

## Article

# First Principles Study of Atomic Oxygen Adsorption on Austenitic Stainless Steels Surfaces: A Theoretical Study

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**Abstract:** The adsorption of atomic oxygen and surfaces is the starting point and key point to understand the oxidation process of stainless steel. Nowadays, numerous studies have focused on the metal composition of stainless steel, while the mechanism of non-metallic elements affecting atomic oxygen adsorption needs to be clarified. Here, adsorption of atomic oxygen on the surface of pure  $\gamma$ -Fe and H/N-containing austenitic stainless steels was investigated using first principles. We found that stable adsorption ( $>6$  eV) can occur on pure  $\gamma$ -Fe and H/N-containing austenitic surfaces. In this process, the presence of hydrogen and nitrogen both enhance the adsorption of atomic oxygen, but their influence mechanisms are in opposition. Hydrogen enhances adsorption by breaking metal bonds near the surface, while nitrogen promotes adsorption by enhancing structural stability. The adsorption promotion of hydrogen ( $-6.7629$  eV) is stronger than that of nitrogen ( $-6.6374$  eV), but it can reduce the stability of the system. The introduction of appropriate nitrogen atoms may be beneficial to the improvement of corrosion resistance. This study provides valid data and a unique perspective on the erosion protection of atomic oxygen on austenitic surfaces.

**Keywords:** austenite; first principles; adsorption; atomic oxygen; stainless steel



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## 1. Introduction

Stainless steel materials with excellent mechanical, processing and welding properties [1] are often used to build vacuum systems [2] and in aerospace applications [3]. However, they are often subject to atomic oxygen erosion when used in the low earth orbit environment because of the large amount of atomic oxygen present in this environment [4]. This erosion results in the formation of various oxides on the surface, which can change the surface properties.

Nowadays, the research on the oxidation process of stainless steel surfaces has been widely reported [5–8] and many encouraging results have been achieved. It has been recognized that oxidation begins with oxygen adsorption. The subsequent process is the nucleation, growth and coalescence of two-dimensional oxides. In these processes, the complex interaction between atomic oxygen and metal surfaces is the core. Oxygen adsorption at the long bridge site is generally considered to be more stable [9] than at other sites considered to be highly symmetrical in adsorption [10]. In addition, Tomasz Ossowski and Adam Kiejna [11] have shown that the adsorption of atomic oxygen at all highly symmetrical sites (pseudo threefold-hollow, long-bridge, short-bridge, on-top) is stable at both low (0.25 monolayer) and high (1 monolayer) coverage conditions. The electron is transferred from the surface Fe atom to the oxygen atom when the atomic oxygen interacts with the surface of stainless steel [9]. In fact, previous theoretical studies have shown that oxygen produces dissociative adsorption on the surface of iron [10]. The

adsorption of atomic oxygen is a non-activated process when the coverage rate is up to 1 monolayer [12], while the dissociation adsorption is non-activated when the coverage rate is lower (<0.5 monolayer) [12,13]. As adsorption proceeds, oxygen atoms tend to gather and begin to penetrate below the surface to form FeO. The penetration of more oxygen atoms leads to the gradual transformation of FeO into Fe<sub>3</sub>O<sub>4</sub> [14]. However, the adsorption of atomic oxygen will be disturbed by other kinds of atoms. For instance, atomic oxygen is more likely to be trapped by Cr [15,16] because of the stronger electronegativity difference between oxygen and chromium [17]. Therefore, a common understanding is that the corrosion resistance of stainless steel stems from the chromium-rich oxide layer (theoretically composed of different oxides of iron and chromium and their mixtures, with the main component being Cr<sub>2</sub>O<sub>3</sub> [18]), which acts as a barrier to prevent further diffusion of atomic oxygen into the material [19–21].

Many studies attribute the good corrosion resistance of stainless steel to Cr<sub>2</sub>O<sub>3</sub> to the low diffusion constants of Cr and O [22–25]. Meanwhile, it has higher chemical stability compared to Fe oxides [26,27]. Chromium dominates the entire oxide layer at very low oxygen pressures (below 103 Pa) and temperatures above 350 °C [28–31]. These oxides can effectively improve the corrosion resistance of the alloy. For example, the contact surface on the nanometer scale presents a more uniform and compact shape when the clean surface of pre-oxidized FeCrNi alloy makes contact with water vapor. This dense Cr oxide barrier layer can prevent the further oxidation of Fe [8]. However, this can lead to many serious consequences. One consequence is the depletion of Cr content on the surface, which will greatly affect the surface performance. On the other hand, only iron oxide is formed on the surface at temperatures up to 400 °C, although not all Fe-Cr alloys follow this rule [32]. This means that the protective layer dominated by Cr is not always effective.

