

Article **Examining the Optimal Use of WBG Devices in Induction Cookers**

Ahmet Erken [*](https://orcid.org/0000-0002-7047-7651) and Atiye Hulya Obdan

Department of Electrical Engineering, Yildiz Technical University, Istanbul 34710, Turkey; obdan@yildiz.edu.tr ***** Correspondence: ahmeterken97@gmail.com

Abstract: Modern induction cookers have started to demand challenging features such as slim design, high power ratings, high performance, and silence. All those requirements are directly related to the power semiconductors used in power converters. Si (silicon)-based power semiconductors are not capable of answering those demands because of strict operating conditions, such as high ambient temperatures. Therefore, WBG (Wide Band Gap) power semiconductors have been getting attention. In this study, WBG power semiconductors will be compared with Si-based IGBT (Insulated Gate Bipolar Transistor) under different operating conditions. The best option to use WBG power semiconductors in modern induction cookers will be analyzed. The performance of a series-resonant half-bridge converter was evaluated under various operating conditions. Measurements were obtained from the real operating conditions of induction hobs. The switching frequency is changed from 20 kHz to 100 kHz, while the power rating is increased to 3.7 kW. In addition to traditional 4-zone induction cooktops, this discussion also provides a comprehensive analysis of high-segment, fully flexible induction cooktops. While the IGBT-based design exhibits 25.79 W power loss per device, the WBG device exhibits 6.87 W in the maximum power condition of conventional induction cooker operation. When it comes to high-frequency operation, the WBG power device exhibits 10.05 W at 95 kHz. Total power loss is still well below that of the IGBT-based conventional design. Appropriate usage of WBG power semiconductors in modern induction cookers can exploit many more benefits than Si-based designs.

Keywords: induction cooking; wide band gap devices; resonant converters

1. Introduction

Induction cooking applications have been drawing attention due to their superior performance, such as fast heating, efficiency, controllability, cleanness, safety, and lower carbon emissions, for a long time. The working principle of an induction cooktop is based on Faraday's Law. It produces a high-frequency magnetic field with the help of a power electronics converter and an induction coil, and then this magnetic field induces eddy currents directly beneath the ferromagnetic pan. As a result of this process, joule and hysteresis losses heat up the pan [\[1\]](#page-25-0). The basic building block is shown in Figure [1.](#page-1-0)

Meanwhile, there are some criteria that define the performance of an induction cooktop. High zone power ratings, high performance, total height of the product, and silence are the most prominent ones. These criteria are directly related to power semiconductor switch losses. All the commercialized induction cookers have been using IGBTs for a long time. There are different types of IGBT technologies, some of which are directly produced for resonant applications. IGBTs can be preferred thanks to their low saturation voltage (*VCEsat*), which results in low conduction loss; however, they have limited switching capacity because of the tail current they have during turn-off. Most modern induction cooktops operate between 18 kHz and 50 kHz, and their resonance frequency is between 18 kHz and 20 kHz [\[2](#page-25-1)[–4\]](#page-25-2).

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Figure 1. Basic building block of domestic induction heating systems.

