribution of a specific ore type to overall processing efficiency may be masked [\[20,](#page-23-5)[25](#page-23-10)[–27\]](#page-23-11).

The influence of ore mineralogy and texture on the recovery of Ni from the MMZ ore horizon at Nkomati (milled at a grind size of P67 at 75 µm) was studied before (but excluded the effect of varying grind size) [\[20\]](#page-23-5), while the PCMZ remained unstudied. Hence, the aim of the present study is to assess the impact of variable grind size on flotation performance [\[25](#page-23-10)[,26](#page-23-12)[,28](#page-23-13)[–34\]](#page-23-14) for the MMZ and the PCMZ ore horizons. This objective is achieved by conducting laboratory-scale sequential grinding, bench-top flotation, and quantitative mineralogical investigation of the flotation feed and flotation products [\[28](#page-23-13)[,33](#page-23-15)[,34\]](#page-23-14). Although commonly conducted in-house by the various mining companies, published case studies are comparatively rare, and hence the results of the present study should also be of use to other mines world-wide where nickel is recovered from sulfide ores of varying ore mineralogy and texture.

2. Technical Background

The geology of the Uitkomst Complex and mineralization at Nkomati Nickel Mine have been well documented by [\[11,](#page-22-9)[13](#page-23-1)[–19\]](#page-23-4). This study focuses primarily on the MMZ and the PCMZ orebodies that, at the time of undertaking this study, were being exploited at the Nkomati mine (the mine is currently under care and maintenance). These two orebodies are characterized by varying sulfide textures, which include disseminated, net-textured, and massive varieties. There are also varying degrees of alteration and oxidation in certain areas of the orebodies, with the development of a variety of secondary silicate and oxide minerals [\[11](#page-22-9)[,13](#page-23-1)[,14,](#page-23-16)[16,](#page-23-17)[17\]](#page-23-2). The mine feed cut-off grade is 0.3% Ni for the MMZ ores and the target grind employed at the mine is 67 wt% passing 75 μ m, while the mine cut-off grade of the PCMZ ores is 0.25% Ni with a target grind of 80 wt% passing 75 µm. Metal recovery is accomplished through froth flotation [\[18,](#page-23-3)[19\]](#page-23-4).

3. Sampling and Methodology

3.1. Sampling

Thirteen representative samples were collected from ore stockpiles at the Nkomati mine for petrographic study, the acquisition of quantitative mineralogical data using an automated SEM-based platform, as well as laboratory-scale metallurgical test work which included milling and flotation. The samples were hand-sorted according to sulfide texture types. Following the approach documented by [\[19\]](#page-23-4), ten samples, about 12 kg each, were collected from the MMZ ore stockpiles (high- and medium-grade ore stockpiles) and three samples were collected from the PCMZ ore stockpiles, respectively. The ten samples from the MMZ comprised high- and medium-grade variants of the bleb (denoted by Bleb_HG for the high-grade variant and Bleb_MG for the medium-grade variant), disseminated (Dis_HG and Dis_MG), massive (MS_HG and MS_MG), semi-massive (SMS_HG and SMS_MG), and net-textured (Net_HG and Net_MG) sulfide ores. The three samples from the PCMZ ore stockpiles consisted of high- and medium-grade variants of disseminated chromite-rich sulfide ore (denoted by PCMZ_HG for the high-grade variant and PCMZ_MG for the medium-grade variant), and a massive chromitite ore (MCHR).

Each sample was crushed to -2 mm and split using a rotary sample splitter into 6×1 kg sample aliquots for milling and flotation, while 75–100 g were submitted for assay, and 3 g aliquots were used to prepare 30 mm resin mounts for mineral liberation analysis (MLA). Three MLA block mounts were prepared for each ore type, per three grind sizes, and were analyzed at the University of Johannesburg. Geochemical analysis was conducted at the Genalysis laboratories in Australia.

3.2. Petrography

Polished thin sections of ore samples from the MMZ and the PCMZ were subjected to petrographic analysis on an Olympus BX51 Optical Microscope, to determine the mineralogy and textural characteristics of the different ore types [\[35](#page-23-18)[–38\]](#page-23-19).