In fact, interstitial nonmetallic atoms such as nitrogen also affect the adsorption of atomic oxygen. These atoms can exist stably in the gap of FCC due to the small atomic radii. They can affect the oxidation process by causing local structural deformation and affecting the movement of electrons in the crystal. Hydrogen can be present in stainless steel in a variety of forms, such as an interstitial atom [33], owing to its small atomic radius. These hydrogen states can have many effects on the properties of the alloy such as hydrogen embrittlement [34]. In contrast, nitrogen can only obtain low mobility due to its large atomic radius. Similar to hydrogen, nitrogen can also exist in steel in the form of interstitial atoms. It is a very strong element for forming and stabilizing austenite [35,36]. It is well known that nitrogen alloying can significantly improve the pitting resistance of austenitic stainless steel despite its limited solubility. Ye et al. [37] believed that the rapid passivation and stabilization mechanism of the nitrogen-containing surface of austenitic stainless steel [38–41] is closely related to the improvement of adsorption capacity caused by the presence of N atoms. These atoms can change the properties of the local structure and thus affect the adsorption of atomic oxygen. Unfortunately, relevant studies are lacking.

In this work, we investigated the effect of interstitial atoms H and N on the adsorption of atomic oxygen using first principles.  $\gamma$ -Fe is used to represent austenitic stainless steel. Six control groups were set up to investigate the effect of interstitial atoms on atomic oxygen adsorption. In all models, spin polarization is included. The adsorption energy is used to analyze the interaction between atomic oxygen, and surface and cohesion energy is used to characterize the stability of the system. The electronic structure is analyzed by density of states (DOS), electron localization function (ELF) and crystal orbital Hamilton population (COHP). Atomic charges based on Mulliken's work is used to analyze charge transfer. This study provides valid data and a unique perspective on the erosion protection of atomic oxygen on austenitic surfaces.

## 2. Calculation Details

This work is based on the density functional theory (DFT) in the Vienna Ab-initio Simulation Package (VASP) [42]. The eight-layer face-centered cubic (FCC) structure with 144 atoms is used as an austenitic stainless steel. The interstitial atoms H and N are placed

in a second layer close to the surface before structure optimization. Atomic oxygen is placed in a vacuum layer above the interstitial atoms. The distance between atomic oxygen and the surface is within the van der Waals radius. After the pure austenite is fully relaxed, the fractional coordinates of the atoms in the lower five layers are fixed to represent the bulk phase, while the top three layers are allowed to relax. A vacuum layer of 15 Å is introduced in the c-axis direction to eliminate periodic effects. Adsorption energy ( $E_{ads}$ ) and cohesive energy ( $E_{coh}$ ) [43,44] are used to discuss the adsorption state and stability of the system, respectively, and the calculation formulas of these are as follows:

$$E_{ads} = E_{tot} - E_{sub} - E_{ao}$$

where  $E_{tot}$  is the total energy of the model,  $E_{sub}$  is the energy of the block without sorbent and  $E_{ao}$  is the energy of the atomic oxygen.

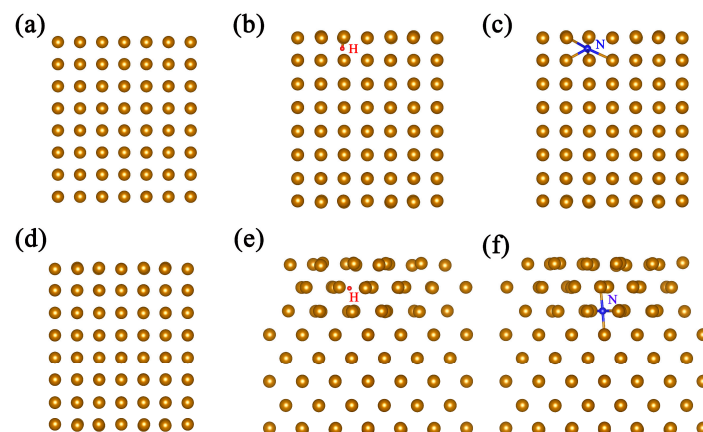
$$E_{coh} = \frac{1}{n} \left( E_{tot} - \sum x_A E_{atom}^A \right)$$

where  $n$  is the total number of atoms,  $E_{tot}$  is the total energy of the model,  $x_A$  is the number of atoms of type A and  $E_{atom}^A$  is the energy of an isolated type A atom.