Figure 1. Basic building block of domestic induction heating systems. WBG power semiconductors are applied to domestic and industrial induction heating applications. WBG power semiconductors are evaluated in different power electronic systems and compared with Si-based designs in [\[5\]](#page-25-3), while Si-based switches are compared
in the compared with Si-based designs in [5], while Si-based switches are compared with WBG power switches in [0]. There is also a variety of research that is uncelly related
to induction cookers. Si IGBT, GaN HEMT (Gallium Nitride High Electron Mobility Transistor), and SiC MOSFET (Silicon Carbide Metal Oxide Semiconductor Field Effect Transistor), and the integral (cincent can but them charge connectionated their lines.
Transistor) are compared in [\[7\]](#page-25-5) for a 2.0 kW power rating. Refs. [\[8](#page-25-6)[,9\]](#page-26-0) compared SiC mateliers, are computed in [1] for a 2.6 km power raing. These [0], computed site
MOSFET and SiC JFET (Junction Field Effect Transistor) in terms of power losses. In these works, power ratings range from 200 W to 1800 W, while switching frequencies change between 45 kHz and 125 kHz. Ref. [\[10\]](#page-26-1) compares normally-on SiC JFET and Si IGBT in a series resonant half-bridge converter at 2.4 kW power rating up to 500 kHz switching frequency. All SiC power semiconductor technologies are tested and evaluated for induction cookers in [11]. Normally-on and normally-off SiC JFETs, SiC BJT (Bipolar Junction Transistor), and SiC MOSFETs are tested and compared from different perspectives. SiC BJT power switches are evaluated for a new ZCS (Zero Current Switching) converter in [\[12](#page-26-3)[,13\]](#page-26-4). Although most of the research focuses on series-resonant half-bridge converters, there are also papers related to single-ended quasi-resonant converters. Refs. [\[14–](#page-26-5)[16\]](#page-26-6) apply SiC power switches to single-switch resonant converters. WBG devices enable us to configure induction cooktops in different ways, which are hard to design with Si-based
 \overline{S} power semiconductors. Refs. [\[17](#page-26-7)[–19\]](#page-26-8) use GaN HEMT power switches and design full-flexi

in the state of power switches and design full-flexi power ratings range from 200 W to 1800 W, while switching frequencies change between high-segment induction cooktops. Ref. [\[17\]](#page-26-7) uses GaN HEMT in 2 MHz switching frequency and loads power up to 15 A. It also considers thermal perspective and layout design.
Ref. [12] eleberates on full flori industion seekers. It simulates 200 W lead november. rest ₁₂₀ can overter on tail held interested converts. It emittated converts to 101 kHz to 500 kHz switching frequencies ranging from 100 kHz to 500 kHz. Ref. [\[19\]](#page-26-8) implements GIT All SiC power semiconductor technologies are tested and evaluated for induction cookers (Gate Injected Transistor) GaN HEMT technology in induction cookers at 2.2 kW power and 50 kHz–100 kHz switching frequencies. There are different research papers about WBG power semiconductors that show that with WBG power switches in [\[6\]](#page-25-4). There is also a variety of research that is directly related Ref. [\[18\]](#page-26-9) elaborates on full-flexi induction cookers. It simulates 800 W load power for

A series resonant half-bridge converter is evaluated at different operating conditions. Measurements are inspired by real induction cooker operating conditions. The power rating is increased up to 3.7 kW, while the switching frequency ranges from 20 kHz to 100 kHz. Apart from traditional 4-zone induction cookers, high-segment full-flexi induction cookers are also elaborated in detail. To show the benefits of WBG device performance, WBG power devices under power ratings range from 0.3 kW to 1 kW while switching frequencies range from 265 kHz to 1 MHz.

The objectives of this research can be summarized as follows:

• The proper power semiconductor selection criteria for domestic induction cooktops elaborates on full simulates on full simulates 800 W load power for different powe

- The benefits of using WBG in domestic induction under different operations in comparison with Si-based IGBT are examined.
- The power losses are analyzed for each specific working condition. Thermal and electrical measurements are taken.
- The proper conditions to switch from Si-based conventional design to WBG-based state-of-the-art design are researched.

2. Power Semiconductor Selection for Series Resonant Half-Bridge Converter

2.1. Operating Conditions for Series Resonant Half-Bridge Converter

To determine the performance of a power semiconductor, there are two significant operating conditions in an induction cooktop: In operation 1, the power converter is working at its maximum load power and minimum switching frequency, whereas in operation 2, it is working at a lower load power and a higher switching frequency. In this section, these operating conditions are analyzed in detail to determine the proper power semiconductor selection.

2.1.1. Operating Condition 1: Maximum Load Power—Minimum Switching Frequency

Condition 1 is the maximum load power condition where the switching frequency is so close to the resonant frequency, thus switching losses are mostly dominated by conduction losses. As can be seen from the waveforms in Figure [2a](#page-3-0),b, the turn-off current is nearly zero, thus switching losses are negligible. Because of the snubber capacitors, the diode region does not occur. As a result, total loss is mostly dominated by conduction loss.

