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# A Real Distribution Network Voltage Regulation Incorporating Auto-Tap-Changer Pole Transformer Multiobjective Optimization

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Received: 11 June 2019; Accepted: 11 July 2019; Published: 14 July 2019



Abstract: A number of studies realized operation of power systems are unstable in developing countries due to misconfiguration of distribution systems, limited power transfer capability, inconsistency of renewable resources integration, paucity of control and protection measures, timeworn technologies, and disproportionately topology. This study underlines an Afghanistan case study with 40% power losses that is mainly pertinent from old distribution systems. The long length of distribution systems, low-power transfer capability, insufficient control and protection strategy, peak-demand elimination, and unstable operation (low energy quality and excessive voltage deviations) are perceived pre-eminent challenges of Afghanistan distribution systems. Some attainable solutions that fit challenges are remodeling (network reduction), networks reinforcement, optimum compensation strategy, reconfiguration options, improving, and transfer capability. This paper attempts to propose a viable solution using multiobjective optimization method of auto-tap-changer pole transformer (ATCTr). The proposed methodology in terms of optimal numbers and placement of ATCTr can be known as a novel two-dimensional solution. For this purpose, a real case of Kabul City distribution system is evaluated. Simulation results indicate the effectiveness of the proposed method in reducing system losses and improving system overall performance. This approach tends to regulate the voltage deviation in a proper and statutory range with minimum number and optimum placement of ATCTrs. The proposed method is simulated using MATLAB® environment to compare and evaluate performance of the proposed network under different situations and scenarios.

**Keywords:** auto-tap-changer pole transformer (ATCTr); distribution network; genetic algorithm (GA); multiobjective optimization; voltage deviation control; voltage regulation; voltage stability

# 1. Introduction

Electric power distribution system with multifarious topologies, configurations, and characteristics is one of the salient components of a power system. In most developing countries, increasing demand for electrical energy enforces distribution systems for an increasingly expansion and broadening. For any expansion, power energy quality and efficiency require special attention of control, improvement,



and management. One of the most effective factors in an electric power energy quality is voltage deviation and stability. Extension of a network length and expansion of topology can be associated with the risk of statutory and standard limit [1]. Kabul is a densely populated and capital city of Afghanistan that distribution networks suffer unstable-rated operation. These networks are extended without length limitation consideration, which demonstrates unstable voltage beyond the statutory range with huge technical and economic losses. In recent years, the government of Afghanistan bounded to retain environmental protection and sustainable development in accordance with the Paris Agreement 2015 (combat climate change), and Sustainable Development Goals (SDGs) 2030. Reform of the energy sector has been part of this endeavor. Afghanistan's distribution networks are the least developed and old-fashioned part of the power system. In addition to the technical and financial losses, shortage of access to electric energy has led to increased utilization of primary energy resources and fossil fuel with high environmental impact. Meanwhile, distribution systems to remote areas are extended without expandability capacity (in local and regional networks) consideration. In priority, it must seriously consider and adopt appropriate solutions. The effective delivery of power to the end users can be achieved by improving reliability, efficiency, cost-effectiveness, and sustainability measures of production and distribution [2].

Various investigations using different optimization techniques, methods, and solutions are conducted to regulate voltage and reduce energy losses in a distribution system. In [3], multiobjective optimization of auto-tap-changer pole transformer with respect to minimizing the voltage deviation of a 16-bus distribution network was tested. In [4], a coordinated control of distributed energy storage system (ESS) with traditional voltage regulators including on-load tap changer transformers (OLTC) and step voltage regulators (SVR) was applied. Authors of [5] proposed data fusion theory to develop a comparative diagnostic method to determine the operation status of on-load tap changers mechanism. A study was carried out in [6] to enhance power quality with automatic tap change in transformer in a smart grid distribution system. In [7], an implementation of a prototype electronic tap-changer instead of mechanical tap-changer was proposed. This method was demonstrated with some shortcomings, such as low operating speed, short lifetime, and heavy size. In [8], the authors employed a nonlinear dynamic model of OLTC, impedance loads, and decoupled reactive power voltage relations to reconstruct the voltage collapse phenomenon. This method aims to determine operation status of on-load tap changers mechanism. Likewise, in [9], a network reconfiguration was carried out over two domains simultaneously: Re-switching strategies and transformer tap-changer adjustments. Similarly, several techniques and strategies for voltage stability enhancement and regulation have been applied, using several case studies under different conditions [10–15]. This study aims to present a fully solid-state tap-changer solution with a new control strategy and optimal configuration.

