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Mold Nonsinusoidal Oscillation Mode and Its Effect on Slag Infiltration for Lubrication and Initial Shell Growth during Steel Continuous Casting

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Abstract: The effect of nonsinusoidal oscillation at different modification ratios (α) on slag lubrication was investigated during mold oscillation. A validated and reliable multiphase model was employed, which involved flow and solidification of the molten steel and mold slag. The main results revealed that a large amount of liquid slag at the entrance of the mold–strand channel reflowed into the slag pool at the middle of the negative strip period. The phenomenon was more distinct, with an increase in the modification ratio. The modification ratio had no obvious effect on the average thickness of the liquid film at different depths below the meniscus. A modification ratio of 0.5 caused less fluctuation of the transient liquid film. Quantitative prediction of slag consumption indicated that as the modification ratio increased from 0.2 to 0.5 to 0.8, the average values were 0.278, 0.286, and 0.279 kg/m², respectively. Shell solidification and growth near the meniscus mainly occurred when the mold was descending, which not only depended on the heat flux, but also on the liquid slag flow, the pressure driven by slag rim, and the mold oscillation. Optimization of the modification ratio of nonsinusoidal oscillation could be an alternative to delay growth of the initial shell towards the molten steel. A modification ratio of 0.5 had the least robust shell tip at the meniscus, thereby reducing entrapment of inclusions and bubbles by the shell tip.

Keywords: numerical simulation; steel; continuous casting; nonsinusoidal oscillation; lubrication; slag consumption; initial shell growth

1. Introduction

Mold oscillation technology was pioneered by Junghans [1,2] in the early 1930s and successfully applied to the continuous casting of nonferrous metal, which initiated large scale industrial application. In 1949, Junghans and Rossi [1,2] first implemented an oscillating mold for the continuous casting of steel, with the aim of smooth demolding and friction reduction on the strand surface. In early oscillating molds, the copper plates are always periodically moved downward a certain distance at a velocity equal to the casting speed, and then rapidly returned to the initial position [1]. Consequently, both the absence of gradual varied velocity difference between the mold (V_m) and strand (V_c) and the abrupt change in direction of mold movement could cause negative effects on oscillating devices and increase the incidence of breakout. A significant advance was the conversion to sinusoidal oscillation mode [1]. Sinusoidal oscillation eliminated the inherent velocity relationship between the mold and the solidifying shell. This technique performed well in healing tiny cracks on the strand surface during the negative strip period (NSP; t_n , the portion of the oscillation cycle where the mold descend faster than the shell) [3–5] and in the demolding process during the positive strip period (t_p , which constitutes the

remainder of the oscillation cycle). With increasing diversity of continuous casting technology, such as use of high-speed casting and some special steel grades, the adjusting ability of sinusoidal oscillation is, however, limited, because it only depends on the oscillation frequency and amplitude. To satisfy the requirements of further reducing the friction and improving the lubrication conditions exerted on the strand surface, an innovative nonsinusoidal oscillation mode was proposed by Mizukami et al. [6] and Suzuki et al. [7], and a new oscillation parameter—the modification ratio (α)—was introduced on the basis of sinusoidal oscillation, as indicated in Figure 1a. α represents the extent of asymmetry of the nonsinusoidal oscillation, which is defined as the time shift of the highest (or lowest) peak from the corresponding sinusoidal peak compared with one-quarter of the total period of the oscillation cycle [8,9].

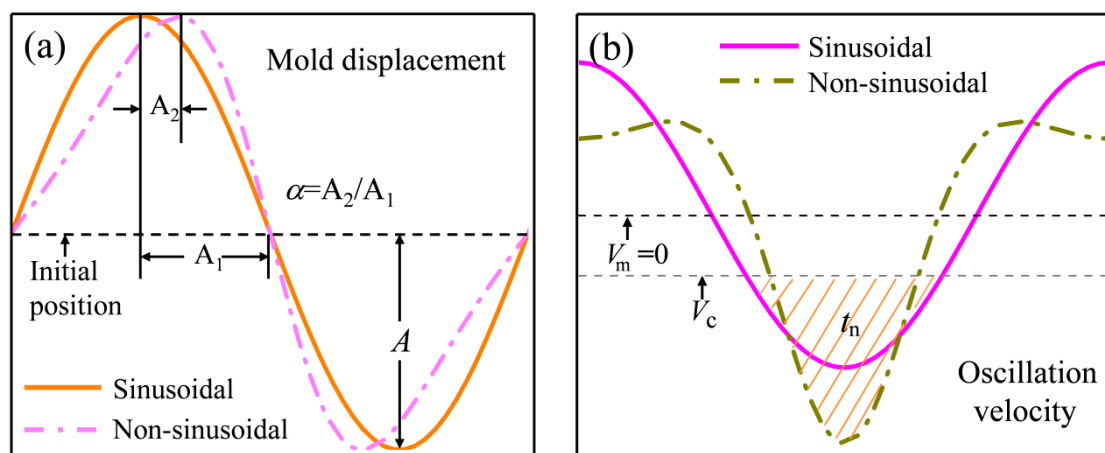


Figure 1. Schematic of sinusoidal and nonsinusoidal oscillation waveform curves: (a) mold displacement and (b) mold oscillation velocity.

Figure 1b shows that nonsinusoidal oscillation has a rapid velocity change during the downward oscillation and a shorter t_n and longer t_p than those of sinusoidal oscillation. As previously reported [10–13], oscillation marks on the strand surface become deeper with longer t_n ; hence, the nonsinusoidal mode is favorable in ameliorating the surface quality. The required level of the compressive force imposed on the solidified shell increases with increased relative speed during t_n and, due to the elongation of t_p , the decreased relative speed in t_p between the mold and strand can reduce the tensile force exerted on the solidified shell, which may be critical to solder surface cracking and strand demolding [4]. Several industrial trials and laboratory experiments [6,7,9,10,14–19] have been conducted to investigate the influence of nonsinusoidal oscillation mode on the continuous casting process, as summarized in Table 1.