2.1.2. Operating Condition 2: Lower Load Power—Higher Switching Frequency

In this condition, the switching frequency is increased to reduce load power. When the load power is decreased, the load current decreases; therefore, conduction loss will be lower than in Operating Condition 1. Switching losses are higher than in Operating Condition 1 because of increased frequency and a higher turn-off current. The diode region occurs obviously due to the operation in the inductive region. Waveforms are shown in Figure [3a](#page-4-0),b. The power losses are dominated by conduction losses; however, switching and diode losses are also effective on converter performance.

The major electrical parameters for the two operating conditions are listed in Table [1.](#page-2-0)

Table 1. Operating conditions fundamental parameters.

Figure 2. Operating condition-1 waveforms: (a) 4 ms/div; (b) 20 µs/div. Yellow waveform: gate drive signal, blue waveform: IGBT V_{CE} voltage, red waveform: IGBT I_C current measured by Rogowski coil, green waveform: induction coil current, purple waveform (math2): IGBT current without Rogowski Rogowski offset, orange waveform: IGBT power loss. offset, orange waveform: IGBT power loss.

and diode losses are also effective on converter performance.

Figure 3. Operating condition-2 waveforms: (a) 4 ms/div; (b) 20 µs/div. Yellow waveform: gate drive signal, blue waveform: IGBT V_{CE} voltage, red waveform: IGBT I_C current measured by Rogowski coil, green waveform: induction coil current, purple waveform (math2): IGBT current without Rogowski

offset, orange waveform: IGBT power loss.

2.2. Si-Based Power Semiconductor Selection

Modern induction cookers prefer Si-based IGBTs thanks to their low saturation voltages (*VCEsat*) and moderate switching capacities, which are limited due to tail current phenomena occurring during turn-off. As can be seen from the operating conditions explained in the previous sections, conduction loss is one of the most important factors affecting total losses. That is the reason IGBTs are preferred in this application. There are plenty of manufacturers that produce Si-based IGBTs for half-bridge converters. 600–650 V and 40–50 A IGBTs are mostly used in series resonant half-bridge converters. This section tries to find out the most suitable IGBT by comparing their performances with selected WBG devices.

The datasheet parameters are used preliminarily to compare IGBTs. The first parameter is the saturation voltage. Figure [4a](#page-5-0),b show saturation voltages of IGBTs for different junction temperatures. The second parameter is the diode forward voltage. Figure [5a](#page-6-0),b show forward voltage drops for different junction temperatures. As mentioned above, conduction loss is the major contributor to total switch loss. Therefore, $V_{\mathsf{CE}_{sat}}$ is the most crucial parameter to determine IGBT.

Figure 4. IGBT saturation voltages at different junction temperatures: (**a**) IGBT ாೞೌ voltages at 25 **Figure 4.** IGBT saturation voltages at different junction temperatures: (**a**) IGBT *V_{CE_{sat}* voltages at \bullet 7.25 °C in the saturation of \bullet 7.25 °C in the saturation of \bullet 7.25 °C in the saturation of \bullet 7.25 °C} ²⁵ ◦C junction temperature; (**b**) IGBT *^VCEsat* voltages at 175 ◦C junction temperature.

Appl. Sci. **2023**, *13*, x FOR PEER REVIEW 8 of 29

Figure 5. Diode ி voltages at different junction temperatures: (**a**) Diode ி voltages at 25 °C junc‐ **Figure 5.** Diode V_F voltages at different junction temperatures: (**a**) Diode V_F voltages at 25 °C junction temperature; (**b**) Diode V_F voltages at 175 °C junction temperature.

When *V*_{*CEsat*} − *I*_C characteristics are compared at different junction temperatures, Infineon's IHW50N65R6 and Onsemi's FGHL75T65MQDT IGBTs are suitable for highpower applications. However, IHW50N65R6 is selected for comparison with the WBG devices since this IGBT is specifically produced for induction heating applications and $\frac{1}{\sqrt{1-\frac{1$ is preferable both in terms of cost and technical specifications. When comparing $V_F - I_F$ characteristics that are at different junction temperatures, IHW50N65R6 is not the best option to choose; however, diode conduction loss is a small portion of the total conduction losses, hence making IHW5065R6 the best selection for this application. IHW50N65R6 has Reverse Conduction IGBT (RC IGBT) technology, which integrates the body diode into the IGBT die so it only uses one die. This is advantageous in terms of manufacturing, cost, packaging, and EMI.