Over the past decades, power system blackouts due to voltage instability were repeatedly reported; namely, Tokyo blackout on 23 July 1987 and United Kingdom, Sweden, Canada, Denmark, Italy, and the United States blackouts in 2003 [16]. Power system voltage stability has been discussed enough over the past decades. In [17], a control strategy for reactive power compensation using storage system was studied. This study aimed to improve system stability by a proper prediction of reactive behavior and demand for different operation conditions. In [18], the authors presented the stability analysis using the load and generation levels as a direction vector for the base system through continuation power flow (CPF) under normal condition and contingency. The authors of [19] proposed a wavelet transform (WT) based on data analysis to extract the features from real-time active power and RMS (root mean square) voltage of the power grid. This study applied a hybrid classification technique based on particle swarm optimization (PSO) and support vector machines (SVM) to classify the features and diagnose different types of faults in a smart grid system.

Previous studies investigated the use of control devices in a variety of ways based on different optimization methods. Most of these studies were focused on required number of control device without considering the optimum placement and number of these devices. The proposed methods can technically be feasible, but economically they are not acceptable. Therefore, reducing number of control

devices in a system is another important objective. To solve the trade-off problem, the multiobjective optimization is an excellent tool. Additionally, the increase in tap position changing can reduce contacts lifespan and accelerate deterioration of transformer oil in the switching process [20]. This paper provides a method of multiobjective optimization of auto-tap-changer pole transformer (ATCTr), in term of optimum number and placement of tap position changes. Meanwhile, a multiobjective optimization using genetic algorithm [21–25] is applied to minimize voltage deviation. In Section 2, characteristics of system model and problem description are discussed. Section 3 presents the methodology, follows by the simulation result and comparison in Section 4. At last, Section 5 concludes simulations findings and briefs novelty and effectiveness of the study.

#### 2. Characteristics of the System Model and Problem Description

The targeted model in this study was located in Kabul city (capital of Afghanistan). Triple energy sectors, generation, transmission, and distribution systems, suffer technical and economic losses. After a long-term political instability and lack of maintenances, Kabul city distribution networks demonstrate many problems; namely, transformer no-load loss, imbalance between primary and secondary distribution systems in terms of power transfer, scattered distribution transformer from gravity center of load, unbalance reactive power and distributed three phase supply, lack of protection devices, long length of customers cables, use of nonstandard equipment, etc. [26]. Reports pertain 25–40% losses to distribution systems that require a viable solution and proper management of technical and economic losses [27]. Meanwhile, an increasing population growth forces distribution networks to operate close to their stability limit within maximum expandability [28]. Definitely, system expansion under stressed voltage control condition has a direct impact on voltage profile and power losses [29]. For this case study, voltage deviation at distribution level is out of acceptable range; whereas, at the time of peak load demand, it reaches 15% voltage deviation.

Figure 1 shows the proposed 20 kV distribution system consisting of 22 buses and 21 lines that are considered a real model of simulation. Table 1 illustrates the mentioned distribution system transmission lines parameters. The proposed model supplies residential, commercial, and industrial consumers. This system consists of transformer stations (TSs) and junction station (JS-6) that feeds from the (110/20 KV, 50 MVA Breshna Kot substation).



Figure 1. Breshna Kot distribution network model.

Line Neurolean	Bus C	ode	Longth (km)	$\mathbf{R}(\mathbf{pu})$	<b>X</b> (pu)
Line Number	From	То	- Lengui (Kiii)	K (pu)	x (pu)
1	1	2	0.75	0.246	0.072375
2	2	3	0.8	0.2624	0.0772
3	3	4	0.6	0.1968	0.0579
4	3	12	0.4	0.1312	0.0386
5	4	5	0.65	0.2132	0.062725
6	5	6	0.95	0.3116	0.091675
7	5	13	0.7	0.2296	0.06755
8	6	7	0.65	0.2132	0.062725
9	6	14	1.4	0.4592	0.1351
10	14	15	0.6	0.1968	0.0579
11	7	8	0.8	0.2624	0.0772
12	7	16	0.65	0.2132	0.062725
13	16	17	0.6	0.1968	0.0579
14	17	18	0.55	0.1804	0.053075
15	8	9	0.65	0.2132	0.062725
16	9	10	0.4	0.1312	0.0386
17	9	19	0.8	0.2624	0.0772
18	19	20	0.45	0.1476	0.043425
19	20	21	0.4	0.1312	0.0386
20	21	22	0.4	0.1312	0.0386
21	10	11	0.45	0.1476	0.043425

Table 1. Kabul city 20 kV distribution system transmission line parameters.

