

Article

# Effects of ATIG Welding on Weld Shape, Mechanical Properties, and Corrosion Resistance of 430 Ferritic Stainless Steel Alloy

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**Abstract:** Flux activated tungsten inert gas (ATIG) welding is a variant of tungsten inert gas (TIG) welding process with high production efficiency, high quality, low energy consumption, and low cost. The study of activating flux mechanism by increasing weld penetration has direct significance in developing flux and welding process. This study has been conducted on 430 ferritic stainless steel alloy. Design of experiment is used to get the best formulation of flux. Based on Minitab17 software, nineteen compositions of flux were prepared using the mixing method. Fluxes are combinations of three oxides ( $\text{MoO}_3\text{-TiO}_2\text{-SiO}_2$ ). Using the optimizer module available in Minitab 17 software, the best formulation was obtained to achieve the best weld depth. Hence, the obtained depth is twice greater than that achieved by conventional TIG welding. Moreover, mechanical properties and corrosion resistance have been investigated for TIG and ATIG welds respectively in tensile, impact, and hardness tests, and in potentiodynamic polarization measurement test.

**Keywords:** ATIG; ferritic stainless steel; weld shape; mechanical properties; corrosion resistance

## 1. Introduction

Tungsten inert gas (TIG) welding process is widely applied in the stainless-steel fabrication industry when weld quality is required. However, the productivity achieved by this process is low because of its shallow depth of penetration. On the other hand, TIG process can be performed with flux activated tungsten inert gas (ATIG) and it consists of depositing a thin layer of metallic oxides on the workpiece surface before welding. ATIG presents the possibility of increasing the penetration depth using the same conventional TIG welding parameters. The use of activating fluxes for TIG welding (ATIG) was invented by the E.O Paton Institute of Electric Welding in the sixties [1,2]. It was originally intended to be used with titanium and then with steels and copper-base alloys [3–5]. It has the advantages of eliminating the need of edge preparation, increasing the penetration depth, and

reducing the number of weld pass. Consequently, the process resulted in narrow welds, small size of HAZ, low heat input, and decrease in residual welding distortions. The productivity of ATIG process could be increased up to 3 times compared to the conventional TIG process [6–8]. Two types of mechanism have been formulated to explain the high penetration of ATIG welds:

- (1) Marangoni convection mechanism: The molten metal behaves like pure metal and a centrifugal convection phenomenon is instigated in the welding joint. The molten metal moves from center of weld pool to the edges, leading to a wide and shallow weld bead, contrariwise ATIG weld metal has a centripetal movement related to oxygen liberated from oxides during the welding operation. Oxygen, tellurium, selenium, and sulfur as surfactant elements, even in small quantities, contribute to a centripetal convection, leading to a depth weld bead [9–16].
- (2) Arc constriction mechanism: During the ATIG welding process, fluorine or chlorine elements migrate towards the arc weld and react with the outer arc electrons. The latter phenomenon contributes to a constriction of the arc. Such constriction of the arc increases the temperature at the anode because of the increase in the current density at the anode (arc spot is constricted) and the arc force action on the weld pool (Lorentz force). Moreover, fluorine contributes to the increase in the associated arc voltage [17–21].

Literature shows that more than 32 different oxides were used for ATIG welding of stainless steel according to their weld specimen in order to increase the weld penetration [22]. Fluxes can be used in the form of single flux (oxide or halide type) to study their individual effect on the morphology and on the mechanical properties [23–25], or in the form of mixed fluxes. In general, the mixed fluxes can be either binary or ternary. The binary fluxes allow getting optimum percentages that can improve the aspect, and the shape, as well as the mechanical properties of welds [26–31]. However, in ternary fluxes, statistical programs are used to develop a formulation on the percentages of the flux components in the aim of enhancing depth and mechanical properties of the welds [32–35].

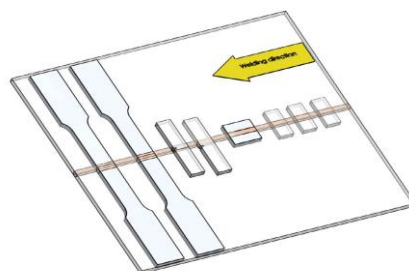
In this work three different kinds of oxide fluxes, namely  $\text{MoO}_3$ - $\text{TiO}_2$ - $\text{SiO}_2$ , were used to investigate the effects of combinations of these oxides and the best composition of flux to improve the depth of weld with the best mechanical properties of 430 ferritic stainless steel comparing to the conventional TIG process.

## 2. Experimental Procedure

Test specimens were made from 430 ferritic stainless steel with dimensions 200 mm × 200 mm × 5.5 mm. Chemical composition was shown in Table 1. Figure 1 shows test samples for mechanical testing and weld morphology. Prior welding acetone was used to clean and remove dust and contaminations.

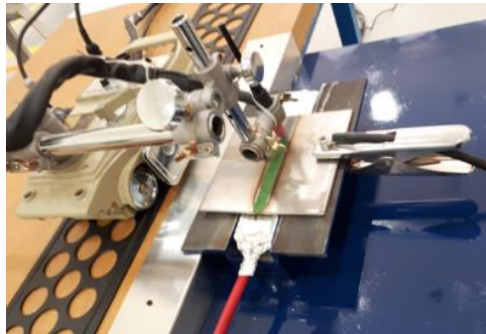
**Table 1.** Chemical composition of 430 ferritic stainless steel.