2.3. WBG-Based Power Semiconductors Selection

Wide-band gap power semiconductors have been popular for modern power electronics applications such as EV (Electrical Vehicle) charges, renewable energy systems, traction inverters, PFC (Power Factor Correction) circuits, and motor drivers. While the requirements of modern systems have been getting more challenging, Si-based power semiconductors, which are already within their theoretical limits, are not able to live up to those demands. The advantageous characteristics of wide band gap power semiconductors, such as high PCB (Printed Circuit Board) density, lack of bulky heatsinks, and cooling fans, are just a few of them. As Si-based power semiconductors get closer to their theoretical limits, new searches focus on wide band gap semiconductors. Table [2](#page-7-0) compares the basic chemical characteristics of Si and WBG semiconductors.

Table 2. Semiconductor Material Comparison.

In series resonant half-bridge converters, the maximum voltage stress of power switches is 325 V. Therefore, a power semiconductor whose voltage rating is 650 V can be selected. To compare with Si-based power semiconductors, GS66516B from GaN Systems is selected in order to examine the usage of WBG power semiconductors in domestic induction heating applications. It can switch on and off at tremendous speeds that Si-based devices cannot reach. Its voltage strength is 650 V, which is very well suited for gridconnected series resonant half-bridge converters. The electrical characteristics of selected power semiconductors are shown in Figure [6a](#page-8-0)–c.

Figure 6. *Cont*.

Figure 6. Characteristics of selected power semiconductors for domestic induction heating application: (**a**) IHW50N65R6 IGBT *VCEsat* characteristics for different junction temperatures; (**b**) GS66516B *RDSon* characteristics for different junction temperatures; (**c**) Reverse conduction characteristics for both.

3. Experimental Results

The WBG power device is tested at different operating conditions to find out the optimum operating conditions to use WBG power semiconductors properly. First, the WBG power semiconductors are operated in conventional domestic induction cooking conditions and analyzed at high power and low switching frequencies. Secondly, WBG power semiconductors are analyzed by operating at high switching frequencies with the same zone powers as conventional induction cooktops. Finally, WBG power semiconductors operate in high-segment full-flexi induction cooktops and are analyzed for different switching frequencies and powers. At the end of the measurement results, advantages and disadvantages are listed. When and how to use this new generation of power semiconductors in domestic induction cooktops is elaborated in detail. Figure [7](#page-9-0) shows the roadmap for how to integrate WBG devices into domestic induction cooktops.

conductors in domestic induction cooktops is elaborated in detail. Figure 7 shows the

 $\frac{1}{2}$ systems GRA systems GRA systems GRA systems $\frac{1}{2}$ is chosen to compute the WBG power semiconductor with the Si-based IGBT. This board is specifically designed for high-power applications;
with the Si-based IGBT. This board is specifically designed for high-power applications; hence, it contains two GS66516B GaN HEMTs in parallel. Its PCB structure is designed as an IMS (Insulated Material Board). The power stages are shown in Figure [8a](#page-10-0)–c. GaN Systems GSP65RxxHB-EVB is chosen to compare the WBG power semiconductor

Figure 8. *Cont*.

 $\overline{}$, and $\overline{}$ are $\overline{}$ and $\overline{}$ and $\overline{}$

Figure 8. Power sections are used in measurements. (a) Line filter; (b) Resonance Converter; (c) Gate driver circuitry block diagram. driver circuitry block diagram.

While all thermal measurements are taken with Fluke Ti480, all oscilloscope meaurements are taken by TELEDYNE Lecroy HDO6054. To prevent power devices from a surements are taken by TELEDYNE Lecroy HDO6054. To prevent power devices from a thermal runaway, a cooling fan is used. While its rated voltage is 12 V DC, it is used in a thermal runaway, a cooling fan is used. While its rated voltage is 12 V DC, it is used in a 5 V DC condition. 5 V DC condition.