3.3. Automated Mineralogy

Representative splits of each coarsely crushed (−2 mm) ore type sample (also referred to as unprocessed ore) were mixed with resin and then cast into 30 mm resin molds to set. The 30 mm blocks were polished, coated with carbon, and examined with an FEI 600F MLA

for mineral modal mineralogy, using the GXMAP procedure [\[39](#page-23-20)[,40\]](#page-23-21). All analyses were completed at $350\times$ magnification. The samples were also examined for pentlandite grain sizes' distribution, using the SPL_GXMAP procedure.

All of the milled ore feeds, collected from the swirling pulp in the flotation cell prior to flotation, were sieved to −75 + 38 µm in order to exclude any fine materials that may report to the concentrate through entrainment and entrapment, rather than true flotation [\[41,](#page-23-22)[42\]](#page-24-0). The $-75 + 38$ µm fraction most likely contains material that reports to the concentrate by true flotation, while the coarser particles (e.g., $>75 \mu m$) and the finer materials (e.g., $<$ 38 μ m) float poorly [\[43,](#page-24-1)[44\]](#page-24-2). Although optimization of the flotation kinetics may still result in the efficient recovery of both fine and coarse particles [\[45](#page-24-3)[,46\]](#page-24-4), this is not the primary focus of the present contribution. Each of the fractions was split into representative aliquots using a rotary micro riffler, mixed with resin and cast into 30 mm blocks, polished and coated with carbon. These were then examined for pentlandite liberation using SPL_GXMAP.

3.4. Milling

The samples collected for study were subjected to mill tests in order to determine their milling behavior with respect to the rate at which the ore is reduced in size with progressive milling time. This was accomplished using ore which was crushed to −2 mm. A 210 mm diameter steel rod mill, charged with a 1 kg sample aliquot, was utilized, in conjunction with 6 \times 25 mm, 8 \times 20 mm and 6 \times 16 mm mill rods [\[47\]](#page-24-5). Prior to milling, 1 kg of crushed quartz [\[44\]](#page-24-2) was milled in 500 mL water for 15 min, in order to clean the mill. Following disposal of the quartz and rinsing, a 1 kg sample aliquot was then placed in the mill, with 500 mL of water added, in order to produce a slurry comprising of 66% solids by weight. The rotation of the rod mill was set at 61 rpm.

Milling was conducted for 10 min and the grind was determined (as weight % passing $75 \mu m$) by wet sieving and weighing of the milled product after drying in an oven at low temperature (110 °C). The samples were then returned to the mill for a further 15 and 25 min of milling (that is, a total milling time of 50 min), and the size analysis was conducted again for each of these additional milling intervals.

Using the milling rate data thus produced, further milling was conducted on new 1 kg aliquots of each ore type (crushed to -2 mm) for grind sizes of P57, P67, and P77 at 75 μ m (MMZ) as well as grind sizes of P70, P80, and P90 at $75 \mu m$ (PCMZ).

3.5. Flotation

Laboratory scale flotation testing was conducted using a 2.5 L flotation cell mounted on a Denver laboratory flotation test machine. The milled slurry was made up to 35% solids by adding a further 1.36 L of water. The impeller speed was set at 1100 rpm and the air flow rate was maintained at 7 L/min in all of the tests. A froth depth of 2 cm was maintained, and a scraping depth of 0.5 cm above the slurry level was utilized for the froth collection. Before starting flotation, 65 mL (or about 60 g dry weight) of the swirling pulp in the flotation cell was collected for chemical analysis ('assay') of the flotation feed. Details of the reagents used, additional sequence and conditioning times are as per [\[19\]](#page-23-4). The reagents added included primary collector sodium isobutyl xanthate (SIBX), secondary collector Senkol 700, frother Senfroth 200, and depressant Sendep 300. All of the reagents used were supplied by Senmin Chemicals Pty LTD (now known as AECI Mining).

Dosages of 10, 100, 20, and 350 g/t of Senkol 700, SIBX, Senfroth, and Sendep were used, respectively. A volume of 0.01 mL Senkol 700 was added to the mill charge prior to milling, after which the mill charge was then milled to the target grind.