Elements	C	Mn	P	S	Si	Cr	Ni	N
Weight %	0.025	0.25	0.032	0.0015	0.031	16.28	0.017	0.0546



**Figure 1.** Test specimens for mechanical testing and weld morphology.

Three different kinds of oxide fluxes,  $\text{SiO}_2$ ,  $\text{MoO}_3$ , and  $\text{TiO}_2$ , were used. Products have been heated separately in furnace at  $150\text{ }^\circ\text{C}$  during 1 h to eliminate humidity. A flux in the form of powder has been mixed with acetone and made in the form of paste; brush was used to apply the mixture on plain surface to be welded. The TIG welding machine was used. A water-cooled torch with a standard 2% thoria tungsten electrode rod having diameter of 3.2 mm has been used for the experiments. The end of the electrode was prepared by reducing the tip angle to  $45^\circ$  and the arc length was 2 mm. The shield gas flow rate was 8 L/min and 4 L/min on back side of weld. The torch was mounted on a motorized carriage as shown in Figure 2. The welding parameters selected for TIG welding are listed in Table 2.



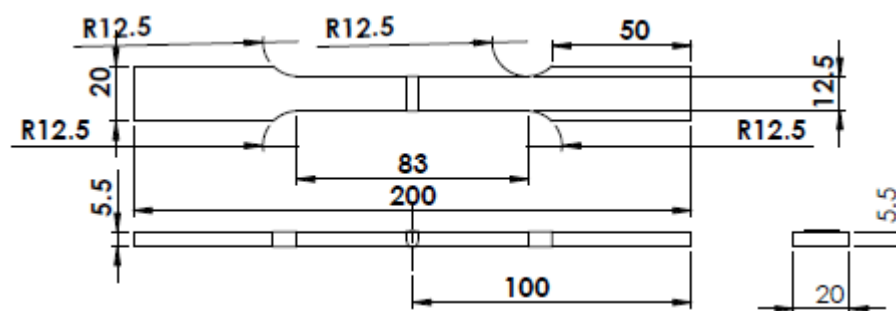
**Figure 2.** Experimental machine of TIG welding with flux paste: a motorized carriage, torch and workpiece.

**Table 2.** Welding parameters.

Parameters	Range
Welding speed	15 cm/min
Welding current	180 Amp
Arc Length	2 mm
Electrode tip angle	$45^\circ$
Shield gas on work piece	Argon with flow rate 12 L/min
Shield gas on back side	Argon with flow rate 5 L/min
Welding mode	Negative direct current electrode

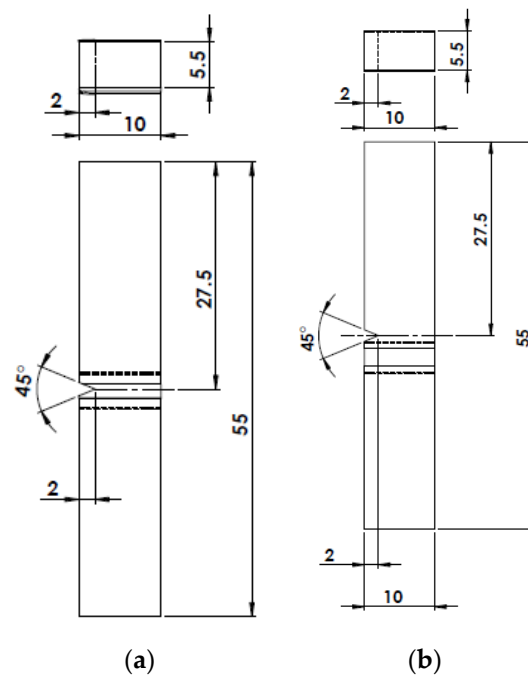
After the welding process, the samples for mechanical testing (tensile, impact and hardness tests) were cut far from the welding starting point to be sure that at this location the arc welding was stabilized. The morphology of the welds was revealed by an etching operation of the samples in an acid bath consisting of one volume of water, 2 volumes of hydrochloric acid (HCl) and one volume of nitric acid ( $\text{HNO}_3$ ). Samples for hardness measurements underwent the same treatment mentioned above.

The tensile tests were carried out with a computer control electro-hydraulic servo universal testing machine model WAW-300E (Jinan testing equipment IE, Jinan, China). The specimens were cut according to ASTM E8M-04 as shown in Figure 3.



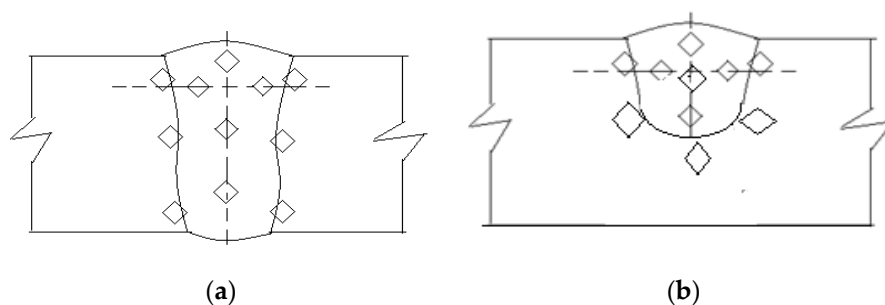
**Figure 3.** Test specimen for the tensile test (units in mm).

The impact tests were performed with the Charpy “V” notch impact testing machine model JBS-500 (Jinan testing equipment IE, Jinan, China). The specimens were cut according to ASTM E23 and broken in the impact test in the weld zone and in the heat affected zone (HAZ) as shown in Figure 4.



**Figure 4.** Test specimens for the impact test (units in mm). The notch is in the weld zone (a) and in the heat affected zone HAZ (b).

Vickers hardness measurements were obtained by a digital hardness tester model HVS-50 (SCTMC, Shanghai, China) and according to ASTM E92-82 with a standard load of 10 kgf. For each sample, the considered result was the average value of five indentations in the weld bead as shown in Figure 5.