3.1. Si-Based IGBT in Conventional Induction Cooking Operation

In this section, the selected IHW50N65R6 (Infineon) is tested in conventional induction cooking operations. While oscilloscope measurements are shown in Figure [9a](#page-11-0),b thermal measurements are shown in Figure [10a](#page-12-0),b. Power circuit parameters and power losses are shown in Tables [3](#page-10-1) and [4,](#page-10-2) respectively.

	P_{input} [kW]	f_{sw} [kHz]	$R_{eq} [\Omega]$	$\text{Leg}\left[\text{uH}\right]$	C_{res} [nF]	C_{sub} [nF]	$t_{\text{d}t}$ [µs]	Fan Level [V]
Cond. 1	3.70	20.00	2.60	54.00	2×680	2×2.2	1.50	5 V/(12 V)
Cond. 2	2.40	22.00	3.29	52.00	2×680	2×2.2	1.50	5 V/(12 V)

Table 4. Power losses for conventional induction cooking operation (IHW50N65R6).

Figure 9. IHW50N65R6 oscilloscope measurements at conventional induction cooking operations: **Figure 9.** IHW50N65R6 oscilloscope measurements at conventional induction cooking operations: (**a**) Operating condition−1 waveforms; (**b**) Operating condition−2 waveforms. Yellow (CH1) and red (**a**) Operating condition−1 waveforms; (**b**) Operating condition−2 waveforms. Yellow (CH1) and red (CH2) waveforms are low and high side IGBT V_{CE} voltages, respectively; blue waveform (CH3) is coil current; green waveform (CH4) is high side IGBT current; orange waveform (MATH2) is high side IGBT power loss. side IGBT power loss.

Figure 10. *Cont.*
 Example 20. *Cont*.

Figure 10. IHW50N65R6 thermal measurements at conventional induction cooking operation: (**a**) **Figure 10.** IHW50N65R6 thermal measurements at conventional induction cooking operation: (a) Thermal measurements of operating condition 1; (b) Thermal measurements of operating condition 2.

This IGBT is one of the best IGBTs that could be used in domestic induction cooking applications. Therefore, these thermal measurements and power losses refer to WBG power *3.2. WBG Device in Conventional Induction Cooking Operation* semiconductor measurements.

3.2. WBG Device in Conventional Induction Cooking Operation

In this section, the selected GS66516B is tested in conventional induction cooking urements are shown in Figure 12a,b. The power circuit parameters and power losses are operations. While the oscilloscope measurements are shown in Figure [11a](#page-13-0),b, thermal shows these the countries in the countries of the contribution of the state of the contribution of the power circuit parameters and power losses are shown in Tables [5](#page-12-1) and [6,](#page-12-2) respectively. $\overline{}$

	P_{input} [kW]	f_{sw} [kHz]	$R_{eq} [\Omega]$	Leq $[uH]$	C_{res} [nF]	C_{snub} [nF]	t _{deadtime} [µs]	Fan Level [V]
Cond. 1	3.70	19.00	2.60	58.00	2×680	2×2.2	0.50	5V/(12 V)
Cond. 2	2.40	21.50	3.00	54.00	2×680	2×2.2	0.50	5V/(12 V)

Table 5. Power circuit parameters for conventional induction cooking operation (GS66516B).

Table 6. Power losses for conventional induction cooking operation (GS66516B).

Figure 11. GS66516B oscilloscope measurements at conventional induction cooking operation: (a) Operating condition 1 waveforms. (**b**) Operating condition 2 waveforms. Red (CH2) and green (CH4) waveforms are low and high side HEMTs V_{DS} voltages, respectively; blue (CH3) waveform is coil current.

Figure 12. *Cont.*
 $\begin{aligned} \text{Figure 12.} \text{ } & \text{Cont.} \end{aligned}$

Figure 12. GS66516B thermal measurements at conventional induction cooking operation: (a) Thermal mal measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2. measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2.