Perdew-Burke-Ernzerhof (PBE) [45] exchange-correlation functional and Projector Augmented-Wave (PAW) [46,47] pseudopotential are used in this work. We use a cut-off energy of 500 eV to compute all models. Self-consistent field (SCF) convergence threshold is set to  $1 \times 10^{-5}$  eV/atom. The model of pure austenite was first fully relaxed. Then, all models were optimized for atomic positions, and the force on each ion was less than 0.02 eV/Å. The Grimme method of DFT-D3 [48] was used to correct the van der Waals forces between atomic oxygen and austenite. Spin polarization was also considered. A  $2 \times 1 \times 1$  k-point grid in the Brillouin region was used in all models. VASPKit [49] is used in the analysis of DOS. Visualization for Electronic and Structural Analysis (VESTA) [50] is used to draw the ELF [51]. Local-Orbital Basis Suite Towards Electronic-Structure Reconstruction (LOBSTER) [52–54] is used for COHP [55]. Atomic charges based on Mulliken's work [56] were used to analyze charge transfer.

### 3. Results and Discussion

First, the pure  $\gamma$ -Fe and austenite containing interstitial atoms H and N was calculated, and these models are shown in Figure 1. The cohesive energy is shown in Table 1.



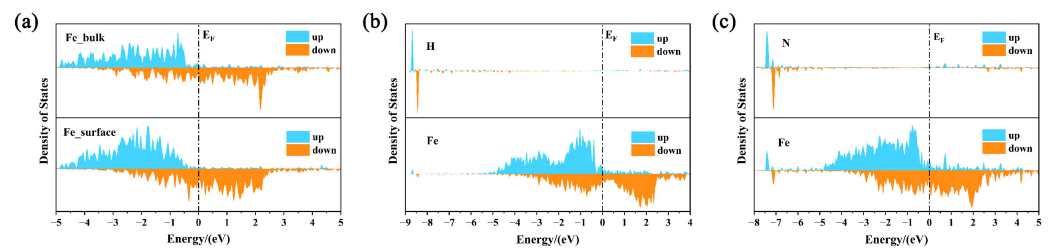
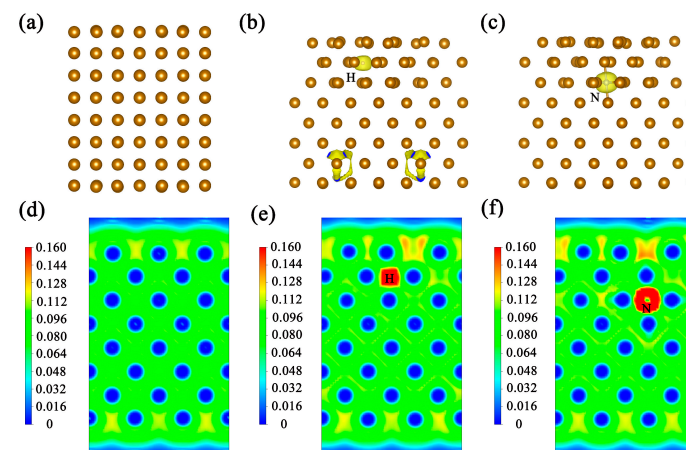
**Figure 1.** Models of pure  $\gamma$ -Fe and H/N-containing austenite. (a–c) are the models of pure  $\gamma$ -Fe and H/N-containing austenite before geometry optimization, respectively. (d–f) are the models of pure  $\gamma$ -Fe and H/N-containing austenite after geometry optimization, respectively.

**Table 1.** Cohesive energy of all models without atomic oxygen adsorption.

	$E_{coh}/(\text{eV/atom})$
Pure $\gamma$ -Fe	−4.4515
H-containing Fe	−4.4413
N-containing Fe	−4.4741

Both hydrogen and nitrogen atoms can be stably located at the gap of  $\gamma$ -Fe, but they are at different sites, as seen in Figure 1. The small atomic radius [17] allows the hydrogen atom to be trapped by the Fe atom. Turnbull and Hutchings [57] suggested that austenite is a trap for hydrogen capture. Although the trap effect in austenite is smaller than that of the austenite-ferrite interface, the existence of austenite makes the diffusion path provided by ferrite more tortuous. However, Turk et al. [58] argue that it is uncertain whether austenite can be treated simply as a point trap. It is undeniable that hydrogen can stably exist in the interior and surface of austenite and affect its properties, although the mechanism of hydrogen capture is controversial. On the contrary, the nitrogen atom is located in the octahedral gap in the FCC structure. It is able to interact with multiple nitrogen atoms to stabilize the FCC structure. This is demonstrated by an increase in cohesion energy, as seen in Table 1. These also have been confirmed by a large number of previous studies [33,35,36,59–61]. This octahedral interstitial atom can bring additional lattice distortion energy to the overall system [61], resulting in a significant increase in strength and corrosion resistance [62]. In fact, these nitrogen atoms can react with Cr to form a relatively stable interstitial nitride phase on the surface of stainless steel. They can act as kinetic barriers for alloy dissolution [63].