Previous studies indicate that nonsinusoidal oscillation was preferred over the conventional sinusoidal mode in certain aspects, such as enhancement of slag consumption and reduction of the frictional force, yet it was not clear what the mechanisms of slag infiltration were for nonsinusoidal mode. Furthermore, the influence of α on lubrication, which is the most noticeable distinction between the nonsinusoidal and sinusoidal modes, has not been thoroughly studied. In the current study, a validated and reliable multiphase model [20] was applied to investigate the effect of α on lubrication to the shell. The following aspects were studied; liquid slag infiltration at the meniscus, distribution of pressure in the flux channel, liquid film thickness, and transient slag consumption. Growth of the solidified shell at the meniscus with various α was also discussed to provide guidance to select the modification ratio.

Table 1. Studies of the effect of nonsinusoidal oscillation mode on slag lubrication.

Method	Main Findings	Authors	Year	Refs.
Experimental continuous caster	Nonsinusoidal mode was more effective to reduce the friction force on the strand surface by ~60% and increased the slag consumption by ~10% compared to the conventional sinusoidal mode at 2.0 m/min.	Mizukami et al.	1986	[6]
Industrial trials	The liquid frictional force decreased by ~40% with 0.4 of α , and most of the reduction was attributed to the decrease of relative speed during the t_p .	Suzuki et al.	1991	[10]
Industrial trials	The maximum friction exerting on the initial shell for the nonsinusoidal mode ($\alpha = 0.4$) was reduced by approximately 62% at 2.0–2.2 m/min in comparison with that for sinusoidal mode.	Suzuki et al.	1992	[7]
Mold simulator	Slag consumption improved significantly with the increased of α from 0 to 0.4.	Tsutsumi et al.	1998	[14]
Industrial trials	Nonsinusoidal mode ($\alpha = 0.24$) resulted in an increase of slag consumption by ~10%.	Shin et al.	2006	[9]
Mathematical model	With the prolongation of t_p , the slag consumption increased, the maximum friction force on the strand surface decreased significantly with the increase of α .	Wang et al.	2010	[15]
Mathematical model	The liquid slag–film thickness increased from less than 100 μm for the sinusoidal case to 200 μm for the nonsinusoidal mode.	Lopez et al.	2012	[16]
Cold model	Nonsinusoidal oscillation prolonged the t_p , in which the channel was widened, contributing to more slag consumption and lowering frictional force. Higher α increased the negative pressure and improved the slag infiltration.	Yang et al.	2014	[17, 18]
Mathematical model	Increasing α to 0.24 slightly increased slag consumption by 2.4% and the predicted slag consumption enhanced as the increases of α .	Jonayat and Thomas	2014	[19]

2. Solution Methods

2.1. Model

A two-dimensional multiphase model [20] was utilized to investigate the effect of nonsinusoidal oscillation on lubrication to the shell. A schematic of the calculation domain is shown in Figure 2a, which mainly comprises half of a submerged entry nozzle (SEN), an oscillating mold copper plate, and fluid areas including air, molten slag, and steel. Periodic oscillation of the copper plate was realized using the method of dynamic mesh. The mesh of the fluid domain was elaborately refined near the steel–slag interface and adjacent to the copper plate side, in which the minimum cell size was 50 μm (Figure 2b). The number of structured grids was approximately 200,000. The time step was increased gradually, and the value of 0.0001 s was kept after the calculation became stable. The employed mold flux was designed for the continuous casting of low-carbon steel, the basicity and break temperature of which were 0.9 and 1352 K (1079 °C), respectively. The break temperature, T_b , was utilized to distinguish the liquid and solid layers. In the temperature range below, T_b , the slag layer was regarded as solid and, conversely, the slag film was treated as a liquid layer. The viscosity of the mold slag was measured by the rotating cylinder method [21]. Variation of viscosity during the cooling process was as follows

$$\eta_{\text{slag}} = \begin{cases} -0.00152 \times (T - 273) + 2.14, & T > T_b \\ -0.11152 \times (T - 273) + 120.60, & 1335\text{K} < T < T_b \\ 3.0, & T < 1335\text{K} \end{cases} \quad (1)$$

where η_{slag} is the viscosity (kg/(m·s)) of the slag, T is the temperature (K), and T_b is the break temperature (K) of the slag. A comprehensive introduction to the multiphase model, casting parameters, and physical property parameters of the steel and slag used in this study was proposed by Zhang et al. [20].