A 10 mL volume of the SIBX was added to the flotation cell while running at 1100 rpm and conditioned for 1 min, followed by 2 mL of Senfroth 200 and a further 2 min of conditioning. A volume of 17.5 mL Sendep 300 was finally added, followed by a further 2 min of conditioning time.

Air flow into the flotation cell was initiated, and concentrates were collected by scraping the froth every 15 s for 1, 3, 10 L and 30 min of cumulative flotation times for each

of the four timed concentrates, respectively. Each feed, concentrate, and tailing sample was dried in an oven at 110 °C, and cooled in air. Concentrate volumes ('mass pulls'; i.e., the flow rate of solids reporting to the concentrate) were determined through weighing. Flotation tests were executed in duplicate for each ore type; with the feed, concentrate, and flotation tailings combined per sample.

The concentrations of Ni and other elements in the feed and tailings were analyzed at the Genalysis Laboratory in Australia [\[48\]](#page-24-6). The detection limit of Ni is in the order of 1 ppm (optical emission spectrometry). The recovery of Ni is based on the mass of Ni in the feed, concentrate, and flotation tailings. Concentrate grade is based on the mass of Ni in the concentrate and is expressed as a function of Ni recovered from the flotation feed.

the concentrate and is expressed as a function of Ni recovered from the flotation feed.

4. Ore Sample Characterization

4.1. Macroscopic Description

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Five sulfide ore textures namely, the bleb, disseminated, massive, semi-massive, and net-textures are represented in the ore samples selected from the MMZ ore hori-zon (Figure [1A](#page-4-0)–E; Table [1\)](#page-5-0). Two ore textural types comprise the samples from the PCMZ ore horizon, being disseminated chromite-rich sulfide ores, as well as a massive chromite ore (Figure [1F](#page-4-0),G; Table [1\)](#page-5-0).

Figure 1. Macroscopic images of the distribution of sulfides (i.e., rock textures) of hand-sized polished rock slabs of ore samples collected from the MMZ (A-E), as well as the PCMZ (F,G) ore horizons. Scale bar bottom right $= 1$ cm.

Table 1. Macroscopic textures of ore types from the MMZ AND PCMZ ore horizons. **Table 1.** Macroscopic textures of ore types from the MMZ AND PCMZ ore horizons.

Table 1. *Cont*.

4.2. Microscopic Description

Petrographic features of the ore types are as per Figures [2–](#page-7-0)[6,](#page-11-0) and Tables [2](#page-6-0) and [3.](#page-11-1)

Table 2. Microscopic (petrographic) descriptions of thin section of the MMZ ores.

chalcopyrite, pentlandite, pyrrhotite, and pyrite and some of the sulfides have been replaced by Fe-oxides along grain boundaries (Figure [6F](#page-11-0)). Finer-grained sulfides are disseminated throughout the silicate matrix.

Table 2. *Cont*.

Figure 2. Photomicrographs of the medium-grade and high-grade bleb textured sulfide ores transmitted plane polarized and mineral abbreviations are provided light of mineral abbreviations are as follows: ((**A–D**) transmitted plane polarized light; (**E**,**F**) reflected light). The mineral abbreviations are as follows: amphibole (Amp); chlorite (Chl); clinopyroxene (Cpx); chromite (Chr); glaucophane (Gln); hornblende (Hbl); orthopyroxene (Opx); oxide (Ox); plagioclase (Pl); chalcopyrite (Ccp); pentlandite (Pn); pyrrhotite (Po); pyrite (Py); serpentine (Srp); and talc (Tlc). The scale bar at the bottom right of the images represents $500 \mu m$. BMS = base metal sulfides.

Figure 3. Photomicrographs of the high-grade and medium-grade disseminated sulfide ores showing various silicate (A,D,E) and sulfide (B,C,F) minerals. The scale bar at the bottom right corner of the images represents 500 μ m. Refer to Fi[gu](#page-7-0)re 2 for explanation of the mineral abbreviations.