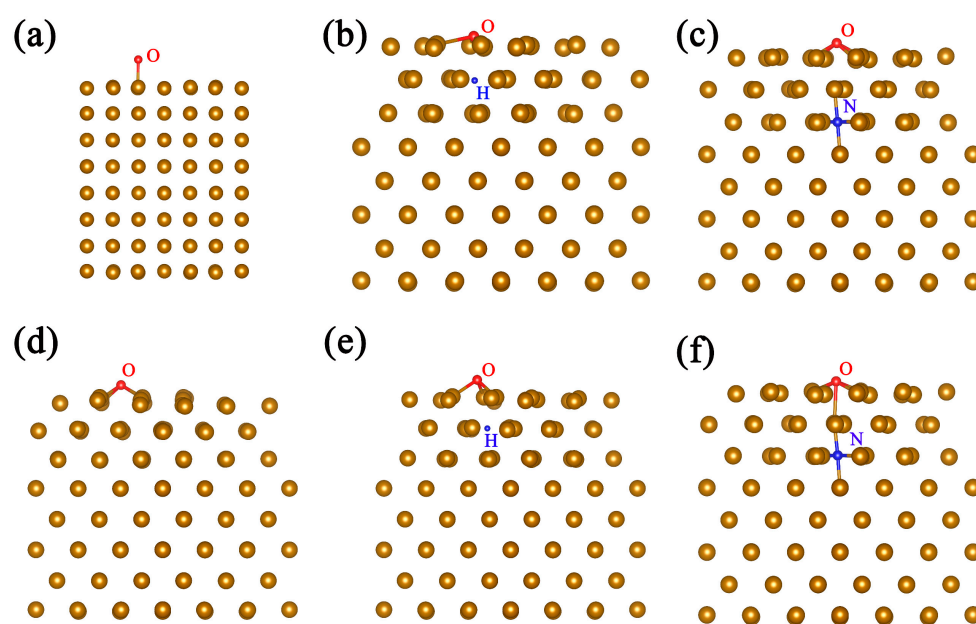
The DOS and ELF of pure  $\gamma$ -Fe and H/N-containing austenite are shown in Figures 2 and 3, respectively.

**Figure 2.** DOS of pure  $\gamma$ -Fe and H/N-containing austenite. (a–c) are the DOS of pure  $\gamma$ -Fe and H/N-containing austenite, respectively.**Figure 3.** DOS of pure  $\gamma$ -Fe and H/N-containing austenite. (a–c) are the 3D ELF of pure  $\gamma$ -Fe and H/N-containing austenite, respectively. (d–f) are the 2D ELF of pure  $\gamma$ -Fe and H/N-containing austenite, respectively.

Both hydrogen and nitrogen doping cause charge enrichment, as shown in Figure 3b,c. The solitary electron property of hydrogen allows the charge inside the metal to be effectively bound around it, which can break the metal bonds in a localized environment. One consequence of this is that good ductility may be weakened near the local environment of the doping. The conclusion that a large amount of hydrogen is harmful to austenite has been proven by many previous works [34,64–66].

However, the nitrogen atoms located in the octahedral gap sites enhance the stability of the FCC structure. Although nitrogen doping can also cause lattice distortion in the local structure, the FCC structure is not damaged, which is consistent with previous studies [62,67–69]. The DOS also confirms these. In pure  $\gamma$ -Fe, the 3D orbitals of the internal Fe atom have good delocalization property in the energy range of  $-5$  to  $3$  eV due to the internal crystal field, as seen in Figure 2a. On the contrary, the surface Fe atom has higher activity, which results in the occupied state of 3D electrons mainly in the energy range of  $-4$  to  $2$  eV. The DOS of the Fe atom produces corresponding occupied states in the deep energy range of  $-7$  to  $-9$  eV after the interstitial atom was introduced, as seen in Figure 2b,c. It indicates that a chemical bond is formed between the interstitial atom and the Fe atom. In particular, for the nitrogen atom, its p-orbital undergoes a more pronounced dispersion.

Then, adsorption behavior of atomic oxygen on these model surfaces was calculated, and these models are shown in Figure 4. The adsorption energy, cohesive energy and Mulliken charge of atomic oxygen are shown in Table 2.