**Figure 5.** Hardness test locations in the FZ and HAZ of ATIG (a) and TIG (b).

In order to investigate the corrosion resistance, potentiodynamic polarization tests were used by a potentiostat system AUTOLAB-PGSTAT302N (Metrohm, Utrecht, Netherlands). The samples were cut to the dimensions of  $20 \times 20 \text{ mm}^2$  and polished to 1200 grit with SiC Emri papers. The tests were conducted on parent material, TIG welded material and ATIG welded material. The potentiodynamic tests were carried out at room temperature in 3.5% NaCl and at a scan rate of 1 mV/s. Silver chloride (Ag/AgCl) was used as the reference electrode, platinum (Pt) as the auxiliary electrode, and the sample as the working electrode.

### 3. Results

#### 3.1. Weld Morphology

Mixing method in mini tab 17 software (version 17, Minitab, Pennsylvania State University, State College, PA, USA), which is the more appropriate in our work, was applied and that reduce the number of experiments to be conducted. The obtained results are reported in Table 3.

**Table 3.** Weld bead dimensions and ratio R for the used nineteen fluxes.

Exp. No.	TiO <sub>2</sub> (weight %)	MoO <sub>3</sub> (weight %)	SiO <sub>2</sub> (weight %)	W (mm)	D (mm)	R = D/W
1	100	0.00	0.00	7.94	3.94	0.50
2	75	25	0.00	7.74	4.53	0.59
3	50	50	0.00	6.90	5.32	0.77
4	25	75	0.00	8.56	3.06	0.36
5	0.00	100	0.00	8.46	4.47	0.53
6	0.00	75	25	9.88	4.00	0.40
7	0.00	50	50	11.96	2.74	0.23
8	0.00	25	75	8.84	4.33	0.49
9	0.00	0.00	100	8.80	3.06	0.35
10	25	0.00	75	8.58	5.03	0.59
11	50	0.00	50	7.96	3.97	0.50
12	75	0.00	25	8.84	3.98	0.45
13	33.33	33.33	33.33	7.48	4.75	0.64
14	66.66	16.66	16.66	7.98	4.81	0.60
15	16.66	66.66	16.66	9.22	4.23	0.46
16	16.66	16.66	66.66	8.96	3.70	0.41
17	25	50	25	10.84	3.16	0.29
18	25	25	50	8.84	4.39	0.50
19	50	25	25	9.06	4.55	0.50

The weld morphology is characterized by the penetration depth D and the bead width W giving the ratio R (D/W).

#### 3.2. Mixture Contour Plot

In order to obtain a better depth of weld bead, an optimum combination of the fluxes for the maximum penetration was estimated using Minitab 17 software with the mixing method. The input data was the compositions of flux and the output response was the depth and the ratio (D/W). Triangular coordinate systems allow visualizing the relationships between the components in a three-component mixture. The mixture contour plots of the generated depth of penetration D using Minitab software is shown in Figure 6 and the contour plots of the ration R is shown in Figure 7. All the contour plots were generated based on the experimental results.

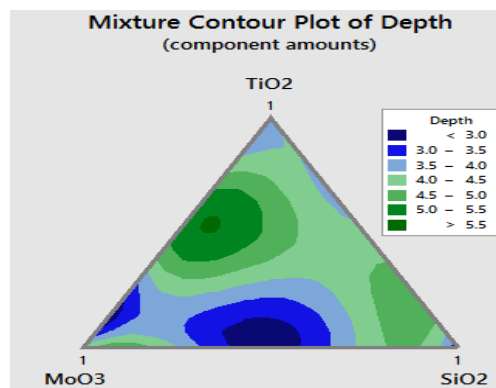


Figure 6. Mixture contour plot of depth D.

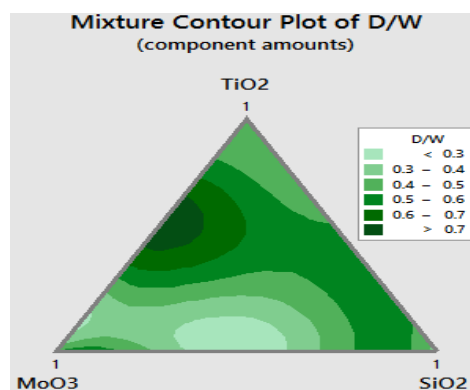
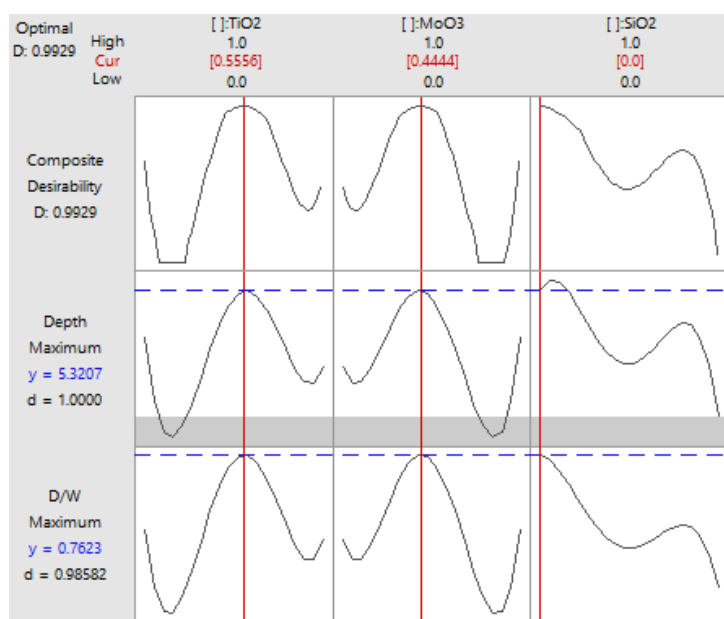


Figure 7. Mixture contour plot of ratio R (D/W).

The mixture contour plot for depth shows a large region where the maximum depth can be attained.