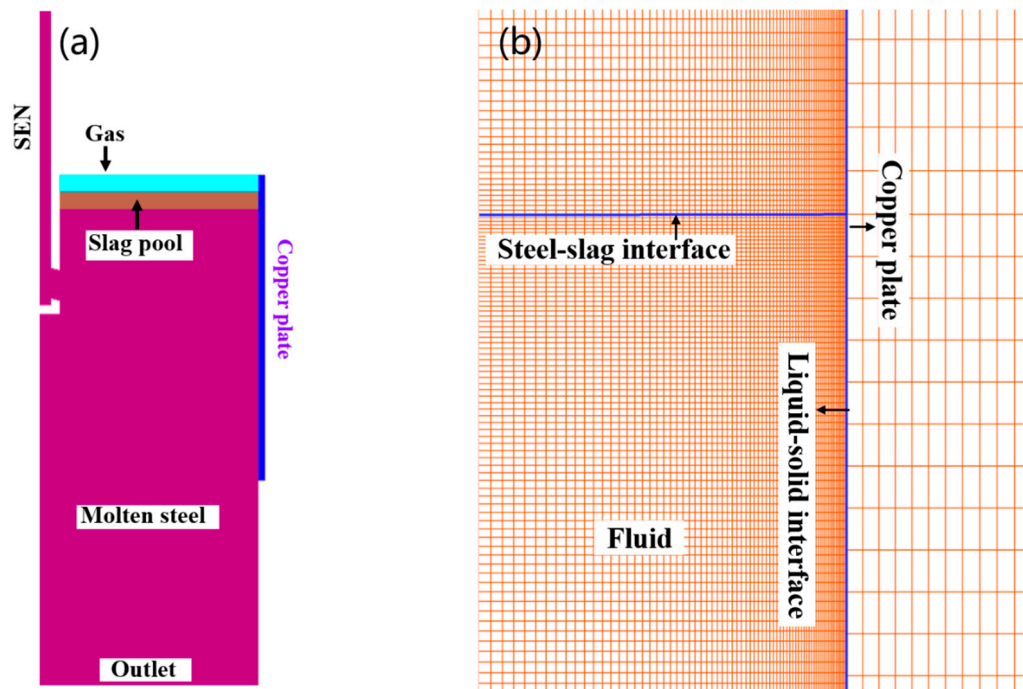


Figure 2. Schematic of (a) mold model and (b) mesh of computation domain.

2.2. Nonsinusoidal Oscillation Mode

Three cases of nonsinusoidal oscillation modes with α of 0.2, 0.5, and 0.8 were discussed. The corresponding curves of oscillation velocity were given in Figure 3. The casting speed was 0.9 m/min, and the mold oscillation amplitude (A , mm) and frequency (f , Hz) were 3 mm and 2 Hz, respectively. The displacement (S , m) and oscillation velocity (V_m , m/s) of the nonsinusoidal mode were expressed as below.

$$S = \frac{A}{1000} \sin[2\pi ft - \alpha \sin(2\pi ft)], \quad (2)$$

$$V_m = 2\pi \frac{A}{1000} f [1 - \alpha \cos(2\pi ft)] \cos[2\pi ft - \alpha \sin(2\pi ft)]. \quad (3)$$

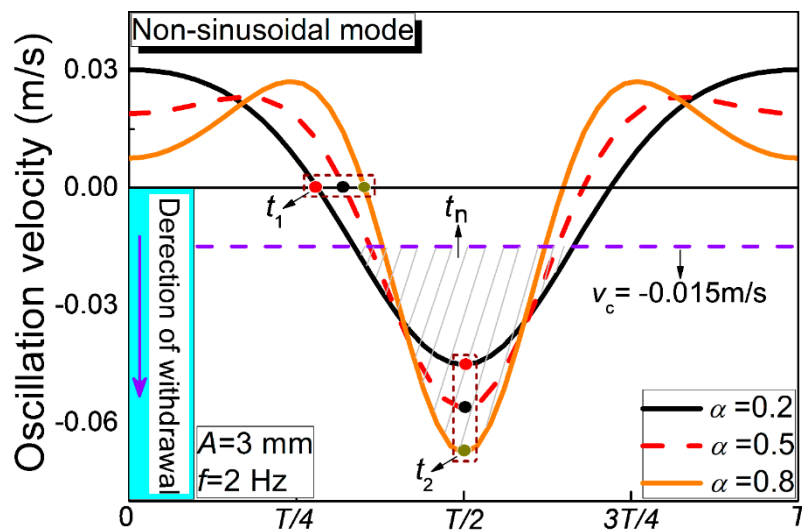


Figure 3. Oscillation velocity of nonsinusoidal mode with different modification ratios.

3. Results and Discussion

3.1. Inflow Behavior of Liquid Slag Near Meniscus

Two specific moments— t_1 and t_2 —as plotted in Figure 3, corresponding to the same oscillation position with different values of α , were selected for comparative analysis of the inflow characteristics of liquid slag at the meniscus. At t_1 , the mold ascended to its highest position with zero velocity in t_p , while at t_2 , the mold moved back to the initial position with peak downward velocity in the middle of t_n . Figure 4 demonstrates the inflow behavior of liquid slag at the entrance of the mold–strand channel, where the liquid slag begins to lubricate the initial solidified shell. To intuitively elucidate the infiltration, the velocity vector of the liquid slag was adopted to indicate its motion. At t_1 , the slag flow was strongly downward into the mouth of mold–strand channel and has an even distribution of velocity for all three cases. Subsequently, as the mold continued to descend and reached the middle of t_n (at t_2) with maximum velocity, a large volume of liquid slag adjacent to the initial shell was squeezed out from the channel and back into the slag pool; the infiltration circumstances of liquid slag predicted in the model was consistent with the reported by Jonayat and Thomas [19]. The flow-back tendency increased with the increase of α . The phenomenon is caused by the solid rim descending under the drive of the copper plate, which imposes an oppressive function on the liquid slag and plays the role of a piston occupying the space of the liquid flux [22]. Compared with the sinusoidal oscillation in our previous work [20], the flow-back motion of nonsinusoidal oscillation was more violent than the former during the middle of t_n . Additionally, the slag channel became narrower to a certain degree from t_1 to t_2 and a broader channel at the meniscus was observed at α of 0.2 than that with higher values of α .