#### 3. Methodology

Maintaining stable operation and reliable supply remain the first ever anticipation of any distribution system [30]. The effectiveness of voltage control device over available approaches for voltage stability and control are highlighted in the literature. This study targets ATCTr from different standpoints of optimum selection, requirement, and placement. Proper planning of ATCTr contributes voltage stability and improve voltage profile with minimum number of control devices. Since ATCTr devices are expenses, considering the minimum penetration of these devices with optimum placement can optimize resources technically and economically (installation and maintenances costs). This paper deals with optimum required number and placement of ATCTr using multiobjective algorithm.

# 3.1. Multiobjective Optimization Using Genetic Algorithm

Multiobjective formulations are realistic models for many complex engineering optimization problems. A reasonable solution to a multiobjective problem is to investigate a set of solutions, each of which satisfies the objectives at an acceptable level without being dominated by any other solution. Multiobjective optimization using genetic algorithm (GA) is approached in this paper to obtain the optimal number of ATCTr, and minimize voltage deviation [21–25]. Load flow analysis is simulated by Newton–Raphson (NR) method [31]. The current distribution network is considered as a single-phase model, operating under a balanced state.

## 3.2. Objective Functions

Selection of the objective functions is a significant task to obtain an optimum solution in an optimization problem. It also necessarily affects optimization behavior as well. In this study, two objective functions are considered for optimization as shown in Equations (1) and (2).

$$min: F_1 = \sum_{i=1}^N a_i \tag{1}$$

$$min: F_2 = \sum_{i=1}^{N} \left( V_{i,t} - 1 \right)^2 \tag{2}$$

where,  $F_1$  is the objective function, it represents the total number of installed ATCTr, and  $F_2$  is another objective function represents overall voltage deviation of nodes.  $a_i$  represents the number of introduced ATCTr at each node *i*,  $V_{i,t}$  is the voltage deviation on each node *i* at time *t*, *N* is the total number of nodes.

Constraint inequalities are as follows:

$$V_{min} \le V_i \le V_{max} \tag{3}$$

$$T_{min} \le T_i \le T_{max} \tag{4}$$

where,  $V_i$  is the distribution voltage of node *i*;  $V_{min}$ ,  $V_{max}$  are voltage lower and upper limits, respectively.  $T_i$  is the tap position of node *i*;  $T_{min}$ ,  $T_{max}$  are the tap position lower limit and tap position upper limit, respectively.

Equality restriction is as follows:

$$g_A: \sum_{t=0}^{q} x_t = 5$$
 (5)

$$g_B : \sum_{t=0}^{q} x_t = 10 \tag{6}$$

$$g_C : \sum_{t=0}^{q} x_t = 15 \tag{7}$$

where  $g_A - g_C$  are the constraints of the number of tap change position, and  $x_t$  is the tap change position number at time *t*.

#### 3.3. Optimal Placement Problem

Optimal placement problem of control devices remains a serious issue. Sometimes, disarrangement of control device not only cannot be effective, also can be associated with technical and economic losses. Likewise, if equipment is not fit in an optimal location, its effectiveness decreases and is not technically feasible. When the objective function is set to minimize voltage deviation and number of installed ATCTr, in this scenario, voltage control efficiency depends on the placement of ATCTr [32,33]. Moreover, optimal scheduling of devices depends on the placement of the devices. Therefore, optimum placement of ATCTrs can reduce voltage deviation.

Multiobjective optimization using GA with the objective function of voltage deviation was applied to solve the optimization problem. The proposed method aims to hence perform a power flow analysis, to calculate voltage magnitudes at different buses. GA randomly in each process locates ATCTr in different nodes with different alignments and configurations. These processes are repeatedly carried out until the comparison between all genes is made. Finally, the best gene (optimal placement) with least voltage deviation is specified from comparing the last population with the best gene from the new population. In order to take into account, the optimal placement of ATCTrs, a string of N bits (representing the total N nodes) was used to decide the location nodes at which to introduce an ATCTr, as shown below:

$$\mathbb{P} = (a_N, a_{N-1}, \dots, a_1), \ (a_i \in 1, 0) \tag{8}$$

where,  $\mathbb{P}$  represents the placement of installed ATCTrs in overall nodes. Here, "0" represents a node with no ATCTr, whereas "1" represents a node with ATCTr-installed bus. Figure 2 and Table 2 represent an example of coding used for multiobjective optimization; the placement of installed ATCTrs in distribution network is demarcated with circles.



Figure 2. An example of auto-tap-changer pole transformer (ATCTr) installation placement cording.

