



# Article Reverse Osmosis Membrane Zero Liquid Discharge for Agriculture Drainage Water Desalination: Technical, Economic, and Environmental Assessment

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**Abstract:** Agricultural drainage water (ADW) represents a potential source for fresh water after receiving appropriate treatments to satisfy the water quality requirements. Desalination of ADW with medium salinity and moderate contamination with organic and inorganic chemical pollutants could provide a techno-economically feasible approach for facing water scarcity in arid areas. The current work presents a conceptual zero liquid discharge ADW desalination system proposed to treat 300,000 m<sup>3</sup>/d. The system is based on pretreatment to remove impurities harmful to desalination by staged reverse osmosis (RO) membrane. The brine from the last RO stage is treated via thermal vapor compression followed by evaporation in solar ponds to recover more fresh water and salts of economic value. The essential technical features of the proposed system components are formulated. The proposed system components and its technical and economic indicators are deduced using available software for water pretreatment, RO membrane, desalination, thermal desalination, and solar evaporation ponds. The system provides total distilled water recovery of about 98% viz. 294,000 m<sup>3</sup>/d in addition to recovered salts of 245,000 t/y. The net cost of water production amounts to USD 0.46 /m<sup>3</sup>. The environmental considerations of the system are addressed and advantages of applying zero liquid discharge system are elucidated.

Keywords: agricultural drainage water; RO membrane; desalination; evaporation; economics; ZLD

# 1. Introduction

Water shortage has emerged as a major issue as the world's population grows and natural water supplies get depleted. It has been forecasted that the global demand for fresh water will exceed the supply by 40% by 2030 [1,2]. It is expected that water scarcity will increase from about one third to nearly half of the global urban population in 2050 [3]. Desalination has been widely used in regions with limited water supplies to address the problem of water shortages [4]. Desalination is the extraction of freshwater from brackish or salt water. Since the oceans cover 70% of the earth's surface, salty water desalination has the potential to offer a plentiful freshwater supply. Desalination has proved to be a viable and reliable solution to the worldwide water shortage during the last few decades. As of 2020, the global installed desalination capacities for freshwater production are about 97.2 million  $m^3$ /day provided by 20,971 projects [5]. The current global trend shows that membranebased desalination technology is finding new outlets for supplying water to meet the growing water demand in most of the water-scarce countries [6,7]. The climate changes due to global warming are constantly increasing the salinity level of both land and seawater, thus reducing the availability of existing fresh water for households, agriculture, and industry. Irrigation with desalinated seawater has led to a significant increase in salinity and boron in the soils, which could affect the yield of moderately tolerant crops [8]. This has made it urgent to invent an appropriate water treatment technology that not only removes macro,



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**Copyright:** © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). micro, and nano-pollutants, but also desalinates water to a significant extent. Continued research and development of new treatment technologies are essential to improve the availability and quality of water supplies for agricultural use [9,10]. Consequently, thermal and membrane-based desalination technologies are playing an important role in solving global water scarcity problems.

Desalinated water has several advantages including (a) reduction of the possibilities of soil salinity, which has adverse effect on soil properties, (b) increasing the cultivated land area and the number of crops, and (c) improving crop quality and productivity [11]. Brackish water reverse osmosis (RO) and seawater reverse osmosis (SWRO) are the two most common desalination methods used to produce water for agriculture (SWRO). When compared to thermal desalination methods, SWRO has emerged as the most sophisticated and leading technique because of higher product water quality, reduced energy needs, and hence cheaper water costs [12].

Therefore, the aim of this work is to develop a cost effective and integrated scheme for ADW desalination with zero liquid discharge. The system is based on pretreatment to remove impurities harmful to desalination by staged reverse osmosis (RO) membrane.

#### 2. Methods

## 2.1. Identification of Typical Characteristics of ADW

Agricultural drainage water (ADW) is characterized by variation of its composition from one site to another due to different effluent sources discharged to a specific drain [13]. Large drains or more specifically final drain streams exhibit moderate variation in quality as compared to small drains receiving frequent shock loads. Examples of large drains in Egypt are Bahr El-Bakar, El-Omoum, and Bahr Hadous. In this study, a typical main drain water source is considered, based on relatively stable water composition, allowing to propose an appropriate technique for treatment. Also, main drains allow considering large capacity and provide flexibility in the treatment plant site selection based on economic and environmental considerations.