The mixture contour plot of ratio R shows a very small confined region where a maximum ratio can be achieved. This region is poor on  $\text{SiO}_2$  and rich on  $\text{TiO}_2$  and  $\text{MoO}_3$ . To get the best proportions of this three ingredients we used the optimizer module available in Minitab 17. Figure 7 displays the optimization plot for depth and ratio D/W.

The optimization plot in Figure 8 shows how the variables  $\text{TiO}_2$ ,  $\text{MoO}_3$ , and  $\text{SiO}_2$  affect the predicted responses in terms of depth and ratio D/W. Numbers at the top of the columns that show the current variable settings and the high and low variable settings in the data. Two points for each cell represent the two levels of the categorical variable so the level for each variable is 1 (high level) and level 0 is low level. The in between level represents the best mixing flux composition which is 56%  $\text{TiO}_2$  + 44%  $\text{MoO}_3$  + 0%  $\text{SiO}_2$ .



**Figure 8.** The optimization plot for depth and ratio D/W.

The first column in Figure 8 contains, for the current variable settings, the predicted response “y”, and the individual desirability score “d”. So, the predicted response for depth is  $y = 5.32$  mm and the corresponding desirability is 1. The predicted response for ratio D/W is  $y = 0.76$ , the corresponding desirability is 0.98. The overall composite desirability becomes 0.99. It indicates that the variables achieve favorable results for all responses, which means that both responses are within acceptable limits.

### 3.3. Confirmation Test

ATIG welding was performed using the flux having the optimum composition (optimal flux) under the same welding parameters. The cross-sections of the weld beads were photographed using an optical microscope CAROLINA (CAROLINA, Burlington, VT, USA). The obtained penetration depth D was 7.24 mm and the bead width W was 9.70 mm leading to an aspect ratio D/W of 0.75. Bead profile data of the weldments of ATIG with the optimal flux and of the conventional TIG are listed in Table 4 and displayed in Figure 9. Figure 10 presents micrographs showing the cross section of TIG welded bead and that of ATIG with optimal flux. It is clearly shown that the bead has a full penetration for ATIG. Tables 4 and 5 show standard deviation ( $\sigma$ ), which represents a measure of the amount of variation or dispersion of a set of values. For depth and width measurements, standard deviation is less than 0.3 mm.

**Table 4.** Measurements of depth and standards deviation of TIG and ATIG (optimal flux).

Sample	Number of Tests	Max. Depth (mm)	Min. Depth (mm)	Mean Depth (mm)	Standard Deviation $\sigma$
TIG	3	3.9	3.4	3.63	0.251
ATIG	3	7.43	7.1	7.24	0.169

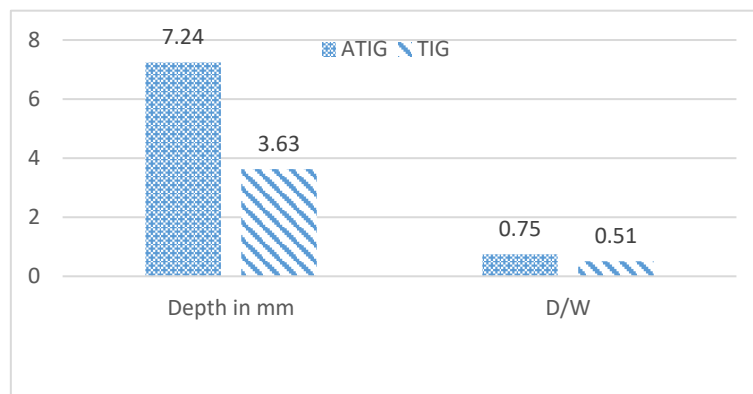


Figure 9. ATIG (optimal flux) and TIG (conventional) welded beads morphology.

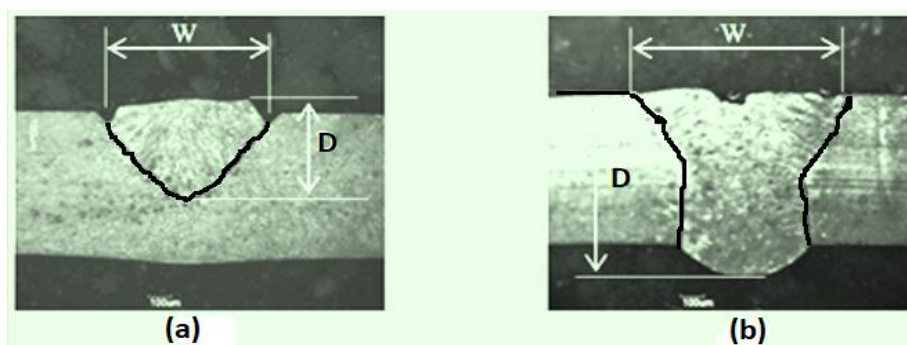


Figure 10. Width (W) and depth (D) of welded beads of TIG (a) and ATIG (b).

Table 5. Measurements of width and standard deviation of TIG and ATIG (optimal flux).

Sample	Number of Tests	Max. Width (mm)	Min. Width (mm)	Mean Width (mm)	Standard Deviation $\sigma$
TIG	3	7.3	7.0	7.14	0.052
ATIG	3	9.8	9.5	9.70	0.100

From Table 6, it can be seen that the ATIG penetration depth was increased of about 99% comparatively to that one of the conventional TIG welding.

Table 6. Weldment bead profiles data of TIG (conventional) and ATIG (optimal flux).