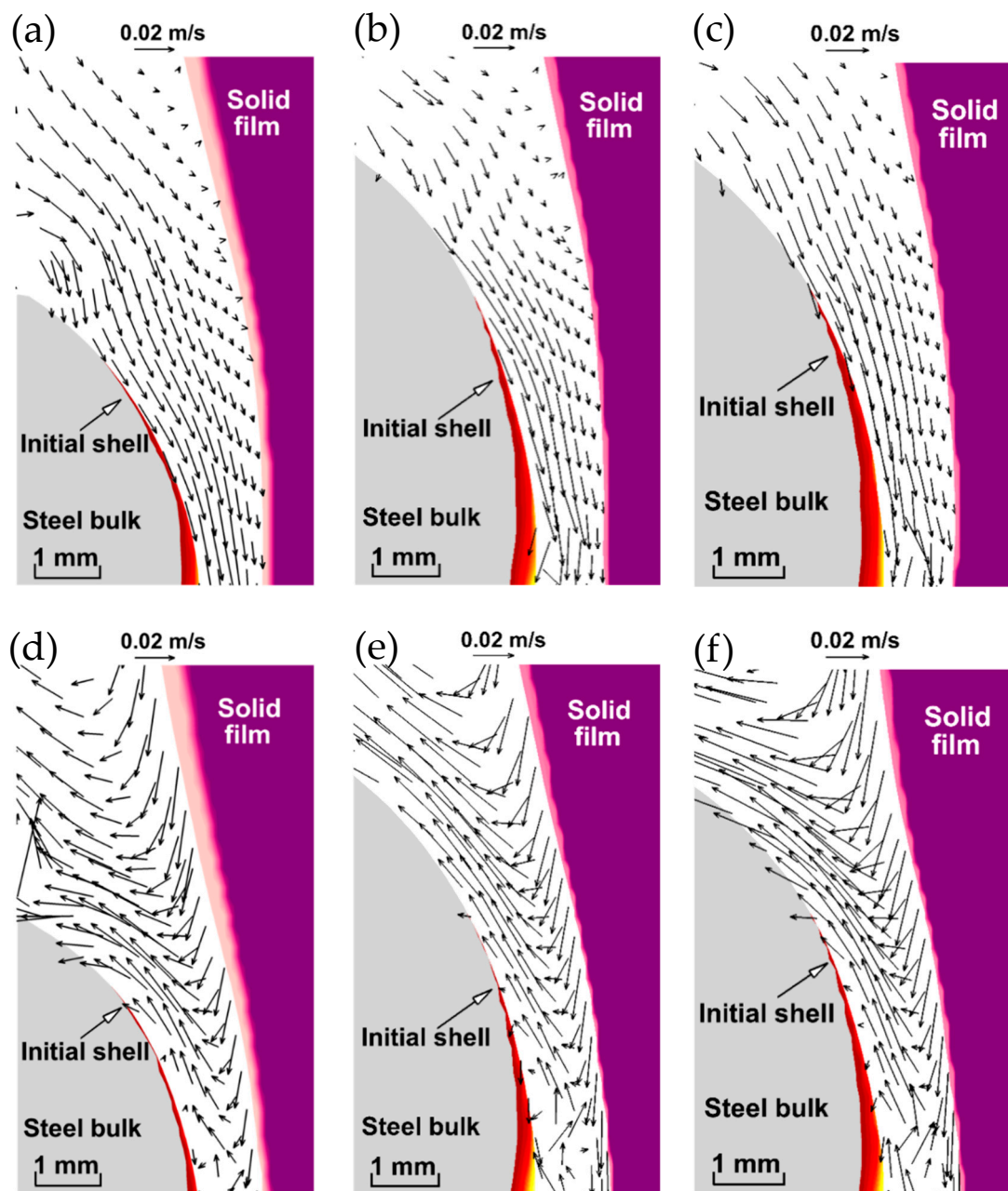


Figure 4. Slag infiltration near the meniscus at different moments for nonsinusoidal oscillation mode: (a) t_1 , $\alpha = 0.2$, (b) t_1 , $\alpha = 0.5$, (c) t_1 , $\alpha = 0.8$, (d) t_2 , $\alpha = 0.2$, (e) t_2 , $\alpha = 0.5$, and (f) t_2 , $\alpha = 0.8$.

Figure 5 shows the corresponding pressure distribution in the slag channel near the meniscus. At t_1 , the downward pressure along the channel gradually increased with increase of α ; the maximum pressure at the lower part of the channel increased from 1530 to 1650 Pa. At t_2 , the overall pressure in the channel increased, and the region with pressure larger than 1600 Pa was obviously larger than that at t_1 . The reason was that the copper plate and rim exerted a larger compressive force on the mold–strand channel during downward motion of the mold, which resulted in increased pressure from t_1 to t_2 . In addition, α did seem to have lesser effect on the pressure at the upper part and further away from the channel entrance during the oscillation cycle.

