

Enhancing Cement Paste Properties with Biochar: Mechanical and Rheological Insights

Daniel Suarez-Riera¹, Luca Lavagna^{2*}, Juan Felipe Carvajal¹, Jean-Marc Tulliani², Devid Falliano¹, Luciana Restuccia^{1*}

¹ Department of Structural, Geotechnical and Building Engineering. Politecnico di Torino, Corso Duca degli Abruzzi, 24, Turin, 10129, Italy

² Department of Applied Science and Technology. Politecnico di Torino, Corso Duca degli Abruzzi, 24, Turin, 10129, Italy

* Correspondence: luca.lavagna@polito.it (L.L.); luciana.restuccia@polito.it (L.R.)

Supporting Materials

Methods:

The rheology of the pastes was studied using a rotational rheometer with co-axial cylinders provided by Malvern Pananalytical Company (KINEXUS Pro+) by applying shear rates from 0.1 s^{-1} to 200 s^{-1} over six minutes. The gap between the inner and outer cylinder was 1.15 mm, while the gap between the base of the cup and the bob was set to 5 mm. A Peltier cell was used to keep the system temperature stable at $23 \pm 1.0 \text{ }^{\circ}\text{C}$. The experimental procedure followed the ASTM C1749 standard [1].

Results:

The Bingham model (Eq. **Error! Reference source not found.**) is a rheological model used, for example, for cement pastes with non-zero yield stress and a linear relationship between shear rate and shear stress [2].

$$\tau = \tau_B + \eta_{pl}\dot{\gamma} \quad (1)$$

where τ is the shear stress (Pa), τ_B is the yield stress (Pa), η_{pl} is the plastic viscosity (Pa·s), and $\dot{\gamma}$ is the shear rate (s^{-1}). The yield stress determines the stress above which the material behaves like a fluid, while the plastic viscosity measures how easily the material flows as soon as the shear stress is higher than the yield stress [3].

Table S1. Summary of the main rheological parameters

| ID | BC (%) | τ_B (Pa) | η_{pl} | R^2 |
|-------|--------|---------------|-------------|-------|
| OPC | 0 | 3.19 | 0.35 | 0.999 |
| BC 1% | 1 | 5.65 | 0.37 | 0.999 |
| BC 2% | 2 | 7.79 | 0.47 | 0.999 |
| BC 3% | 3 | 5.44 | 0.490 | 0.998 |
| BC 5% | 5 | 9.27 | 0.75 | 0.997 |
| BC 7% | 7 | 26.12 | 1.11 | 0.999 |

Figure S1 illustrates the effect of the biochar addition on the yield stress (τ_B) and plastic viscosity (η_{pl}) of all the samples. The plain cement reference sample has a τ_B value of 3.19 Pa, while the sample with a biochar content of 2 wt.% showed an increase of around

144%, reaching a τ_B of 7.79 Pa, while a decrement for the sample with 3% (5.44 Pa) was observed. Finally, the mix with a biochar content of 7 wt.% showed a higher yield stress of 26.12 Pa (+ 720% with respect to plain cement mortar). Biochar's effect on main rheological properties probably depends on the sample's preparation, the agglomeration of the particles and their content in each sample. The process of preparing samples matters and significantly influences the sample behavior both in the fresh state and in the hardened state [4,5].

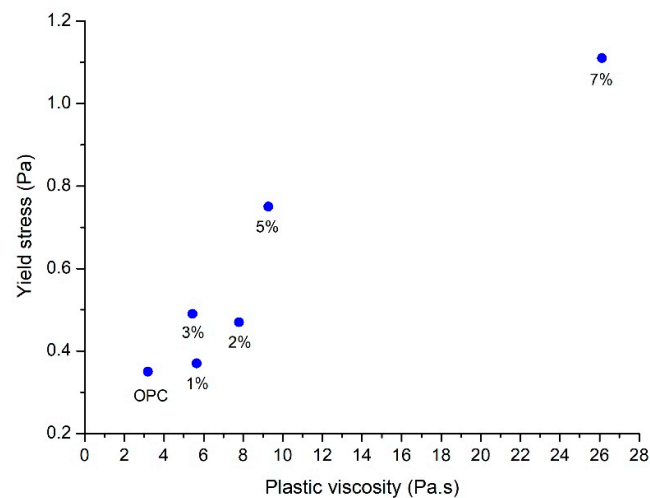


Figure S1. Yield stress in function of plastic viscosity and biochar content.