TIG			ATIG		
D	W	D/W	D	W	D/W
3.63	7.14	0.51	7.24	9.70	0.75

### 3.4. Effect of Optimal Flux on Mechanical Properties

#### 3.4.1. Tensile Test

Results of the tensile test show that the ultimate tensile strength UTS related to ATIG welding is bigger than that one of TIG welding of about 9 MPa. However, these values of UTS can be considered close, as shown in Figure 11. So, we conclude that the optimal flux used in ATIG welding had an impact on the strength resistance of the weld. We notice that the fractures for both TIG and ATIG occur far from the weld zone as shown in Figure 12. Table 7 shows the maximum, minimum, mean and standard deviation ( $\sigma$ ) of tensile strength. Standard deviation is less than 19 MPa.



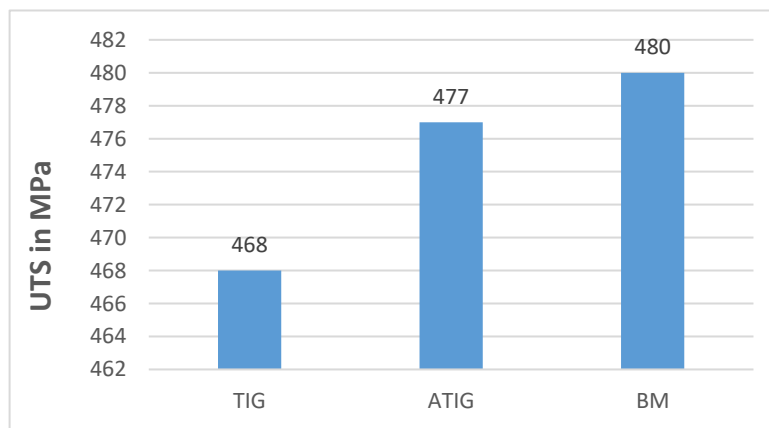


Figure 11. Tensile test results.

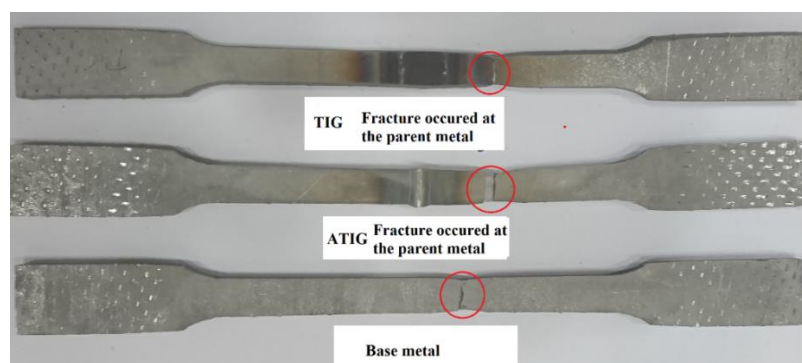


Figure 12. Fracture zones in base metal, TIG weld and in ATIG weld.

Table 7. Measurements of tensile strength and standard deviation of TIG and ATIG (optimal flux).

Sample	Number of Tests	UTS Max. (MPa)	UTS Min. (MPa)	UTS Mean (MPa)	Standard Deviation $\sigma$
TIG	3	482	457	468	12.76
ATIG	3	498	465	477	18.2

### 3.4.2. Hardness Test

Five measurements of Vickers hardness were performed on the cross sectioned coupon in two regions, namely the fusion zone FZ and heat affected zone HAZ. The considered hardness measurement value is the average of these five measurements. Figure 13 shows the Vickers hardness results of TIG weldment without and with activating fluxes in FZ and HAZ. It can be clearly seen that the hardness of ATIG weld is slightly greater than those of TIG weld in both FZ and HAZ. Table 8 shows maximum, minimum, mean, and standard deviation ( $\sigma$ ) of hardness HV. Standard deviation is less than 9 HV.

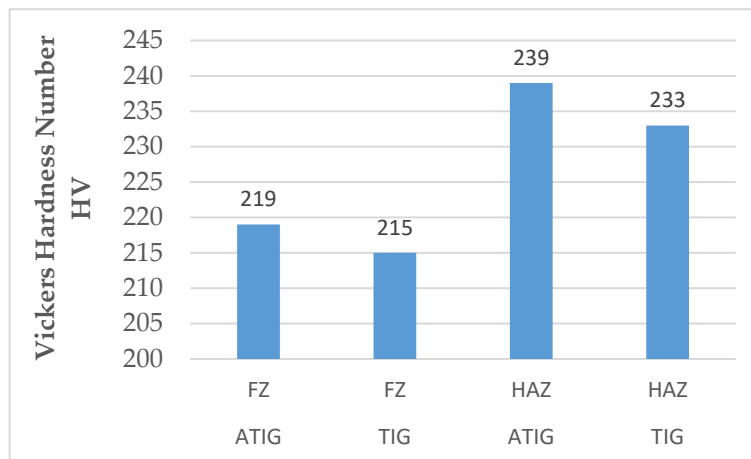


Figure 13. Hardness test results.

Table 8. Measurements of hardness and standard deviation of TIG and ATIG (optimal flux).

Sample		Number of Tests	HV Max.	HV Min.	HV Mean	Standard Deviation $\sigma$
TIG	FZ	5	229	207	215	8.955
	HAZ	5	237	228	233	3.701
ATIG	FZ	5	229	210	219	6.719
	HAZ	5	244	234	239	4.573

### 3.4.3. Impact Test

In order to accurately evaluate the breaking energy in the whole sample, two positions of the notch have been considered and fabricated on the sample, one notch in the fusion zone (FZ) and the other in the heat affected zone (HAZ). Figure 14 presents the obtained results of the impact test in FZ related to conventional TIG welding and ATIG welding with the optimal flux. The results show that the absorbed energy for ATIG weld was 93 J and fell to 59 J for TIG weld. Hence, the result confirms the benefits of using ATIG welding with the optimal flux. The Table 9 shows maximum, minimum, mean, and standard deviation ( $\sigma$ ) of energy absorbed in fusion zone. Standard deviation is less than 1.5 J.