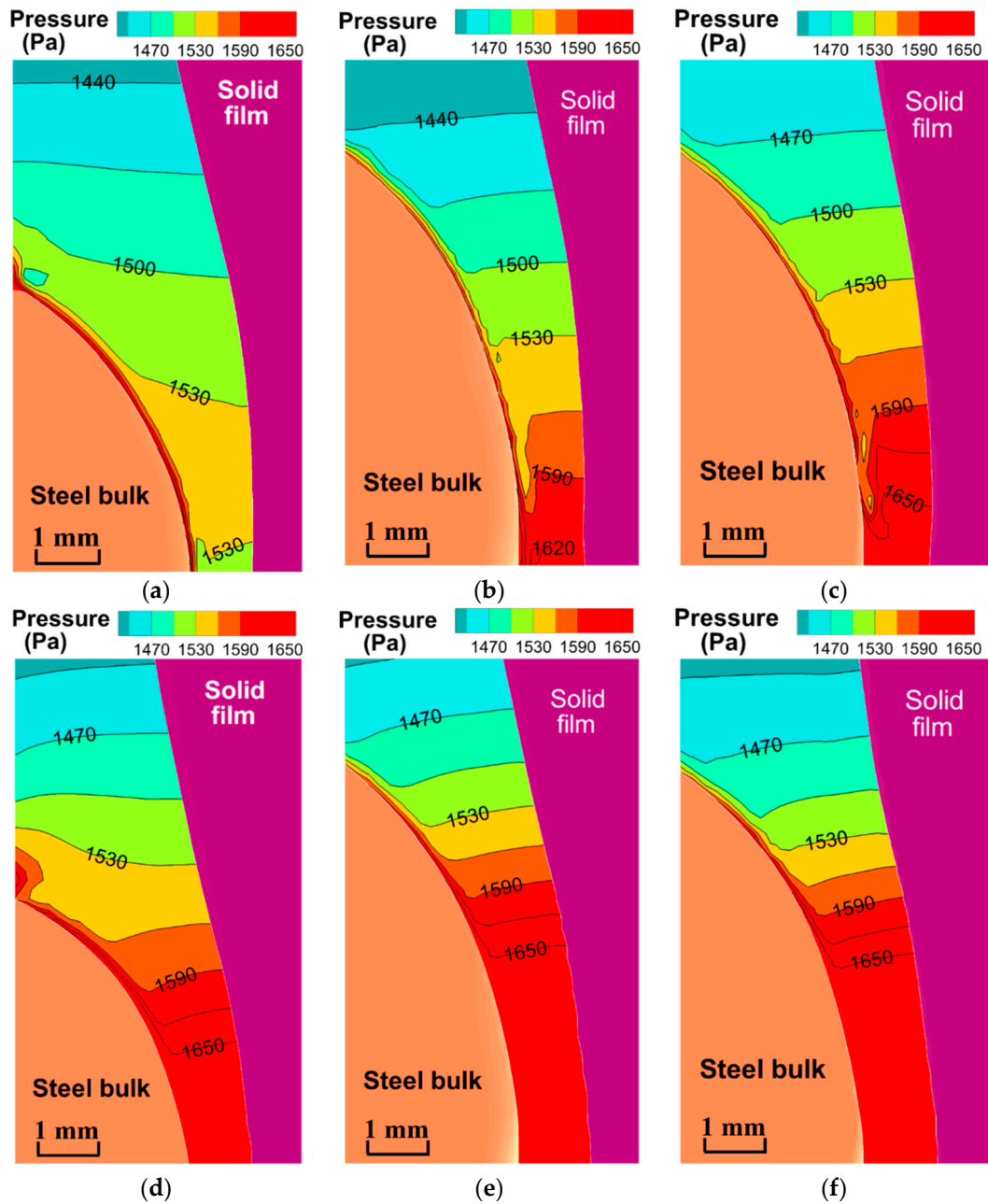


Figure 5. Distribution of pressure in the slag channel: (a) t_1 , $\alpha = 0.2$, (b) t_1 , $\alpha = 0.5$, (c) t_1 , $\alpha = 0.8$, (d) t_2 , $\alpha = 0.2$, (e) t_2 , $\alpha = 0.5$, and (f) t_2 , $\alpha = 0.8$.

3.2. Liquid Slag Film Thickness

Lubrication is closely related to liquid film thickness (d_1). To clarify the effect of nonsinusoidal oscillation, the variations of d_1 at 100 and 400 mm below the meniscus were traced, as indicated in Figure 6. The colored band in the graph represents the NSP. d_1 changed periodically with the mold oscillation: as α increased from 0.2 to 0.8, the fluctuation of d_1 became larger during t_{1v} at locations both 100 and 400 mm below the meniscus. The calculated average d_1 showed no differences for the three cases, being 0.35 and 0.13 mm at the positions of 100 and 400 mm, respectively. To evaluate the stability of the liquid film during mold oscillation, the method of standard deviation was applied. The comparison in Figure 7 revealed that there was a relatively steady variation of transient d_1 when the modification ratio was 0.5.