3.3. WBG for High-Frequency Induction Cooking Conditions 3.3. WBG for High-Frequency Induction Cooking Conditions

As mentioned in the previous sections, the WBG power semiconductor enables us to As mentioned in the previous sections, the WBG power semiconductor enables us to increase switching frequency due to its superior switching performance. In this section, increase switching frequency due to its superior switching performance. In this section, the WBG device is tested at a high switching frequency without sacrificing power ratings. the WBG device is tested at a high switching frequency without sacrificing power ratings. While the oscilloscope measurements are shown in Figure [13a](#page-15-0),b, thermal measurements While the oscilloscope measurements are shown in Figure 13a,b, thermal measurements are shown in Figure [14](#page-16-0)a,b. The power circuit parameters and power losses are shown in are shown in Figure 14a,b. The power circuit parameters and power losses are shown in Table[s 7](#page-14-1) an[d 8](#page-14-2), respectively. Tables 7 and 8, respectively.

Table 8. Power losses for high-frequency induction cooking operations (GS66516B).

Figure 13. GS66516B oscilloscope measurements at high-frequency induction cooking operation: (**a**) **Figure 13.** GS66516B oscilloscope measurements at high-frequency induction cooking operation: Operating condition 1 waveforms; (**b**) Operating condition 2 waveforms. Yellow (CH1) and red (**a**) Operating condition 1 waveforms; (**b**) Operating condition 2 waveforms. Yellow (CH1) and red (CH2) waveforms are low and high side HEMTs V_{DS} voltages respectively, blue (CH3) waveform is coil current. coil current.

Figure 14. *Cont*.

Figure 14. GS66516B thermal measurements at high-frequency induction cooking operation: (**a**) Ther-**Figure 14.** GS66516B thermal measurements at high-frequency induction cooking operation: (**a**) Thermal measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2. mal measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2.

3.4. WBG for All Metal Induction Cooking Operation 3.4. WBG for All Metal Induction Cooking Operation

Most domestic induction cooktops need ferromagnetic pans to heat up. They cannot Most domestic induction cooktops need ferromagnetic pans to heat up. They cannot heat non-ferromagnetic materials such as copper and aluminum because of their low heat non-ferromagnetic materials such as copper and aluminum because of their low equivalent resistance (R_{eq}) and inductance (L_{eq}). To transfer high power ratings (above kW) to non-ferromagnetic pans with modern induction cooktops, coil and switch current 2.3 kW) to non-ferromagnetic pans with modern induction cooktops, coil and switch current ratings increase to levels that Si-based power semiconductors are not able to withstand. ratings increase to levels that Si-based power semiconductors are not able to withstand. These types of pans can be heated up to high power levels by increasing the switching These types of pans can be heated up to high power levels by increasing the switching frequency to increase the equivalent series resistance. WBG power semiconductors can be frequency to increase the equivalent series resistance. WBG power semiconductors can be used in this type of application to increase switching frequency to heat non-ferromagnetic used in this type of application to increase switching frequency to heat non-ferromagnetic materials [20]. While oscilloscope measurements are shown in Figure 15a,b, [the](#page-17-0)rmal measurements are shown in Figure 16a,[b. T](#page-18-0)he power circuit parameters and power losses are shown in Tables 9 a[nd](#page-16-1) 10, [res](#page-16-2)pectively.

Table 9. Power circuit parameters for all-metal induction cooking operation (GS66516B). **Table 9.** Power circuit parameters for all-metal induction cooking operation (GS66516B).

	P_{input} [kW]	f_{sw} [kHz]	$R_{eq} [\Omega]$	Leq $[uH]$	C_{res} [nF]	C_{snub} [nF]	^L deadtime $[\mu s]$	Fan Level [V]
Opt. 1	2.30	100.00	1.87	17.00	2×94	2×2.2	$0.50\,$	5 V/(12 V)
Opt. 2	1.50	105.00	1.99	17.00	2×94	2×2.2	$0.50\,$	5 V/(12 V)

Table 10. Power losses for all-metal induction cooking operations (GS66516B).

Figure 15. GS66516B oscilloscope measurements at all-metal induction cooking operation: (a) Operating condition 1 waveforms; (b) Operating condition 2 waveforms. Yellow (CH1) and red (CH2) waveforms are low and high side HEMTs V_{DS} voltages, respectively; blue (CH3) waveform is coil current.