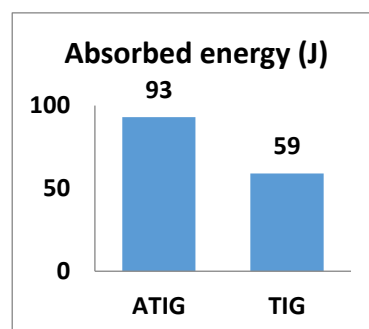
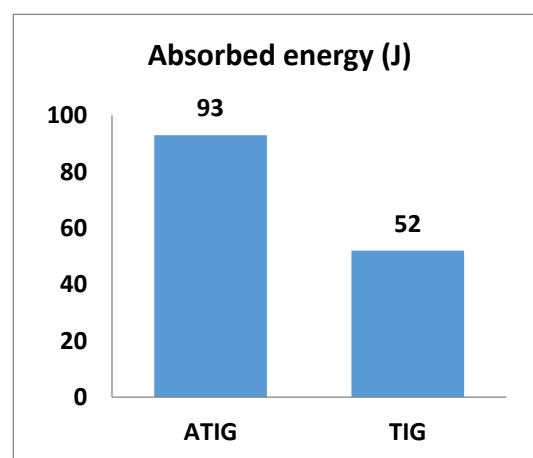


Figure 14. Impact test results of ATIG and TIG in FZ.

**Table 9.** Mesurments of energy absorbed and standards deviation of TIG and ATIG (optimal flux) at fusion zone.

Sample	Number of Tests	Absorbed Energy (J) Min	Absorbed Energy (J) Max	Absorbed Energy (J)	Standard Deviation $\sigma$
TIG	3	56	60	59	1.00
ATIG	3	92	95	93	1.32

Figure 15 presents the obtained results of the impact test in HAZ of conventional TIG welding and ATIG welding with the optimal flux. The results show the same trend as above (notch at FZ). The absorbed energy in HAZ of ATIG weld rose to 93 J. In contrast, the absorbed energy of TIG welds was within limit of 52 J. Once again, the result confirms the advantage of ATIG welding regarding the impact test.

**Figure 15.** Impact test results of ATIG and TIG in HAZ.

The Table 10 shows maximum, minimum, mean, and standard deviation ( $\sigma$ ) of energy absorbed in HAZ. Standards deviation is less than 1.5 J.

**Table 10.** Mesurments of energy absorbed and standards deviation of TIG and ATIG (optimal flux) at HAZ.

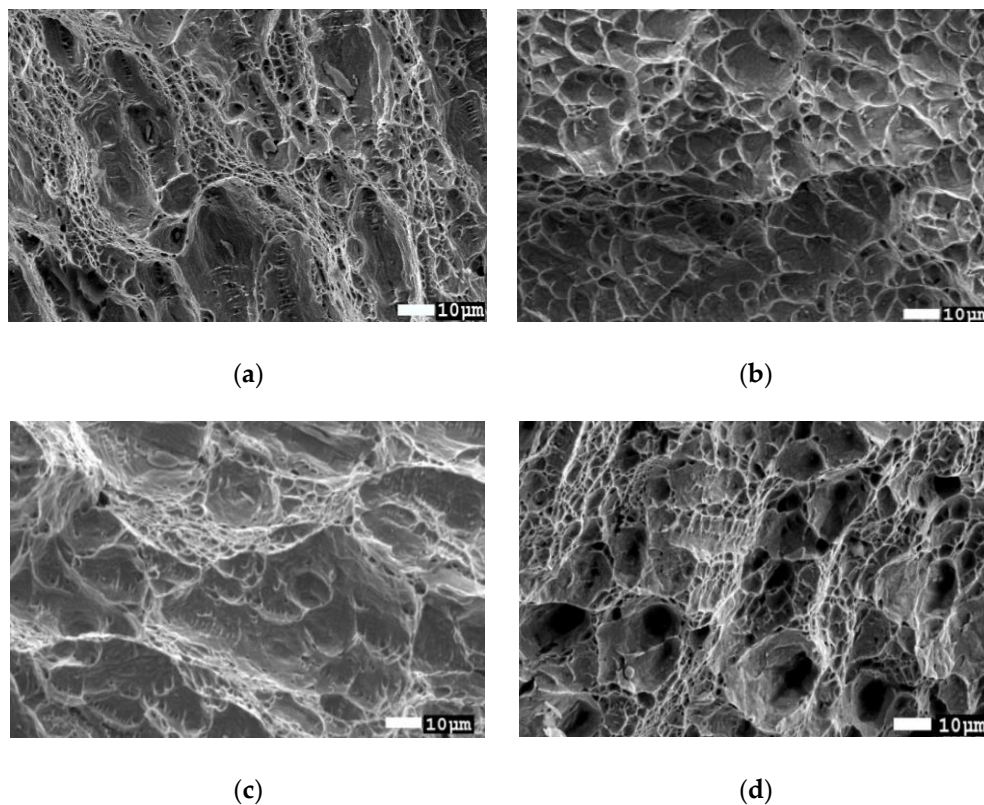
Sample	Number of Tests	Absorbed Energy (J) Min.	Absorbed Energy (J) Max.	Absorbed Energy (J)	Standard Deviation $\sigma$
TIG	3	50	54	52	1.32
ATIG	3	92	95	93	1.32

The obtained impact test results for ATIG welding in FZ or in HAZ are similar. Moreover, almost the same tendency is obtained for TIG welding. As ATIG weld bead is too large, the heat is evacuated slowly; and the proportion of martensite is less than that of TIG welding. As TIG weld bead is relatively small and characterized by a fast cooling rate, martensite and sigma phases are very likely to be developed. Due to the fact that martensite and sigma phases are brittle, the ATIG weld has the property to withstand to sudden loads than TIG weld. On the other hand, the formation of carbide titanium, due to the presence of titanium in the optimal flux in ATIG weld, refines the weld zone grains and so improves the ductility of ATIG weld [36].