The yield stress in the 1% biochar-added samples is similar to that of plain cement. However, with higher biochar additions, the yield stress increases due to the greater quantity of particles and the potential interlocking effect, along with a larger number of agglomerates that need to be broken. A low yield stress value is targeted to reach high flowability and high filling ability, whereas a moderate viscosity is important to keep a good cohesiveness and to limit segregation of the mix [6]. Ordinary concrete has a rather high yield stress value (around 500 Pa), while in self-compacting concrete, the yield stress varies from a few Pa to less than 60 Pa [7].

After biochar addition and without any dispersant/superplasticizer, biochar cement pastes yield stress is close to that of self-compacting concrete. Adding particles, specifically those with large specific surface areas, increases yield stress and plastic viscosity due to the higher water demand. Contrarily to yield stress, the plastic viscosity continuously increases with the addition of biochar from 0.35 Pa·s to 1.11 Pa·s, for plain cement and after 7% B addition, respectively (Table S1, Figure S1), since the viscosity is directly influenced by the volume of solids in the mix [8]. In fact, plain cement paste can be seen as a water suspension of cement particles surrounded by a thin layer of water around cement particles. This layer reduces friction between particles and lubricates them, allowing the paste to flow easily. Fine biochar particles absorb a lower amount of water with respect to coarser ones (0.94 ± 0.02 g of water for 1 g of dry biochar). Thus, the local w/c is not altered at the same rate as with coarse biochar particles. However, fine biochar particles are porous and absorb a certain quantity of water. Fine biochar particles can also trap water within interparticle spaces formed because of their agglomeration. This behavior also reduces the available water for lubrication [9].

References

1. ASTM International ASTM C1749-17a - Standard Guide for Measurement of the Rheological Properties of Hydraulic Cementitious Paste Using a Rotational Rheometer 1., doi:10.1520/C1749-17A.

2. Brewer, C.E.; Brown, R.C. Biochar. *Comprehensive Renewable Energy* **2012**, *5*, 357–384, doi:10.1016/B978-0-08-087872-0.00524-2.
3. Ferraris, C.F. *Measurement of the Rheological Properties of High Performance Concrete: State of the Art Report*; Vol. 104;.
4. Rahul, A. V.; Santhanam, M.; Meena, H.; Ghani, Z. 3D Printable Concrete: Mixture Design and Test Methods. *Cem Concr Compos* **2019**, *97*, 13–23, doi:10.1016/J.CEMCONCOMP.2018.12.014.
5. Gupta, S.; Kua, H.W.; Pang, S.D. Biochar-Mortar Composite: Manufacturing, Evaluation of Physical Properties and Economic Viability. *Constr Build Mater* **2018**, *167*, 874–889, doi:10.1016/j.conbuildmat.2018.02.104.
6. Li, Z. *Advanced Concrete Technology*;
7. Bonen, D.; Shah, S.P. Fresh and Hardened Properties of Self-Consolidating Concrete., doi:10.1002/pse.186.
8. Han, D.; Ferron, R.D. Effect of Mixing Method on Microstructure and Rheology of Cement Paste. *Constr Build Mater* **2015**, *93*, 278–288, doi:10.1016/J.CONBUILDMAT.2015.05.124.
9. Gupta, S.; Tulliani, J.M.; Kua, H.W. Carbonaceous Admixtures in Cementitious Building Materials: Effect of Particle Size Blending on Rheology, Packing, Early Age Properties and Processing Energy Demand. *Science of The Total Environment* **2022**, *807*, 150884, doi:10.1016/J.SCITOTENV.2021.150884.

Disclaimer/Publisher's Note: The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.