Table 2. Binary coding use for ATC	Trs placement in nodes.
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Node Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
Installed position	0	0	1	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Comprehensively, the stages of the proposed methodology are demonstrated in the flowchart shown in Figure 3.



Figure 3. Flowchart of the multiobjective optimization of ATCTrs.

## 4. Simulation Result and Comparison

To confirm the effectiveness of introducing ATCTr (with a provision of  $\pm 10\%$  change in voltage at 1.25% additional voltage per tap), simulation results based on the physical structure of the current distribution system is shown in Figure 1.

Proper range for voltage deviation as defined by standard is  $0.95 \le V_i \le 1.05$  pu. The proposed distribution network parameters considering daily load profile and real-time voltage profile of the entire system are plotted in Figure 4a,b, respectively. This is followed by the distribution voltage magnitude using ATCTrs in Figure 4c. The number of tap position changes in a 24-h period ( $g_c$ ) is 15 times. Moreover, the Pareto optimum solution for minimizing the number of introduced ATCTrs and minimizing of the voltage deviation considering tap position changes is shown in Figure 4d.



**Figure 4.** Real distribution network model: (**a**) Daily load profile; (**b**) hourly voltage profile (uncontrolled); (**c**) voltage profile using ATCTrs (controlled); (**d**) Pareto optimal solutions.

Genetic algorithm (GA) as a multiobjective optimization technique is used to obtain study objectives. Since the number of tap position changes is representative of a rough equipment lifetime, multiobjective optimization was solved for tap position using the number of tap position changes as a parameter ( $g_A$ – $g_C$ ). Tables 3–6 show the location of ATCTrs for the solutions A–D. Pareto optimal solutions are shown in Figure 4d.

Node Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
Equality constraint of $g_A$	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Equality constraint of $g_B$	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Equality constraint of $g_C$	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Table 3. Optimum placement of ATCTrs (solution A).

			Tat	ole 4	<b>i</b> . U	ptii	nur	n p	lace	men	tor	AIC	Irs (s	solut	ion	D).						
Node Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
Equality constraint of $g_A$	0	0	1	0	0	1	0	0	1	0	1	0	0	0	0	1	0	0	0	1	0	0
Equality constraint of $g_B$	0	0	0	1	0	0	1	0	1	0	0	0	0	0	1	0	1	0	0	1	0	0
Equality constraint of $g_C$	0	0	1	0	0	0	1	0	1	0	1	0	0	1	0	0	0	0	1	0	0	0

c

Node Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
Equality constraint of $g_A$	0	0	1	0	1	1	0	1	1	0	1	0	1	0	1	1	0	1	1	0	1	1
Equality constraint of $g_B$	0	1	0	1	0	1	1	0	1	0	1	1	1	0	1	0	1	1	0	1	0	1
Equality constraint of $g_C$	0	1	0	1	0	1	1	1	0	1	0	1	1	1	0	0	1	0	1	0	1	1

Table 5. Optimum placement of ATCTrs (solution C).

						•		•														
Node Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
Equality constraint of <i>g</i> <sub>A</sub>	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
Equality constraint of g <sub>B</sub>	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
Equality constraint of g <sub>C</sub>	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

Table 6. Optimum placement of ATCTrs (solution D).

The voltage waveforms for solutions A–D has shown in Figures 5–8.



**Figure 5.** Node voltages of solution A for all tap position constraints ( $g_A$ – $g_C$ ). (a) Node voltages (equality constraint of  $g_A$ ); (b) node voltages (equality constraint of  $g_B$ ); (c) node voltages (equality constraint of  $g_C$ ).

Simulation findings manifest a decisive improvement of voltage profile with stability indicator. Comparison of Figure 4b, c shows an entire system of stable operation and voltage profile transition from lower than 0.85 pu to more than 0.98 pu. Previous studies relied on optimal placement of control devices; while, this study in addition to optimal placement of control devices (Tables 3–6), focused on optimum number of control devices to ensure technical and economic dimensions within a single solution. Figure 4d shows the Pareto optimum solution, which indicates the relationship between the number of ATCTrs and voltage deviation. Besides, number of tap position changes have also been considered as an important factor in a rough equipment life time of an ATCTr depreciation. Increasing changing tap position can significantly reduce a contact lifespan, and accelerates deterioration of

transformer oil in switching process. Therefore, the control of changing tap potions is a known exigence. As shown in Figures 5–8, depending on the equality constraints ( $g_A$ – $g_C$ ), reducing voltage deviation for constants ( $g_B$  and  $g_C$ ) is very close (almost equal). With automatic control and using  $g_B$  instead of  $g_C$  (in addition to setting voltage) enhances the lifespan of ATCTr.