18 of 27

Figure 16. *Cont*.

Figure 16. GS66516B thermal measurements at all-metal induction cooking operation: (**a**) Thermal **Figure 16.** GS66516B thermal measurements at all-metal induction cooking operation: (**a**) Thermal measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2. measurements of operating condition 1; (**b**) Thermal measurements of operating condition 2.

3.5. WBG for Full-Flexi Operation 3.5. WBG for Full-Flexi Operation

The flexi induction cooktops are high-segment induction cookers that can heat every The flexi induction cooktops are high-segment induction cookers that can heat every section of the hob without specific zones. These types of cooktops consist of multiple inverters and induction coils with low power ratings. In this section, operating conditions that could be used in flexi applications are covered. Figur[e 14](#page-16-0) shows waveforms at different operating conditions. The thermal measurements are shown in F[igu](#page-17-0)re 15. All power losses and operating conditions are shown in F[igu](#page-18-0)re 16. While the oscilloscope measurements are shown in [Fig](#page-20-0)ure 17a–e, thermal measurements are shown in [Figu](#page-22-0)re 18a–e. The power circuit parameters and power losses are shown in [Tab](#page-18-1)les [11](#page-18-2) and 12, respectively.

	P_{input} [kW]	f_{sw} [kHz]	$R_{eq} [\Omega]$	Leq [uH]	C_{res} [nF]	C_{snub} [nF]	t _{deadtime} [µs]	Fan Level [V]
Opt. 1	0.87	265.00	8.53	20.00	2×11	2×0.470	0.20	0 V/(12 V)
Opt. 2	0.53	295.00	14.00	18.50	2×11	2×0.470	0.20	0 V/(12 V)
Opt. 3	0.30	500.00	20.00	15.00	2×11	2×0.470	0.20	5 V/(12 V)
Opt. 4	1.00	625.00	5.91	4.60	2×11	2×0.470	0.20	5 V/(12 V)
Opt. 5	0.40	1000.00	8.90	4.80	2×4.7	2×0.470	0.20	5 V/(12 V)

Table 11. Power circuit parameters for full-flexi induction cooking operations (GS66516B). **Table 11.** Power circuit parameters for full-flexi induction cooking operations (GS66516B).

Table 12. Power losses for full-flexi induction cooking operations (GS66516B).

	P_{cond} [W]	P_{sw} [W]	P_{fw} [W]
Opt. 1	0.38	1.86	2.20
Opt. 2	0.14	2.06	2.18
Opt. 3	0.04	3.45	3.46
Opt. 4	0.58	4.43	5.45
Opt. 5	0.17	6.98	7.36

Figure 17. *Cont*.

Figure 17. GS66516B oscilloscope measurements at full-flexi induction cooking operation (a) Operating condition 1 waveforms; (b) Operating condition 2 waveforms; (c) Operating condition 3 waveforms; (d) Operating condition 4 waveforms; (e) Operating condition 5 waveforms. Yellow (CH1) and red (CH2) waveforms are low and high side HEMTs V_{DS} voltages, respectively; blue (CH3) waveform is coil current. waveform is coil current. waveform is coil current. μ waveforms are low and high side HEMTs $\rm{v_{DS}}$ voltages, respectively; blue (CH3)

Figure 18. *Cont*.

IEMT

HEMT

HFMT4 45

45

Figure 18. *Cont*.

 48.4

46.8

 45.2

 43.6

 41.9

Figure 18. GS66516B thermal measurements at full-flexi induction cooking operation: (a) Operatcondition 1; (**b**) Operating condition 2; (**c**) Operating condition 3; (**d**) Operating condition 4; (**e**) Oping condition 1; (**b**) Operating condition 2; (**c**) Operating condition 3; (**d**) Operating condition 4; (**e**) Operating condition 5.