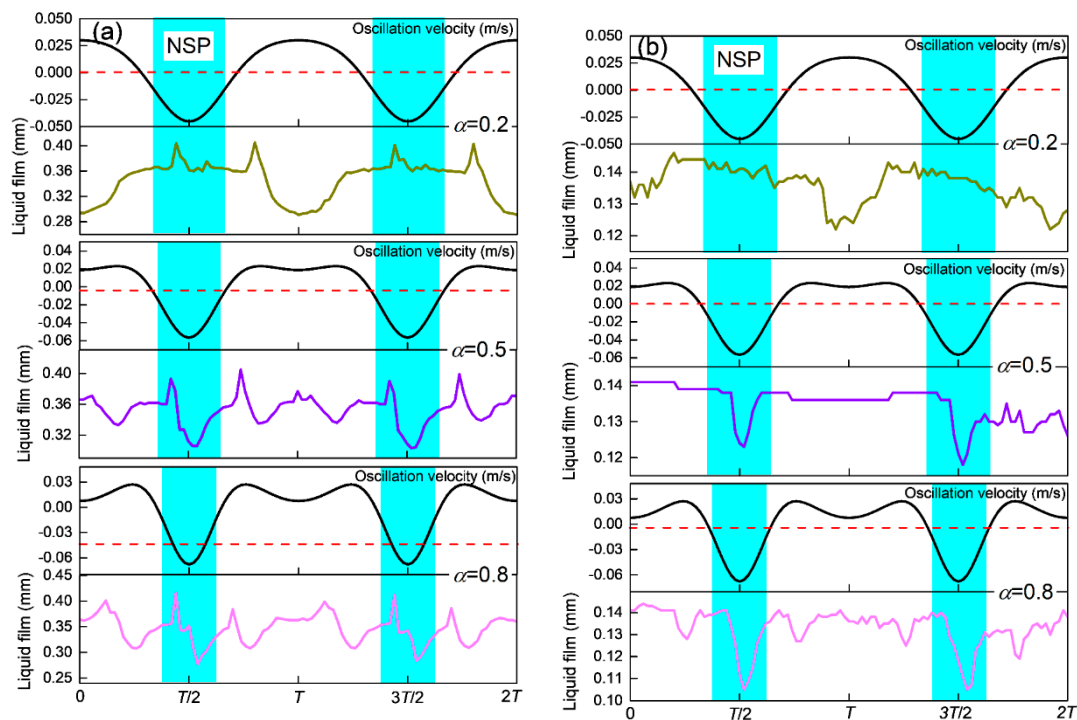


Figure 6. Effect of nonsinusoidal oscillation on the thickness of liquid film at different positions below the meniscus: (a) 100 mm and (b) 400 mm.

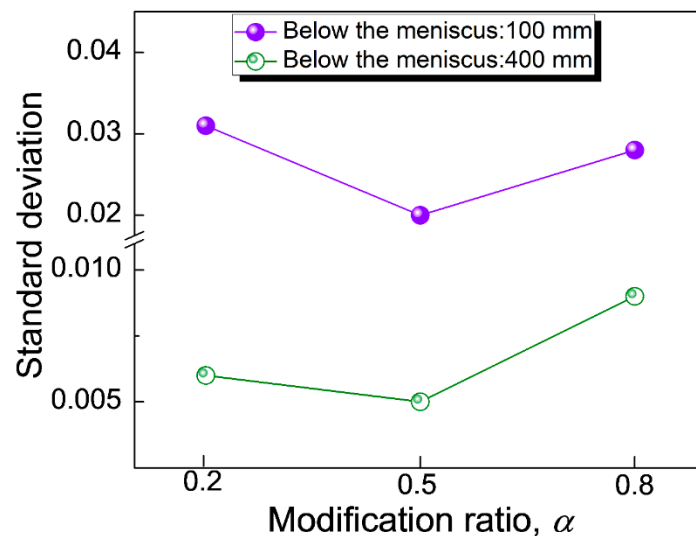


Figure 7. Standard deviation of liquid film thickness with different modification ratios.

3.3. Slag Consumption

Slag consumption (Q_s) stems from liquid slag infiltration into the mold–strand gap and its steady consumption with strand withdrawal [8,9,19,23,24]. A quantitative method to calculate Q_s , which is represented by the slag consumption per unit area of cast slab surface (in kg/m^2), is outlined in our previous work [25]. Figure 8 shows the variations of slag consumption with oscillation cycle for different α . The evolutions of Q_s also presented a periodically analogous fluctuation with the mold reciprocation. At the beginning of t_p , Q_s had less fluctuation; this then persistently decreased from the later part of t_p and reached its lowest value at the middle of t_n . As α increased from 0.2 to 0.5 to 0.8, the minima were 0.15, 0.06, and 0.05 kg/m^2 , respectively. Q_s then incessantly increased until late in the cycle of the next t_p . The fluctuation of Q_s increased as α increased during

t_n . The maximum Q_s values that appearing during the t_p were 0.35, 0.37, and 0.35 kg/m^2 for α of 0.2, 0.5, and 0.8, respectively. The calculated average Q_s for three cases were approximately 0.278, 0.286, and 0.279 kg/m^2 , respectively. In the current study, the Q_s of the nonsinusoidal mode were higher than that of sinusoidal mode, which had Q_s of 0.274 kg/m^2 [25].