Figure 4. Photomicrographs of the high-grade massive sulfide ores (A-C) as well as the mediumgrade massive sulfide ores $(D-F)$ show various silicates and composite sulfides. The scale bar at the bottom right corner of the images represents 500 μ m. Refer to Figure [2](#page-7-0) for explanation of the abbreviations. mineral abbreviations.

Figure 5. Photomicrographs of the high-grade semi-massive (A-C) and medium-grade semi-massive (D-F) sulfide ores show various silicates and sulfides. The scale bar at the bottom right corner of the images represents 500 μ m. Refer to [F](#page-7-0)igure 2 for explanation of the mineral abbreviations.

Figure 6. Photomicrographs of the high-grade net-texture ore (A–C) and medium-grade net-texture ore (**D**–**F**) showing various silicate and sulfide minerals. The scale bar at the bottom right corner of ore (**D–F**) showing various silicate and sulfide minerals. The scale bar at the bottom right corner of the images represents 500 μ m. Refer to Figure [2](#page-7-0) for explanation of the mineral abbreviations.

Figure 7. Photomicrographs of disseminated chromite-rich sulfide ore from the Peridotitic Chromitite Mineralized Zone showing various silicates (A,B,D,E) , sulfides, and chromite (C,F,G) . The scale bar at the bottom right corner of the images represents 500 µm. Refer to Figure [2](#page-7-0) for explanation of the mineral abbreviations.

Figure 8. Photomicrographs of massive chromite ore from the Peridotitic Chromitite Mineralized **Figure 8.** Photomicrographs of massive chromite ore from the Peridotitic Chromitite Mineralized Zone showing various silicate minerals and chromite. (**A**) Chlorite and serpentine forming networks Zone showing various silicate minerals and chromite. (**A**) Chlorite and serpentine forming networks arcounter grains of the chromite grains of the chromite. (*A*) chrome and serpendic forming networks around chromite grains; (**B**) Olivine, serpentine, and chlorite forming networks around chromite grains. The scale bar at the bottom right corner of the image represents 500 μ m. Refer to Figure [2](#page-7-0) for explanation of the mineral abbreviations.

The modal mineralogy of the various MMZ and PCMZ ore types are as per Table 4. *4.3. Quantitative Mineralogy*

The modal mineralogy of the various MMZ and PCMZ o[re](#page-13-1) types are as per Table 4. The MS_MG ore variant contains lower amounts of altered silicates than the MS_HG ore variant. Clinopyroxene (12–46%) and orthopyroxene (up to 30%) are the dominant silicate minerals in all of the samples from the MMZ and PCMZ (Table 4). Pyrrhotite $(4-63%)$ is the most abundant base metal sulfide, with minor quantities of pyrite (up to 10%), pentlandite (up to 7%), and chalcopyrite (up to 1.7%) in the ores from the MMZ. The ore samples from the PCMZ have the most abundant chromite (9–63%) and the least sulfides (Table [4\)](#page-13-1).

Table 4. Mineral modal abundances of samples of the MMZ and PCMZ ore horizons (area % for ore **Mineral BlebMG BlebHG DisMG DisHG MSMG MSHG SMSMG SMSHG NetMG NetHG PCMZMG PCMZHG MCHR** crushed to -2 mm).

4.4. Sample Assay

Nickel contents in the samples of the massive sulfide ore type vary from 3% to 3.5%, in the semi-massive sulfide ore type vary from 1.8% to 1.9%, and up to 1.7% in the high-grade net-textured sulfide ore type and the high-grade disseminated sulfide ore type (Table [5\)](#page-14-0). The Bleb_MG/HG, Dis_MG/HG, NET-MG, and PCMZ_MG/HG are characterized by elevated magnesium contents on the order of 10–16% MgO; whilst the Dis_MG and NET_MG/HG

ores have the highest Ca content, which ranges from 4% to 8% CaO. The MS_MG/HG and PCMZ_MG/HG ores have the lowest Ca content, ranging up to 3% CaO. ϵ highest Ca content, which ranges from 4% to $\delta\%$ CaO. The MS_MG/HG and

Nickel contents in the samples of the massive sulfide ore type vary from 3 to 3.5%, in

4.5. Size Distribution of Pentlandite

The MS_HG and SMS_HG sulfide ore variants are characterized by the coarsest pentlandite, while the MCHR ore types have the smallest pentlandite (Figure [9\)](#page-14-1). The pendandite, while the METHC six types have the smallest pendantale (1 gare 3). The remaining ore types have intermediate pentlandite grain size distributions, of relatively narrow range. le types have intermediate pentlandite grant size distributions, or relatively. \mathbf{e} .