Furthermore, a typical ADW treatment composition is considered. Table 1 presents the typical composition of ADW, which is mainly characterized by the following features: medium salinity in the range of brackish water, high hardness content, high suspended solids, low organic contamination, and low Fe and Mn content.

Item	Na	К	Mg	Ca	Cl	HCO <sub>3</sub>	SO <sub>4</sub>	NO <sub>3</sub>
Conc. (mg/L)	596	30	140	110	1070	370	355	40
Item	Fe	Mn	TDS	ТР	pН	TSS	COD	BOD
Conc. (mg/L)	2	1	2705	1	7.7	80	20	10

Table 1. Raw water composition.

### 2.2. Rationale of Developed Proposed Treatment Scheme

The proposed treatment system is based on technically solid concepts to be applied on large scale and is environmentally accepted. The developed system comprises the following sections:

Pretreatment includes a chlorination section followed by flocculation, filtration, and sludge dewatering. This process sequence ensures the removal of microbiological contamination (e.g., algae), and performs as a softener to remove most of the Ca and Mg content, Fe and Mn, suspended solids, and organic matters. Separated sludge is dewatered and dried to be sold as a recovered by-product, while filtrate from dewatering is recycled to the process. A dual media filtration stage ensures removal of residual turbidity.

Desalination is then proposed to produce high quality water for different applications. Reverse osmosis is the most economic technique applied for that purpose. Desalination is performed by two-stage reverse osmosis (RO) to achieve maximum water recovery. The previous pretreatment allows high water recovery from RO due to eliminating most of the impurities affecting RO performance.

The concentrate from RO is further desalted to increase freshwater recovery via thermal desalination technique to produce fresh water and concentrated brine.

The concentrated brine is directed to solar evaporation ponds to recover salts.

Recovered salts from solar ponds as well as dried residues from water pretreatment present an additional economic value.

### 3. Results

# 3.1. Basic Engineering of Proposed System

Basic engineering essentially comprises material balance and technical features as well as specifications for a specified system capacity. The basis of design of the system components is presented in Table 2.

		1. Pre-Treatment	
Raw Water F	Feed Flowrate	$300,000 \text{ m}^3/\text{d}$	
Chlorine dose		8 mg/L	
Sodium hyd	droxide dose	400 mg/L	
Floce	culant	10 mg/L	
Sys	stem	Low pressure-pumping station, In-line chlorination, chemicals (caustic soda and flocculant) addition, flocculation, and clarification, in one tank, followed by dual media filtration.	
Po	wer	1525 kW	
		2. RO stages	
	First Stage RO	Second Stage RO	
Feed flow rate	300,000 m <sup>3</sup> /d	$30,000 \text{ m}^3/\text{d}$	
Recovery	90%	60%	
	3. T	hermal Concentration	
Feed f	lowrate	12,000 m <sup>3</sup> /day	
Sys	stem	Thermo vapor compression (TVC)	
Po	wer	913 kW	
Reco	overy	50%	
		4. Solar Pond	
Feed fl	ow rate	6000 m <sup>3</sup> /d	
Average clima	ate conditions:		
Tempo	erature	24 °C	
Hun	nidity	50%	
Solar iri	radiation	$412.2 \text{ W/m}^2$	
Wind	speed	3.5 m/s	
Rai	nfall	65 mm/y	
Elevation above sea		15	

Table 2. Basis of design of the system components.

The specifications of the main streams characteristics and components specification have been identified with the aid of software available for chemical pretreatment using the following software:

- WatPro, version 4.0, Hydromantis, water treatment simulator for predicting water quality, Hamilton, Ontario, Canada
- RO using LewaPlus<sup>®</sup>, version 5.0, Calculation and Design Software, LANXESS, Deutschland GmbH Liquid Purification Technologies Kennedy platz 150569 Cologne, Germany,
- Thermal desalination using WT Cost II<sup>©</sup> software developed by the Bureau of Reclamation and Moch Associates, U.S. Department of the Interior, Bureau of Reclamation Technical Service Center, Denver, Colorado, according to the design features provided, and solar evaporation ponds using Excel.

# 3.2. Material Balance

The material balance of the main components of the integrated ZLD desalination system is illustrated in Figure 1. Tables 3 and 4 present the water composition of the main pretreatment streams and RO stages, respectively.