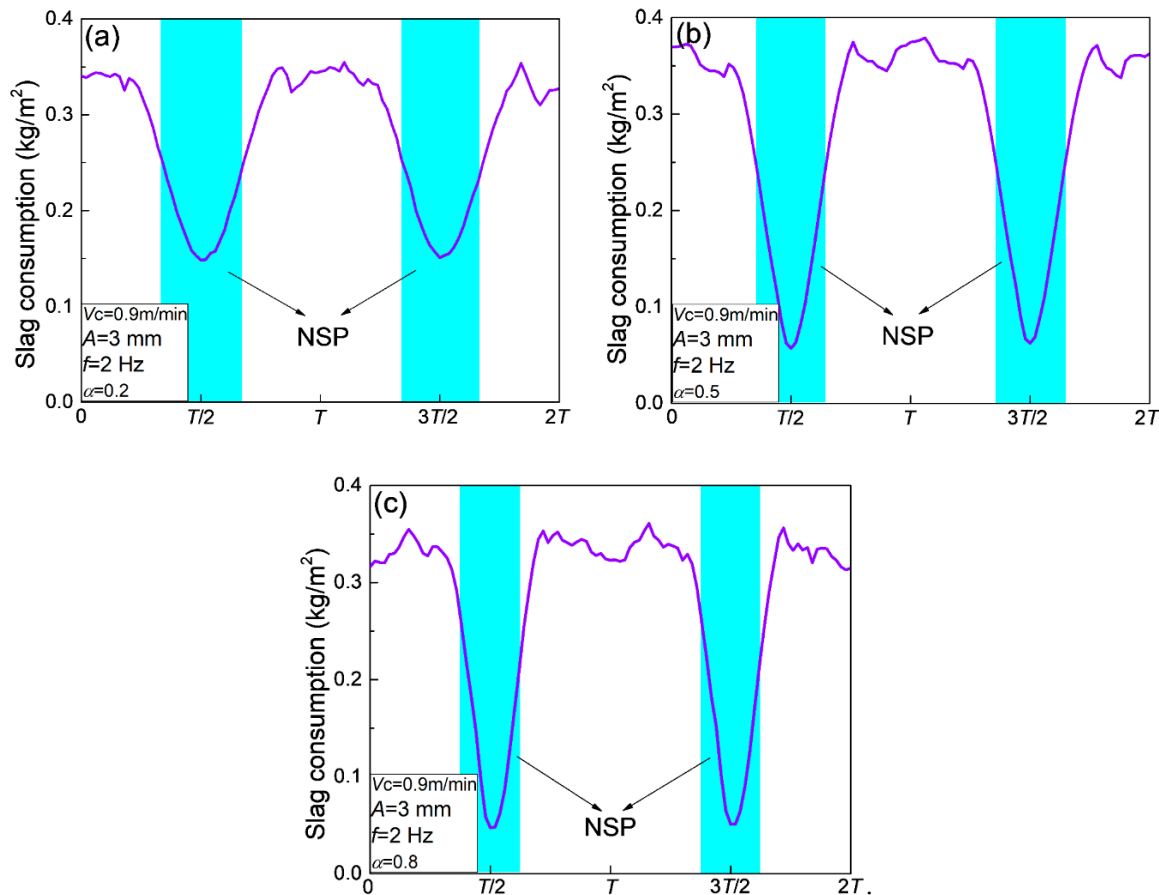


Figure 8. Variations of slag consumption of nonsinusoidal oscillation with different modification ratios: (a) $\alpha = 0.2$, (b) $\alpha = 0.5$, and (c) $\alpha = 0.8$.

Actually, the periodic fluctuation of slag film thickness is closely related to the transient variation of slag consumption during mold oscillation, which also has been reported by Lopez et al. [26]. If the variation of slag film causes violent fluctuation on the local heat flux, some defects, such as cracks, may be generated on the strand surface.

3.4. Heat Flux and Steel Solidification at Meniscus

The formation of subsurface hooks is strongly linked to initial shell solidification and growth in the vicinity of the meniscus during continuous casting of steel [27]. The growth of the shell tip with mold oscillation was investigated under conditions of different α . The vertical proximity of the shell tip to the root of the meniscus shell was expressed as d_m , as indicated in Figure 9a: the case of $\alpha = 0$ corresponds to sinusoidal mode. A greater d_m signifies a greater separation distance between the shell tip and root of the meniscus, meaning that the initial shell growth is more robust. In Figure 9b, nine positions, P_1 to P_9 , on the mold displacement curve were selected to investigate the variations of transient heat flux at 3 mm below the initial meniscus and d_m with mold oscillation; P_5 , P_6 , and P_7 were located in t_n . The predicted results of transient heat flux and d_m are plotted in Figure 10.

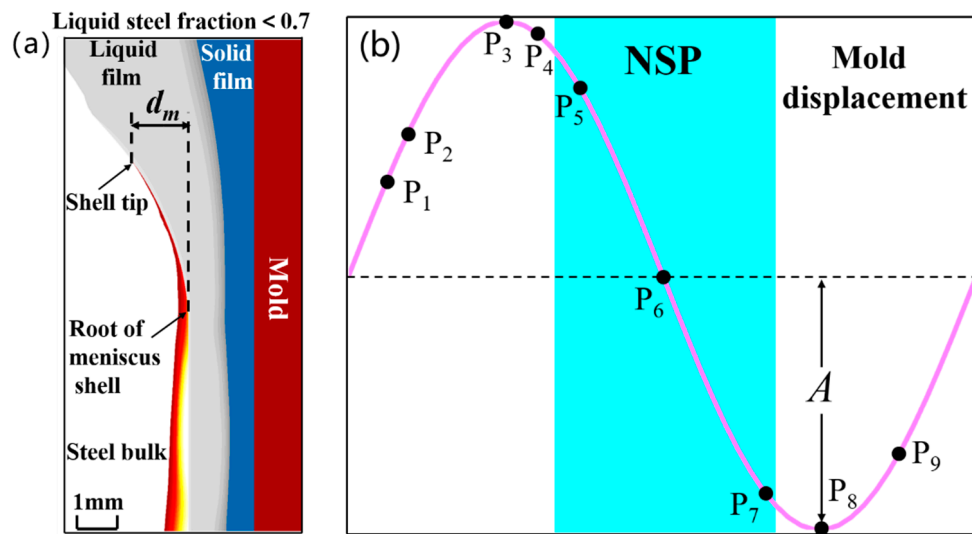


Figure 9. Schematic of (a) solidified shell tip at meniscus and (b) mold displacement.