Figure 9. Pentlandite grain size distributions (equivalent circle diameter) for the samples of the ious ore types collected from the MMZ and the PCMZ (crushed to −2 mm). various ore types collected from the MMZ and the PCMZ (crushed to −2 mm).

5. Sample Milling and Flotation

5.1. Milling Tests

The samples collected of the various ore types from the MMZ and the PCMZ differ substantially in their milling behavior (Figure [10\)](#page-15-0), in that a wide range of milling times are required in order to reduce the various samples to e.g., a P67 of 75 micron (Figure [10\)](#page-15-0). The high-grade ore varieties of the MMZ (with the exception of the MS_HG ore variety) as well as the PCMZ generally requires longer milling times than the medium-grade varieties.

Figure 10. Cumulative mass % passing 75 µm sieve as a function of milling time for samples of the **Figure 10.** Cumulative mass % passing 75 µm sieve as a function of milling time for samples of the different ore textures collected from the MMZ and the PCMZ. different ore textures collected from the MMZ and the PCMZ.

The Ble H G and Discrete ore textural variants or textural variants of the MMZ requires the long-The Bleb_HG and Dis_HG sulfide ore textural variants of the MMZ requires the longest milling times for e.g., a P67 of 75 micron, while the massive sulfide ore variants require the shortest milling time (Figure [10\)](#page-15-0).

 \overrightarrow{P} are type of the \overrightarrow{PC} The MCHR ore type of the PCMR ore horizon mills the fastest of all of the ore types the million tests, as per F_0 , is broad as α is broadly similar (with the MCHR sample, α investigated (Figure [10\)](#page-15-0).

The liberation of pentlandite in the $-75 + 38$ micron sieve fraction of the mill product from the milling tests, as per Figure [11,](#page-15-1) is broadly similar (with the exception of the MCHR sample, which shows very poor liberation of pentlandite compared to all of the other samples investigated). The MG and HG samples of the PCMZ ore horizon are characterized by a somewhat lower level of pentlandite liberation, relative to the samples of the MMZ (Figure [11\)](#page-15-1).

For 11. **Cumulative 11. Cumulative light of the sulful of the sulful of the sulful of the stress from the** $\frac{1}{2}$ the different grind sizes for high- and medium-grade variants of the sulfide ores from the MMZ and the different grind sizes for high- and medium-grade variants of the sulfide ores from the MMZ and **Figure 11.** Cumulative liberation yield of pentlandite (weight %) in the −75 + 38 fractions of feed in the PCMZ.

5.2. Flotation Tests

The flotation efficiency of the various ore types investigated in the present study, for grinds of P57, P67, and P77 at 75 µm (MMZ ore horizon), as well as P70, P80, and P90 at 75 micron (PCMZ ore horizon), is measured using cumulative recovery as a function of total flotation time (Figure [12\)](#page-17-0), as well as concentrate grade as a function of cumulative Ni *Minerals* **2022**, *12*, 649 18 of 26 recovery (Figure [13\)](#page-19-0).

Figure 12. *Cont*.

Figure 12. Cumulative Ni recovery as a function of flotation time for the flotation of the various ore **Figure 12.** Cumulative Ni recovery as a function of flotation time for the flotation of the various ore types at the Nkomati Ni mine, milled to a grind of P57, P67, and P77 at 75 micron ((**A**–**J**) MMZ ore types at the Nkomati Ni mine, milled to a grind of P57, P67, and P77 at 75 micron ((**A–J**) MMZ ore horizon)) as well as a grind of P70, P80, and P90 of 75 micron ((**K**–**M**) PCMZ ore horizon).