	Raw Water	Sedimentation Effluent	Filtration Effluent
Na (mg/L)	596	945	945
Ca (mg/L)	110	28	28
Mg (mg/L)	140	46	46
K (mg/L)	30	30	30
Cl (mg/L)	1070	1070	1070
SO <sub>4</sub> (mg/L)	355	355	355
CO <sub>3</sub> (mg/L)	-	147	147
HCO <sub>3</sub> (mg/L)	370	232	232
NO <sub>3</sub> (mg/L)	40	40	40
Fe (mg/L)	2	-	-
Mn (mg/L)	1	-	-
TOC (mg/L)	10	1	-
TDS (mg/L)	2705	2896	2892
рН	7.7	9.8	9.8
TOC (mg/L)	10	1	-
Turbidity (NTU)	100	5	1
Solid ppt		CaCO <sub>3</sub> 205.6 mg/L	
		Mg (OH) <sub>2</sub> 228.6 mg/L	

Table 3. Water Composition of the main pretreatment streams.

Table 4. Composition of two-stage RO streams \*.

Stream Item	Feed Raw Water	Permeate (1)	Permeate (2)	Concentrate (1)	Concentrate (2)
Na (mg/L)	945	17.5	130	9291	23,080
Ca (mg/L)	28	0.2	1.4	278.4	694
Mg (mg/L)	46	0.3	224	457.4	1140
K (mg/L)	30	0.83	6.12	292.7	722.5
Cl (mg/L)	1070	25	1863	13,622	33,772
SO <sub>4</sub> (mg/L)	355	1.3	9.7	3538.3	8831
CO <sub>3</sub> (mg/L)	147	0	0	0	0.003

Stream Item	Feed Raw Water	Permeate (1)	Permeate (2)	Concentrate (1)	Concentrate (2)
HCO <sub>3</sub> (mg/L)	232	0.04	0.28	20.3	50.3
NO <sub>3</sub> (mg/L)	40	5.4	37.3	350.3	819
CO <sub>2</sub> (mg/L)	0.05	0	273.6	273.6	273.6
TDS (mg/L)	2892	273.6	373.3	24,850	69,108
рН	9.8	2.32	3.18	4.9	5.26

\* Before post-treatment of permeate.



**Figure 1.** Process flow diagram, main components, and material balance of the proposed zero liquid discharge ZLD desalination system.

## 3.3. Technical Features and Specifications of the Proposed System

Table 5 presents the technical features and main technical specifications of the pretreatment stage, which comprises low pressure pumping station, chlorination, chemical treatment, flocculation and sedimentation, sludge dewatering, and clarified water dual media filtration.

Table 5.	The main	technical	specifications	of pretreat	tment components.
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Item	Specifications
Chlorination	Chlorine gas vacuum feeding system $2 \times 100 \text{ kg/h}$ , with 10 chlorine gas cylinders (1 t capacity), with pumps and accessories, control and chlorine detection, and elimination system included in a separate building provided with proper ventilation.
Chemical handling system	NaOH storage tanks (3000) m <sup>3</sup> capacity, pumps centrifugal, CI, 20 m <sup>3</sup> /h, 50 m head, feed tanks 100 m <sup>3</sup> capacity feed pumps CI 10 m <sup>3</sup> /h, 20 m. Flocculant preparation tank (30 m <sup>3</sup> ) and pumps, (tanks 10 m <sup>3</sup> with mixers), feeding pumps 1 m <sup>3</sup> /h, variable speed, 5 bar pressure.
Chemical treat- ment/flocculation/ clarification tank	4 tanks each 40 m diameter, with 4 m side wall depth, with chemical addition/flocculation section inlet, discharge wires, and sludge discharge arrangements. Mixers for rapid mixing and flocculation and sludge scraper.
Sludge dewatering	The system includes sludge pumps $8 \times 10 \text{ m}^3/\text{h}$ , head 50 m. 4 sludge continuous belt filters, each 10 m <sup>3</sup> /h. 4 belt conveyers for cake (1 m width, 20 m length). 4 filtrate recycling pumps 10 m <sup>3</sup> /h, 20 m head.
Filtration unit	Dual media pressure filters (anthracite/sand). Operating pressure 3 bar. Diameter 3.5 m. Filtration rate 30 m <sup>3</sup> /m <sup>2</sup> h. No. 50 With automatic backwash system.