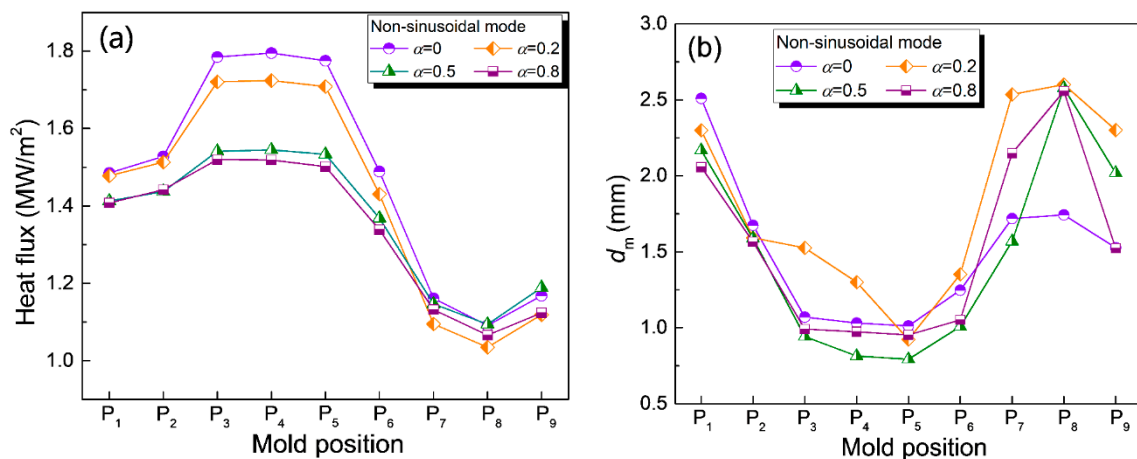


Figure 10. Variations of (a) transient heat flux at 3 mm below the meniscus. (b) d_m during mold oscillation with different modification ratios.

Figure 10 shows that the changing trend of transient heat flux and d_m were more or less coincident in the four cases of α . Moreover, it was found that the heat flux kept an increasing trend, while d_m had a significant reduction when the mold ascended from P_1 to the highest position P_3 ; it revealed that there was absence of steel growth during the period. Subsequently, the mold descended from the highest position to P_5 with a smaller range of motion, there was a slight decrease in heat flux; in the case of $\alpha = 0.2$, d_m obviously decreased, yet only slightly decreased in the other three conditions. The mold continuously oscillated downward from the early part of t_n via the remainder of t_n (P_5 to P_8) and the heat flux decreased sharply; while the d_m continuously increased. Especially, d_m was significantly enhanced during the second half of t_n (P_6 to P_7), and arrived at the peak value at P_8 for the four cases, meaning the meniscus level tends to grow to the molten steel side, then decreased as the mold ascended. It may be speculated that rapid shell growth appeared when the mold was descending, maximum solidification occurred dominantly in the period between the late part of t_n and early part of the next t_p , and there was no growth of the shell during the mold ascension, which is consistent with previous studies [22,26,28]. Actually, it was generally believed that an increased heat flux was beneficial to the growth of initial solidified shell; but, from the above results, it indicates that the formation of initial shell was not only affected by the heat flux, but also by the infiltration of local liquid slag; the pressure driven by slag rim; and the mold oscillation.

For the case of $\alpha = 0$, the average heat flux and d_m at 3 mm below the meniscus were 1.48 MW/m² and 1.5 mm in a single oscillation cycle, respectively. The obtained results have a good agreement with the reported values by Zhang et al. [29,30], which indicated the accuracy of the established model in the study. In addition, the heat flux fluctuations near the meniscus of nonsinusoidal oscillation were significantly smaller than those of sinusoidal oscillation, and the less fluctuations of heat flux is more favorable to the uniform growth of shell. The case with α of 0.5 had a lower value of d_m during the process of the mold descending (P₃ to P₇) and thus its initial shell growth was inferior to that of other cases. Robust growth of the shell tip toward the meniscus is vulnerable to increasing incidences of inclusion and bubble entrapment by the hook [26,27,31]. Consequently, the choice of α can influence the growth of the initial shell at the meniscus: a value of 0.5 is recommended.

It is noteworthy that there is no unified reference standard to choose α . The liquid slag infiltration at different moments changes with the variation of α , which will cause the slag consumption and pressure in the channel to change, further affects the initial shell solidification and growth near the meniscus. For example, the formation of subsurface hooks is related to the initial shell growth near the meniscus during continuous casting of ultralow carbon steel, the hook is prone to gather large inclusions and pose greater effect to the quality of slabs; thus, the effect of α on the growth of shell tip is mainly focused in this case. In addition, the lubrication is particularly critical in the continuous casting of high carbon steel grades, so it is necessary to pay great attention to the effect of α on slag consumption and liquid slag film. Reference standard varies with the change of steel grades and operation conditions.

4. Conclusions

The influence of nonsinusoidal oscillation with different modification ratios on slag infiltration and initial shell growth at the meniscus in slab continuous casting was investigated by employing a two-dimensional multiphase model. The conclusions are outlined as follows.

- (1) Liquid slag infiltrates the mouth of the mold–strand channel, mainly accompanied by even distribution of velocity during t_p . At the middle of t_n , by the action of the copper plate and solid rim, a large amount of liquid slag reflowed into the slag pool. The phenomenon became more severe with an increase of α . Simultaneously, the pressure at the lower part of the meniscus increased dramatically.
- (2) α had no obvious effect on the average thickness of the liquid film at 100 and 400 mm below the meniscus, while α of 0.5 had less fluctuation of the transient liquid film.
- (3) As α increased from 0.2 to 0.5 to 0.8, the average slag consumptions were 0.278, 0.286, and 0.279 kg/m², respectively. Fluctuation of slag consumption increased as α increased during t_n , and the maximum value appearing during t_p . Combining with the flow characteristics of the liquid slag, the slag consumption could be increased by appropriately broadening t_p .
- (4) Shell solidification and growth occurred dominantly in the period that the mold descended and there was little shell growth when the mold was ascending. A α of 0.5 is recommended because the initial shell tip is least robust at the meniscus, which is favorable for preventing the entrapment of inclusions and bubbles and reducing the formation of defects.

Author Contributions: X.Y., Q.W. (Qiangqiang Wang), S.H., and Q.W. (Qian Wang) conceived and designed the numerical simulation; X.Y., and B.J. conducted the simulation and analyzed the simulation results; X.Y. and Q.W. (Qiangqiang Wang) wrote the paper.

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Conflicts of Interest: The authors declare no conflict of interest.

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