The results are highly variable. Generally, the finer grind sizes result in a higher abundance of floatable Ni-containing (pentlandite) particles, as shown by the higher cumulative Ni recoveries for P77 at 75 µm (MMZ) and P90 at 75 µm (PCMZ) (Figures [12](#page-17-0) and [13\)](#page-19-0).

A grind size of $P77$ at $75 \mu m$ results in the highest overall cumulative nickel recoveries for all of the sulfide ore textures from the MMZ, with the exception of the Bleb_MG sulfide ore variant, as well as the SMS_MG sulfide ore variant, which are characterized by the best Ni recoveries at a grind of P67 at 75 µm (Figures [12A](#page-17-0),G and [13A](#page-19-0),G).

A grind size of P90 at P75 µm, for samples from the PCMZ ore horizon, yields the best nickel recoveries in the PCMZ_MG and PCMZ_HG sulfide ores from the PCMZ (Figures [12K](#page-17-0),L and [13K](#page-19-0),L). In contrast, a grind size of P70 at 75 μ m results in the best nickel recovery for the MCHR ore type of the PCMZ ore horizon (Figures [12M](#page-17-0) and [13M](#page-19-0)).

Figure 12. *Cont*.

Figure 13. Cumulative concentrate grade vs. cumulative Ni recovery for the flotation of the various **Figure 13.** Cumulative concentrate grade vs. cumulative Ni recovery for the flotation of the various ore types at the Nkomati Ni mine, milled to a grind of P57, P67, and P77 at 75 micron ((**A**–**J**) MMZ ore types at the Nkomati Ni mine, milled to a grind of P57, P67, and P77 at 75 micron ((**A**–**J**) MMZ ore horizon) as well as a grind of P70, P80, and P90 at 75 micron ((**K**–**M**) PCMZ ore horizon). ore horizon) as well as a grind of P70, P80, and P90 at 75 micron ((**K**–**M**) PCMZ ore horizon).

6. Discussion 6. Discussion

The milling behavior of the Bleb_HG and Dis_HG ore variants from the MMZ corre-The milling behavior of the Bleb_HG and Dis_HG ore variants from the MMZ correlates positively with the increasing modal abundances of pyroxene (particularly orthopyroxene at 24–31%), and correlates negatively with the increasing modal abundances of sulfides, especially pyrrhotite (Table [4;](#page-13-1) Figure [10\)](#page-15-0). This trend is also observed in the chromite-rich sulfide ores of the PCMZ ore horizon, in which the PCMZ_HG ore type (36% orthopyroxene) requires the longest milling times (31–40 min) and the MCHR ore (0.5% orthopyroxene, but with 63% chromite) requires the shortest milling times (15–30 min) to achieve the required grinds (Figure [10\)](#page-15-0), which by inference also means that the abundance of chromite has a major effect on milling times (i.e., ores mill faster with abundant chromite).

However, the modal abundances and hardness of (ortho)pyroxene alone cannot adequately explain the longer milling times required. For example, the net-textured sulfide ores with higher orthopyroxene content (22–29% orthopyroxene) require less milling time (15–23 min) than the Bleb_MG and Dis_MG sulfide ores (15–27 min). The difference in milling times can, therefore, also be attributed to the differences in ore texture and level of mineral alteration [\[21](#page-23-6)[,24](#page-23-9)[,49–](#page-24-7)[51\]](#page-24-8).

The Bleb_MG/HG, Dis_MG/HG, Net-MG, and PCMZ_MG/HG are characterized by high magnesium content, while the Dis_MG and Net_MG/HG ores have the highest Ca content, and the MS_MG/HG and PCMZ_MG/HG ores have the lowest. This is a function of the modal mineralogy, and correlates with the abundance of Ca-and Mg-bearing silicate minerals in these ores (Table [1\)](#page-5-0). The mineralogy and the associated high Ca- and Mgcontents tend to have some downstream effects on the smelting of the concentrates when these minerals report to concentrate [\[23,](#page-23-8)[24](#page-23-9)[,52](#page-24-9)[,53\]](#page-24-10). In such instances, the amine functional group-based depressants could be used to depress excessive fine-milled MgO-containing gangue minerals, as well as liberated pyrrhotite [\[54\]](#page-24-11).