### 3.5. Microstructure

#### 3.5.1. SEM Analysis

Fractographs of impact test conducted on JEOL JSM-7600F scanning electronic microscope (SEM, JEOL, Tokyo, Japan) are represented in Figure 16a–d. Micrograph in Figure 16b shows the formation of multiple dimples which demonstrate that the fracture is in ductile mode in the case of ATIG weld zone. In ATIG heat affected zone in Figure 16d, the fracture is also in ductile mode but with multiple dimples. Moreover, a phenomenon of coalescence of micro-voids leads to the formation of noticeable macro-voids. Combined ductile and brittle fracture mode characterizes the TIG weld zone as well as the TIG heat affected zone as shown in Figure 16a,c. The fracture surface is composed of thin ridges containing colonies of dimples scattered among regions containing cleavage facets. Hence and according to the fractography analyses, in ATIG welding the fracture is ductile and the breaking energy in impact test is relatively high. However, the combined ductile and brittle fracture mode lead to poor resistance for sudden impact loads, as in TIG welding. This analysis explains the obtained results in impact test.



**Figure 16.** Fractographs of impact test in: (a) TIG weld zone; (b) ATIG weld zone; (c) TIG heat affected zone and (d) ATIG heat affected zone.

#### 3.5.2. EDS/SEM Analysis

Figures 17 and 18 show spectrum analyses of fracture face of TIG and ATIG weld zones, respectively.

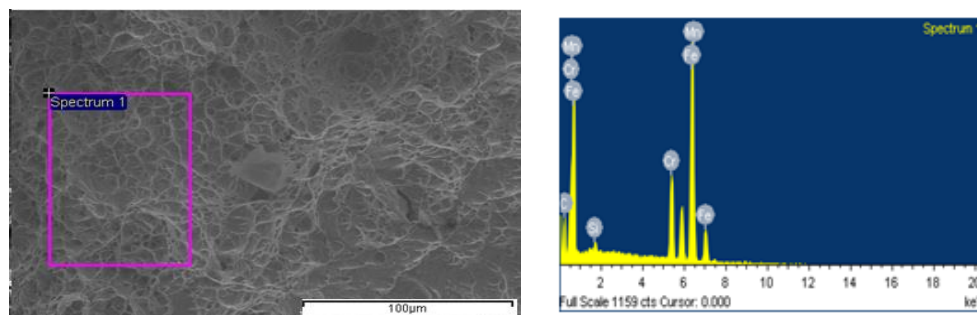


Figure 17. EDS/SEM spectrum analysis of fracture face of TIG weld zone.

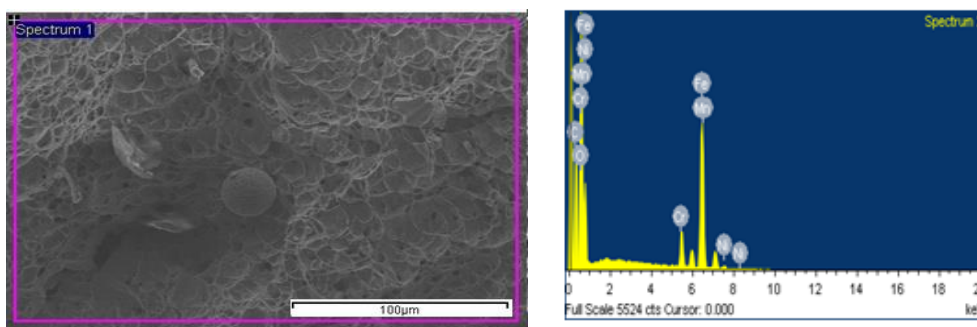


Figure 18. EDS/SEM spectrum analysis of fracture face of ATIG weld zone.

Table 11 shows a decrease of carbon in TIG weld zone compared to the result of ATIG displayed in Table 12. The cooling rate in TIG weld is also fast. Hence, there is a formation of martensite at ferrite grain boundaries. Consequently, carbon element is trapped at the grain boundaries and impedes the formation of high quantities of carbides  $(Cr,Fe)_{23}C_6$  as reported by Lippold and Kotecki [37]. In contrast, in the ATIG weld, the cooling rate is relatively slow due to large size of the weld bead and the formation of martensite being less than that of TIG weld. Moreover, the presence of titanium and molybdenum in the optimal flux contribute to the decrease of the amount of carbides  $(Cr,Fe)_{23}C_6$ . Both elements are strong carbide formers (TiC, MoC) in grains and grain boundaries [38]. The formation of titanium and molybdenum carbides prevents the depletion of chromium in boundaries, which is a benefit to the corrosion resistance

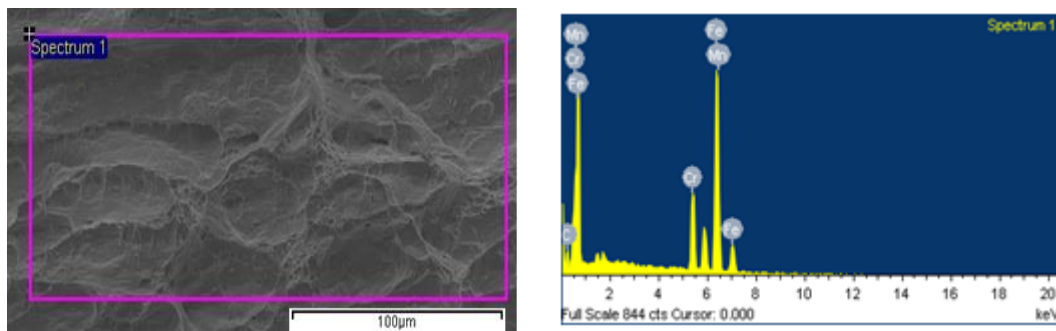
Table 11. Elements present in fracture face of TIG weld zone.