4. Discussion

In this study, the application of WBG power semiconductors in domestic induction In this study, the application of WBG power semiconductors in domestic induction ϵ is in the processes is in verse power switches have been tested under different working. cookers is investigated. WBG power switches have been tested under different working
it is in the studies show in the conditions. All measurements are summarized in Table [13.](#page-22-1) The results of the studies show
characteristics conductivity of the studies show that WBG switches have very reasonable conduction characteristics compared to their Si counterparts. Measurement results are shown in Figure [19.](#page-23-0) Conduction losses are quite dominant in domestic induction heating topologies, so a much better conduction characteristic can be achieved by connecting two or more switches in parallel. Thus, much better product performance can be achieved. Increasing the operating frequency to very high levels compared to conventional operating conditions makes the switching characteristics more important. As can be seen from Figure 20, the WBG semiconductor shows many times better switching characteristics. Therefore, it is much easier to reach high switching frequencies than Si-based IGBTs. With a suitable coil design, performance improvement can be achieved by minimizing switching losses, especially at high frequencies. Coil design is beyond the scope of this study. In the case of full-flexi operation, very high switching frequencies make reverse conduction losses much more important. Measurement results are shown in Figure [21.](#page-24-0) The reverse-conduction characteristics of WBG switches are poor. $t_{\rm max}$ through through the channel. In this way, losses can be additionally minimized. With a summary minimized $\mu_{\rm max}$ Therefore, the reverse conduction region should be kept very short so that the current appropriate coil design, the duration of the free-wheeling region can be further minimized. flows through the channel. In this way, losses can be additionally minimized. With an

[kW] fsw [kHz] Req [Ω] Leq

Pinput

[uH] Cres [nF] Csnub [nF] tdt [μs] Fan Level

Figure 20. All condition 2 measurements. **Figure 20.** All condition 2 measurements.

[V] Pcond [W] Psw

Figure 21. All full‐flexi measurements. **Figure 21.** All full-flexi measurements.

5. Conclusions

In this study, the optimal use of \mathbf{MBC} power devices in domestic induction heating In this study, the optimal use of WBG power devices in domestic induction heating in this study, the optimal use of WBG power devices in domestic induction heating applications is examined. GaN HEMT is tested for different operating conditions to find optimum operating conditions and tried to answer "When it makes sense to switch Si-based IGBTs to WBG power semiconductors". The first step is to use WBG power semiconductors in conventional domestic induction heating conditions. In this condition, the power rating is high and the switching frequency is low; therefore, the main contributor to total power loss is conduction loss. A WBG power semiconductor whose on-state resistance is so low that its conduction loss is well below Si-based IGBTs can outperform. However, a discrete power semiconductor with lower on-state resistance than IGBT can cost too much. Using two or more switches in parallel is another solution, but this is not cost-effective either. Potential EMI problems are another issue to deal with because of the high dv/dt and di/dt ratings. As a result, the fact that a WBG power semi-conductor operates in standard domestic induction heating conditions does not make sense in terms of the total product.

The second step is to use WBG power semiconductors in high-frequency applications with the same zone power as conventional cooktops, thanks to their superior switching performance. In this condition, we can reduce the size of passive components considerably. As a result of this, more efficient power conversion, and a slim, low-noise design can be achievable. The decreasing number of turns in induction coils and capacitors with low ESR (Equivalent Series Resistance) values contributes to total efficiency. The cost of WBG power devices can be met by other design parameters, such as passive components with lower values, heatsinks with low volumes, cooling fans with low power, and induction coils with a lower number of turns. High-frequency operation can also be effective in heating nonferromagnetic materials such as aluminum and copper. These types of pans can be heated without complex induction coil and power converter designs due to their high operating frequencies. As a result, the usage of WBG power semiconductors in high-frequency and power conditions makes sense.

The other operating condition is the flexi induction cooktop design with WBG power devices. Flexi cooktops can heat a pan anywhere on the glass. They use multi-inverters structure with multiple induction coils to achieve this type of design. WBG power devices, specifically GaN HEMT, can be suitable for these designs because they can switch at very high speeds. Ultra-high switching speeds can also enable planar magnetics, which is also

an important advantage for increasing power density. Low power loss due to the superior characteristics of GaN HEMT could enable to design without a heatsink and a cooling fan.

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Nomenclature

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