The mass pulls during flotation progressively increased with milling, and this can be attributed to the generally observed, increasing cumulative liberation yields of sulfides, including pentlandite, as milling progressed in all of the ores from the MMZ and PCMZ (Figure [12\)](#page-17-0), as also observed previously for Nkomati, and elsewhere [\[20](#page-23-5)[,33](#page-23-15)[,55](#page-24-12)[,56\]](#page-24-13). The mass pulls are highest in the samples with the most abundant sulfides (MS and SMS; and Net_MG and Net_HG sulfide ores; and PCMZ_MG and PCMZ_HG ores) due to the higher floatability tendency of sulfides when compared to silicate and oxide (chromite) minerals (Figure [12;](#page-17-0) Table [4\)](#page-13-1). Orthopyroxene, though known to be readily floatable, appears to contribute little to the observed mass pulls in this case [\[57\]](#page-24-14).

The grind of P77 at 75 µm produced the most superior nickel recoveries in all of the sulfide ore types from the MMZ, which is likely a result of the increased pentlandite liberation in this grind size [\[28,](#page-23-13)[33](#page-23-15)[,37](#page-23-23)[,55](#page-24-12)[,56](#page-24-13)[,58\]](#page-24-15). However, the Bleb_MG sulfide ore and the SMS_MG sulfide ore are an exception, and which resulted in the highest Ni recovery in the P67 at 75 μ m grind. This could be due to poor pentlandite recovery in the P77 at 75 μ m grind size in these specific ore variants [\[23,](#page-23-8)[32,](#page-23-24)[44,](#page-24-2)[52,](#page-24-9)[53\]](#page-24-10).

A grind of P90 at 75 µm also yielded the best nickel recovery values in the PCMZ_MG and PCMZ_HG ore variants from the PCMZ, except in the MCHR ore, in which the P70 at $75 \mu m$ grind produced the best nickel recovery value. The overall implication of these outcomes is that the P77 at 75 μ m grind size would be the optimum grind size for milling all of the sulfide ore types mined from the MMZ, to yield the best liberation of pentlandite and the best overall nickel recoveries. The P90 at $75 \mu m$ and P70 at $75 \mu m$ grinds would be ideal to produce the best nickel recoveries from the PCMZ_MG and PCMZ_HG ores, and the MCHR ores, respectively. However, for all practical purposes, due to the inadequacy of a single ore type to meet the daily run of mine ore requirements, a grind of P80 at $75 \mu m$ would be ideal for processing all of the ores as a composite [\[27\]](#page-23-11).

The highest nickel grades produced by the P77 at 75 µm grind in the Bleb_MG, Dis_MG, SMS_MG, Net_MG, and Net_HG sulfide ores; and by the P67 at 75 µm grind in the Bleb_HG, the Dis_MG, and the Dis_HG sulfide ores, as well as the MS_MG sulfide ore (Figure [13\)](#page-19-0) are consistent with the lower mass pulls produced in these grinds. The P80 at 75 µm grind also produced the highest nickel grades in the PCMZ_MG sulfide ore and the MCHR ore, and this is also in agreement with the lower mass pulls achieved by this grind in these ores.

7. Conclusions

The following conclusions are drawn from this study:

(1) The modal abundances of orthopyroxene and sulfides; and the orthopyroxene and chromite in the ores of the MMZ and the PCMZ, respectively, and ore texture, have a direct influence on the milling time requirements and the amount of energy required to produce the required grinds passing 75 µm. Longer milling times are required for

the ores with higher abundances of orthopyroxene and fewer sulfides for the ores from the MMZ, while longer milling times are also required for the ores of the PCMZ with higher abundances of orthopyroxene and less chromite. Ore blending prior to milling could limit the amount of orthopyroxene and increase the sulfides' abundance, thereby reducing the milling times, and ultimately the energy consumption of the milling circuits;