Elements	C	Si	Cr	Mn	Fe
Weight %	11.12	0.60	13.81	10.37	64.11

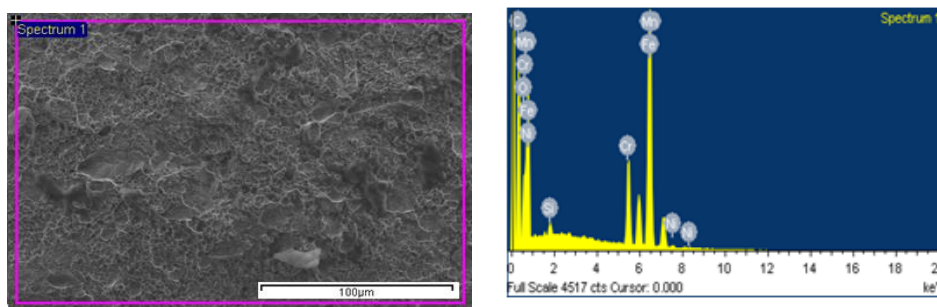
Table 12. Elements present in fracture face of ATIG weld zone.

Elements	C	O	Si	Cr	Mn	Fe
Weight %	18.51	2.67	0.46	12.25	9.21	56.90

Figures 19 and 20 show spectrum analyses of fracture face of TIG and ATIG respectively in HAZ. The TIG weld is partially penetrated and the HAZ rapidly cools leading to the formation of high proportion of martensite phase. Consequently, the available quantity of carbon element is low as shown in Table 13. Regarding ATIG, the HAZ cools slowly and the quantity of martensite is relatively low. Hence, the carbon remaining in carbide precipitations is high as shown in Table 14.



**Figure 19.** EDS/SEM spectrum analysis of fracture face of TIG heat affected zone.



**Figure 20.** EDS/SEM spectrum analysis of fracture face of ATIG heat affected zone.

**Table 13.** Elements present in fracture face of TIG heat affected zone.

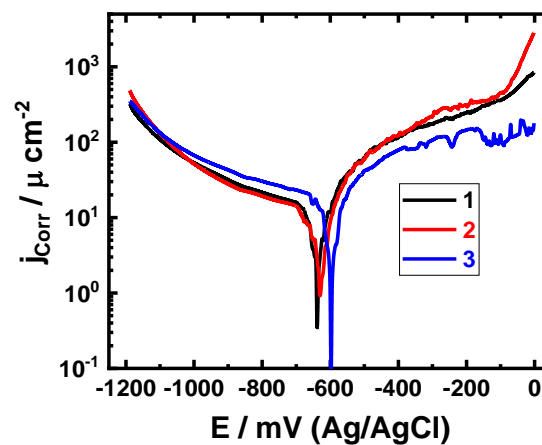
Elements	C	Cr	Mn	Fe
Weight %	6.13	15.23	9.45	69.19

**Table 14.** Elements present in fracture face of ATIG heat affected zone.

Elements	C	O	Si	Cr	Mn	Fe	Ni
Weight %	28.31	3.61	0.45	10.03	7.46	49.21	0.93

### 3.6. Corrosion Behavior

Figure 21 shows the potentiodynamic curves of ferritic stainless steel base metal, TIG welded and ATIG welded.



**Figure 21.** Potentiodynamic polarization curves obtained for (1) Base metal, (2) TIG, and (3) ATIG. after 1 h immersion in the 3.5% NaCl solutions.

The electrochemical parameters are listed in Table 15.

**Table 15.** Potentiodynamic polarization data obtained for the different materials after 1 h immersion in 3.5% NaCl solutions.

Alloy	$\beta_c$ $mV \cdot dec^{-1}$	$E_{Corr}$ $mV$	$\beta_a$ $mV \cdot dec^{-1}$	$j_{Corr}$ $A \cdot cm^{-2}$	Corrosion Rate $mm/y$
Base metal	210	−637	115	9.5	0.102
TIG	170	−640	120	6.7	0.072
ATIG	162	−600	150	8.7	0.094

The corrosion potential is a static indicator of electrochemical corrosion resistance, which reveals the susceptibility of materials to corrosion. It is visible that the corrosion potential  $E_{corr}$  for metal welded with flux ATIG was shifted to positive value with respect to both base metal and metal welded with TIG. The weld obtained from the optimal flux exhibit better corrosion resistance (−600 mV). On the other hand, the corrosion rate, which is a kinetic characteristic of surface material, of ATIG decreased to 0.094 mm/y when compared to the base metal where it was 0.102 mm/y, however it was increased compared to TIG.

#### 4. Conclusions

The present work investigated the effects of three oxides ( $MoO_3$ - $TiO_2$ - $SiO_2$ ) on bead geometry and on mechanical behavior of weldment ferritic 430 stainless steel sheet produced by TIG welding. According to the obtained results, the following conclusions can be drawn:

- (1) Based on the simplex lattice degree four design, nineteen compositions have been prepared from three oxides ( $TiO_2$ ,  $MoO_3$  and  $SiO_2$ ), the best obtained formulation was 55%  $TiO_2$  + 45%  $MoO_3$ . The depth weld of the optimized formula was doubled (7.24 mm) in comparison to conventional TIG weld bead (3.64 mm).
- (2) The mechanical properties (hardness, tensile strength, and breaking absorbed energy) were not decreased using ATIG welding.
- (3) The corrosion potential  $E_{cor}$  for metal welded with the ATIG flux was shifted to positive value.

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