**Figure 6.** Node voltages of solution B for all tap position constraints ( $g_A$ – $g_C$ ). (**a**) Node voltages (equality constraint of  $g_A$ ); (**b**) node voltages (equality constraint of  $g_B$ ); (**c**) node voltages (equality constraint of  $g_C$ ).



**Figure 7.** Node voltages of solution C for all tap position constraints ( $g_A$ – $g_C$ ). (**a**) Node voltages (equality constraint of  $g_A$ ); (**b**) node voltages (equality constraint of  $g_B$ ); (**c**) node voltages (equality constraint of  $g_C$ ).



**Figure 8.** Node voltages of solution D for all tap position constraints ( $g_A$ – $g_C$ ). (a) Node voltages (equality constraint of  $g_A$ ); (b) node voltages (equality constraint of  $g_B$ ); (c) node voltages (equality constraint of  $g_C$ ).

The results are visualized in Figures 5–8, and simulation findings are summarized in Table 7.

Table 7. Comprehensive results of Figures 5–8.

	Solution A	Solution B	Solution C	Solution D
Voltage magnitude for $g_A$	0.8995	0.9397	0.9413	0.9487
Voltage magnitude for $g_B$	0.9157	0.9457	0.9642	0.9711
Voltage magnitude for $g_C$	0.9251	0.9641	0.9703	0.9786

The first column of Table 7 shows voltage magnitudes for solution A, which shows an increase in accordance with equality constraints ( $g_A-g_C$ ), respectively. In the second column, by adding the number of ATCTrs in solution B, voltage magnitudes are maintained at statutory limits ( $0.95 \le V_i \le 1.05$ pu). For constant  $g_C$ , voltage is at an acceptable range. In the third column of Table 7, in addition to maintaining voltage in an appropriate range, a comparison of  $g_B$  and  $g_C$  indicate that voltage values are very close and almost equal (Figure 7). Furthermore, the fourth column shows the similarity of the voltage magnitudes for constants  $g_B$  and  $g_C$  as well (Figure 8). Hence, using  $g_B$  is preferred compared to  $g_C$  for ATCTr's better performances.

For the entire system, the proposed method can improve reinstates busses voltage to rated level and maintain unity behavior among all buses in term of voltage profile. Results indicate that in the presence of the ATCTrs, voltage stability and profile for entire distribution system can be improved. Meanwhile, it can maintain voltage at a proper and statutory range by installing ATCTrs in less than half nodes.

## 5. Conclusions

This paper evaluates the effectiveness of ATCTr as a voltage control device with respect to voltage deviation. This study offers a viable solution for reliable operation of a distribution system in term of voltage deviation control and power transfer improvement. Different from the literature that propose optimal placement of (ATCTr) in a system, this study considers the optimum required number of ATCTr as well. The results indicate the effectiveness of the proposed solution from technical and

economic standpoints. The multiobjective optimization using genetic algorithm (GA) was used based on Newton–Raphson power flow with the objectives of minimizing voltage deviation and simultaneously minimizing the number of introduced voltage control devices. The 22-bus real distribution network was simulated. The proposed algorithm (GA) was compared different cases with specifying the optimum number of ATCTr using Pareto front method. From the findings, this method can effectively overcome the voltage regulation problem by giving optimum location and required number of (ATCTrs).

Author Contributions: Conceptualization, S.M.S.D.; methodology, S.M.S.D. and R.S.; resources, P.M., N.K. and A.M.H.; data curation, M.K.; writing—original draft preparation, S.M.S.D. and M.K.; writing—review and editing, S.M.S.D.; supervision, T.S.

Funding: This research received no external funding.

Conflicts of Interest: The authors declare no conflicts of interest.

# Abbreviations

a <sub>i</sub>	The number of introduced ATCTr at each node <i>i</i>
F <sub>1</sub> , F <sub>2</sub>	Objective functions
$g_A \sim g_C$	The numbers of tap change position
Ν	Total number of buses
$\mathbb{P}$	The placement of installed ATCTrs in overall nodes
$T_i$	The tap position of node <i>i</i>
$T_{min}$ , $T_{max}$	Lower and upper tap position limits
$V_i$	Distribution voltage of node <i>i</i>
$V_{i,t}$	Voltage deviation on each node <i>i</i> at time <i>t</i>
$V_{min}$ , $V_{max}$ .	Voltage's lower and upper limits respectively
$x_t$	The number of taps changing positiont time $t$

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