

## S1. Quadrant based Average Velocity

This analysis provides an average velocity based upon the maximum central velocity ( $V_{max}$ ) by double integration as follows:

$$\frac{V}{4} = V_{max} \int_0^b \int_0^a \left[ 1 - \frac{x^2}{a^2} - \frac{y^2}{b^2} + \left(\frac{x}{a}\right)\left(\frac{y}{b}\right) \right] dx dy$$

$$= V_{max} \int_0^b \left[ x - \frac{x^3}{3a^2} - \frac{y^2 x}{b^2} + \frac{x^2}{2a} \left(\frac{y}{b}\right) \right]_0^a dy$$

$$= V_{max} \int_0^b \left[ a - \frac{a^3}{3a^2} - \frac{ay^2}{b^2} + \frac{a^2}{2a} \left(\frac{y}{b}\right) \right] dy$$

$$= V_{max} \int_0^b \left( \frac{2a}{3} - \frac{ay^2}{b^2} + \frac{ay}{2b} \right) dy$$

$$= V_{max} \left[ \frac{2ay}{3} - \frac{ay^3}{3b^2} + \frac{ay^2}{4b} \right]_0^b dy$$

$$= V_{max} \left( \frac{2ab}{3} - \frac{ab^3}{3b^2} + \frac{ab}{4} \right)$$

$$V = 4V_{max} \left( \frac{11ab}{12} - \frac{ab}{3} \right)$$

$$= V_{max} ab \left( \frac{11}{3} - \frac{4}{3} \right)$$

$$V = \frac{7}{3} ab V_{max}$$

$$(2a * 2b)\bar{V} = \frac{7}{3} ab V_{max}$$

$$\bar{V} = \frac{7}{12} V_{max}$$

## S2. Navier-Stokes equations

The two N-S equations are [1, 2]:

- 1) Mass conservation (continuity equation), which states that the mass flow difference between the inlet and outlet is zero:

$$\frac{\partial \rho}{\partial t} + \rho (\nabla \cdot \vec{V}) = 0$$

where  $\rho$  is the density of the fluid and  $\vec{V}$  is the fluid velocity vector.

- 2) Momentum conservation:

$$\rho \frac{\partial V}{\partial t} = \rho g - \nabla p + \mu \nabla^2 V$$

where  $p$  is the fluid pressure,  $\rho g$  the gravitational force,  $\mu$  the kinematic viscosity of the fluid,  $V$  the fluid velocity, vector and  $\nabla^2$  the Laplacian operator.

## S3. Flow through porous media (facemask)

To simulate the turbulent fluid flow resistance of the mask, the following equations have been used [3]:

$$\frac{\Delta p}{d_f} = -D \mu_f U_f - 0.5 I \rho_f |U_f|^2$$

where  $D$  is the Darcy viscous coefficient, ( $I$ ) is the inertial coefficients,  $\mu_f, \rho_f$  and  $U_f$  are the viscosity, density, and velocity of the fluid, respectively. The ( $I$ ) coefficient can be estimated as follows [4, 5]:

$$I = \frac{1}{1.28^2} \frac{1}{0.5 d_f}$$

where  $d_f$  is the fibre diameter of the mask. When considering a face mask,  $D$  can be calculated as follows [3]:

$$D = \frac{64 \xi^{1.5} (1 + 56 \xi^3)}{d_{pc}^2}$$

where  $\xi$  is the packing fibres density and  $d_{pc}$  is the particles diameter.

## References

- [1] White, F.M.; Majdalani, J. *Viscous Fluid Flow*; McGraw-Hill: New York, USA, Vol. 3, 433–434, 2006.
- [2] Tura, A.; Sarti, A.; Gaens, T.; Lamberti, C. Regularization of blood motion fields by modified Navier–Stokes equations. *Med. Eng. Phys.* 1999, 21, 27–36.
- [3] Dbouk, T.; Drikakis, D. On respiratory droplets and face masks. *Phys. Fluids* 2020, 32, 063303.
- [4] Jaksic, D.; Jaksic, N. The porosity of masks used in medicine. *Tekstilec* 2004, 47, 301–304.
- [5] Jaksic, N.; Jaksic, D. Novel theoretical approach to the filtration of nano particles through non-woven fabrics. *Woven Fabrics*; IntechOpen: London, UK, 2012; pp. 205–238.