The main technical features and specifications of two-stage RO are illustrated in Table 6. The first RO stage (RO1) is responsible for the recovery of fresh water up to 90% of feed water. The concentrate from this stage is directed to a second stage (RO2) to recover more fresh water of up to 60% of the quantity of the concentrate of RO1.

The concentrate of the second RO stage, (RO2) is treated in a thermal concentration unit based on thermo vapor compression (TVC) to recover up to 50% of the concentrate of RO2. The main system components are: boilers with accessories, distiller components, vessels and heat transfer tubes, pumps, degassing and chemical design units, piping including fittings and valves, electrical instrumentation and control, distiller's support including platforms and other necessary components, thermal ejectors, chemical cleaning system, and buildings.

The concentrate from thermal concentration is directed to solar evaporation ponds in a nearby environmentally, economically, and socially accepted site to evaporate water and recover salts of economic value. The effective area of ponds amounts to 401,630 m<sup>2</sup>. The actual area includes banks and walkways, which amount to 50 m<sup>2</sup>. The walls and bottom are lined with layers of clay, geotextile, and HDPE sheets to mitigate any salty water leakage to ground water.

Item	Specifications		
item	1st Stage	2nd Stage	
Feed flow rate	300,000 m <sup>3</sup> /d	30,000 m <sup>3</sup> /d	
Recovery	90%	60%	
Feed pressure "bar"	28.7	57.0	
Pump pressure "bar"	5	5	
Concentrate pressure "bar"	30	30	
High pressure pump Pump/ motor efficiency	84%/94%	84%/94%	
High pressure pumps motors power	12,622 kW	2502 kW	
Pump/motor efficiency	84%/94%	84%/94%	
Booster pump motors power.	626 kW	-	
System components	Cartridge filters, RO trains, RO membrane elements, high pressure pumps with energy recovery. Inter-connecting piping, post treatment, membrane cleaning unit, electrical system, and instrumentation and control, auxiliary equipment and building.		
S	System Configuration		
Number of stages/elements	2/13,150	1/1250	
Elements number per vessel	SW HR 400 34/10	SW HR 400 34/10	

Table 6. Technical specification of RO units.

#### 4. Financial Indicators for ZLD System

## 4.1. Cost Estimation and Financial Indicators

Cost estimates have been performed based on updated published data to the year 2021 using Chemical Engineering Cost index and the prementioned software in Section 3.2

#### 4.2. Construction Cost Estimates

The summary of the construction cost of the proposed system is presented in Table 7. The construction cost is estimated to be about USD 116.4 million. Reverse osmosis units' costs represent about 51.4% of the total costs. The total desalination cost (including RO and TVC) amounts to USD 74.92 million, representing about 64% of the total construction cost. The estimated construction costs per  $m^3/day$  amounts to USD 396/ $m^3d$ . These findings agree well with published work where the capital cost for brackish water RO desalination was USD 100 million at 300  $m^3/d$  by adopting a developed empirical correlation from hundreds of desalination plants [14].

Table 7. Summary of construction cost estimates.

No	Item	Cost USD 1000
1.	Pumping station	11,394
	Pretreatment	
2	Chlorination	2160
۷.	Chemical treatment/flocculation clarification and sludge dewatering	6933
	Filtration	5398
	Total pretreatment	25,885

#### Table 7. Cont.

No	Item	Cost USD 1000
	Reverse osmosis units	
3.	RO1	56,210
	RO2	3610
	Total RO units	59,820
4.	Thermal concentration	15,100
5.	Solar evaporation	15,600
	Total	116,405

#### 4.3. Operating Costs Estimates

Table 7 presents a summary of the operating costs estimates for the proposed system. The annual operating cost is estimated to be about USD 48 million. The major cost items are chemicals and electricity, representing 53% and 21.5%, respectively.

#### 4.4. Annual Production Costs Estimates

The annual production costs are the results of the annual operating cost in addition to annual capital amortization.

Tables 8 and 9 present the estimated operating costs, revenues, and total production costs.