- (2) The positive correlation of high mass pulls with high sulfides' abundances indicate that such elevated abundances are necessary for the flotation-based recovery of Ni. Orthopyroxene, though known to be readily floatable, appears to contribute little to the observed mass pulls;
- (3) The P77 at 75 µm grind produces the best nickel recovery in the ores from the MMZ, while the P90 at 75 μ m, and the P70 at 75 μ m grinds yields the best nickel recoveries in the PCMZ_MG and PCMZ_HG sulfide ores from the PCMZ, respectively. These higher Ni recoveries in the finest grinds, are consistent with increased cumulative mass pulls and cumulative liberation yields of pentlandite with progressive milling. It should, though, be considered that the application of the P77 and P90 at 75 μ m grinding levels may impact negatively on the energy consumption of the milling circuits. However, for all practical purposes, due to the inadequacy of a single ore type to meet the daily run of mine ore requirements, grinds of P77 at 75 µm and P80 at 75 µm would be ideal for processing ores as a composite from the MMZ and the PCMZ, respectively;
- (4) The P77 at 75 µm grind produced the highest nickel grades in the Bleb_MG, Dis_MG, SMS_MG, Net_MG, and Net_HG ore variants of the MMZ, while the P67 at 75 μ m grind produced the highest nickel grades in the Bleb_Hg, Dis_MG, Dis_HG, and MS_MG ores of the MMZ, and the P80 at 75 µm grind produced the highest nickel grades in the PCMZ_MG and the MCHR ores of the PCMZ. This is in agreement with the lower mass pulls achieved by these grinds in these ores. Therefore, a grind of P77 at 75 μ m, as well as a grind of P80 at 75 μ m, would be expected to yield the best overall Ni recoveries and grades in the sulfide ores from the MMZ and the PCMZ, respectively.

8. Recommendations

The following recommendations are worth considering:

- 1. The sulfide ores from the MMZ could be milled at a grind of P77 at 75 µm to produce optimal yields of cumulative liberated pentlandite, and to yield the best overall Ni recovery and grades of up to 88% and 12%, respectively (Figures [12](#page-17-0) and [13\)](#page-19-0), instead of the grind of P67 at $75 \mu m$ currently in use at the Nkomati mine;
- 2. The PCMZ ores which achieved overall recovery and grade values of up to 79% and 8%, respectively, at a grind of P80 at 75 µm, and the MMZ ores which yielded best Ni and grade values of up to 88% and 12% at a grind of P77 at 75 µm, could potentially be blended and milled together at a grind of P80 at 75 µm to achieve optimum recoveries and grades in a single circuit;
- 3. A combination of flotation to recover sulfides within floatable particle sizes and gravity separation to recover liberated sulfides which are beyond floatable sizes and have reported flotation tailings especially for the MS_MG and MS_HG, as well as the SMS_MG and SMS_HG ore variants at the current grind size of P67 at 75 µm grind could be used. This could be followed by regrinding and flotation of the gravity sulfide concentrates to increase overall Ni recoveries, especially in the MS_MG and MS_HG ore variants, as well as the SMS_MG and SMS_HG ore variants;
- 4. More efficient and effective flotation circuits to recover the fine sulfide mineral particles from a single finer target grind size of P77 at 75 µm could also be designed and employed, or flotation reagents' optimization could be employed to recover any fine pentlandite particles that could potentially be lost to tailings;

5. Staged grinding to produce optimal floatable particle sizes and reduce excessive fine sulfide particles, followed by flotation, would likely improve the recovery of the valuable minerals. Staged grinding would also reduce the excessive production of the undesirable Ca- and Mg-rich minerals that are detrimental to downstream processing (resulting in high MgO and CaO contents in flotation products), especially for the Bleb_MG/HG, Dis_MG/HG, Net-MG, and PCMZ_MG/HG with elevated magnesium contents, and the Dis_MG and Net_MG/HG ore with elevated Ca contents. This would strike a balance between size reduction and optimal recoverability of the valuable minerals. Amine-based depressants could also be used to depress excessive fine-milled MgO-containing gangue minerals and liberated pyrrhotite.

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