No	Item		Annual Cost USD 1000/y	
1.		Electricity		
		Electricity consumption: $1.47 \times 10^8$ kWh/y @ USD 0.07/kW/h		
2.	Fuel	75 t/d @ USD 100/t	247	
3.	Chemicals	NaOH 120 t/d @ USD 300/t Cl <sub>2</sub> 2.4 t/d @ USD 150/t HCl (100% basis) 112.5 t/d @ USD 300 t/d Flocculant/anti-scaling 3.6 t/d @ USD 2000/t	11,826 118.3 11,087 2365.2	
			25,396.5	
4.	Membrane Replacement	Membrane lifetime 3 y Membrane cost USD 400/element	1920	
5.	Maintenance	3% of capital cost	3492	
6.	Labor	150 persons @ USD 15,000/y	2250	
	Subtotal		43,595.5	
7.	Other operating cost	10% of subtotal	4359.5	
	47,955.0			

Table 8. Estimates of annual operating costs.

The net annual production costs are estimated to be about USD 56 million. Considering the revenues from recovered salts, the net annual production costs are estimated to be about USD 43.7 million. The net production cost per cubic meter of produced water is USD 0.453 m<sup>3</sup>.

The published range for the unit cost for brackish water RO desalination for 10,000 to 70,000 m<sup>3</sup>/d capacities and 2000–6000 mg/L are 0.39–0.66 USD/m<sup>3</sup> [15,16]. It is worth mentioning that using electrodialysis for brackish water desalination may be lower by 5–33% according to the capacity (Generous et al., 2021). In general, the RO desalination unit cost for seawater and brackish water for capacities up to 450,000 m<sup>3</sup>/d is considered

to be in the range of  $0.7-1.4 \text{ USD/m}^3$  and  $0.3-0.7 \text{ USD/m}^3$ , respectively [14]. Moreover, Panagopoulos (2021) studied brackish water and seawater ZLD systems. He concluded that for the seawater system, the estimated cost is  $0.84 \text{ USD/m}^3$  which is 1.24 times higher than the brackish [17].

Item	Basis	Annual Cost USD 1000
Operating cost	According to Table 8	47,955
Capital amortization	Plant lifetime 20 y Interest rate 4%	8566
Total annual cost		56,521
Revenues	Mixed salts (NaCl, CaCl <sub>2</sub> , MgSO <sub>4</sub> ) 245,000 t/y @ USD 50/t	12,250
Net annual cost		44,271
Cost/m <sup>3</sup>	Plant operation factor 0.9	USD 0.46

**Table 9.** Estimated Annual Costs, Revenues and Cost/m<sup>3.</sup>.

#### 5. Environmental Considerations

The following environmental issues are addressed.

The zero-discharge desalination system provides many advantages related to environment. These include maximization of natural resources recovery and prevention of ground water contamination.

The site of the plant should be carefully selected on the bank of a main drain away from discharge points from polluted sources to avoid shock loads that sharply affect the quality of the water fed to the plant, which may cause severe deterioration of plant performance.

The site of the evaporation ponds should also be properly selected. It should be far from the residential and agricultural areas. It is preferably in a desert area near the plant site. The nature of the site and its hydrogeological characteristics should allow for environmental and economic ponds construction.

Sludge resulting from pretreatment containing mainly calcium and magnesium salts could be safely disposed of or reused after natural sun drying.

The costs of the proposed system should be re-evaluated based on the actual site conditions, which affect production cost, especially chemical water treatment, which represents a considerable proportion of the cost.

### 6. Conclusions

Agricultural drainage water (ADW) with medium salinity and heavy metal contamination could be treated to produce water of high quality for reuse. Zero liquid discharge desalination is technically and environmentally an accepted approach, by attaining maximum water and salt recovery for economic applications.

This case under study for treating ADW with a capacity of 300,000 m<sup>3</sup>/d concluded a total water recovery of 98% of the raw ADW. The 2% concentrated brine treated in solar evaporation ponds could recover about 245,000 ton/per year of salts, containing mainly sodium, potassium, calcium, and magnesium salts.

The estimated construction cost of the plant amounts to about USD 116.4 million, and the cost of produced water amounts to about USD  $0.46/m^3$ .

The cost of water production could considerably increase if lower recovery values are considered. The brine disposal, as an alternative, although may not be accepted from the environmental point of view in many situations, yet, if accepted, could be applied in specific situations with potential cost reduction. **Author Contributions:** Conceptualization, M.H.S. and M.M.E.S.; methodology, A.M.G.A. and H.F.S.; software, H.A.H.; validation; M.M.E.S., S.R.T.; investigation, M.H.S. and M.M.E.S.; original draft preparation, A.M.G.A.; review and editing, S.R.T.; funding acquisition, M.M.E.S. All authors have read and agreed to the published version of the manuscript.

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