**Figure 4.** Model for the adsorption of atomic oxygen on pure  $\gamma$ -Fe and H/N-containing austenite. (a–c) are the models for the adsorption of atomic oxygen on pure  $\gamma$ -Fe and H/N-containing austenite before geometry optimization, respectively. (d–f) are the models for the adsorption of atomic oxygen on pure  $\gamma$ -Fe and H/N-containing austenite after geometry optimization, respectively.

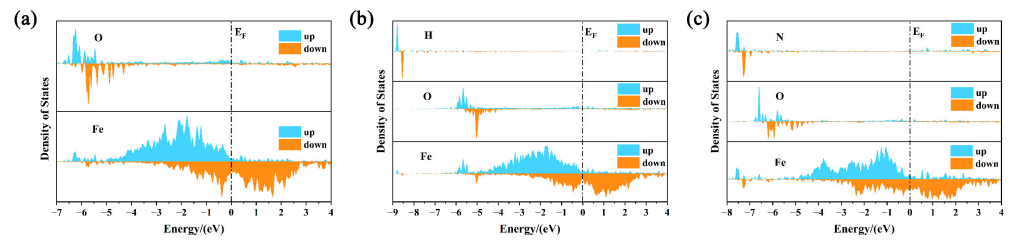
**Table 2.** Adsorption energy, cohesive energy and Mulliken charge of atomic oxygen of all models.

	$E_{ads}/(\text{eV})$	$E_{coh}/(\text{eV/atom})$	Mulliken Charge of Atomic Oxygen/(e)
Pure $\gamma$ -Fe with atomic oxygen	$-6.1312$	$-4.7355$	$-0.69$
H-containing Fe with atomic oxygen	$-6.7629$	$-4.7242$	$-0.66$
N-containing Fe with atomic oxygen	$-6.6374$	$-4.7483$	$-0.69$

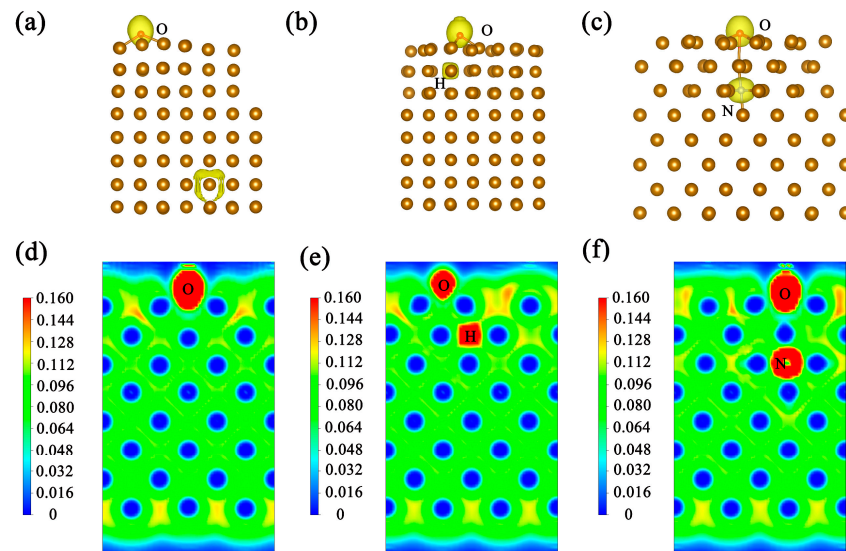
When adsorption occurs, the atomic oxygen interacts with multiple iron atoms and stably adsorbs at the bridge site, as shown in Figure 4. This is consistent with the previous literature [9,10]. Numerous experimental studies have been conducted on the process of oxygen adsorption on iron surfaces. It is shown that oxygen atoms are adsorbed in the fourfold coordinated hollow sites of Fe (100) in the initial stage [70]. On this basis, a series of ordered structures were found. The  $c(2 \times 2)$  superstructure is formed at 0.25 monolayer oxygen coverage [9,71]. They are then transformed into more complex structures under 0.33 monolayer coverage conditions, which are often oversimplified to a  $c(3 \times 1)$  pattern [72]. Additional structures [73] have been proposed to explain the latter model because its mechanism is more complex. For higher coverage, iron oxide begins to form. In this progress, oxygen atoms tend to gather and begin to penetrate below the surface to form FeO. The penetration of more oxygen atoms leads to the gradual transformation of FeO into Fe<sub>3</sub>O<sub>4</sub> [14]. However, these processes are interfered with by other kinds of atoms. As mentioned above, atomic oxygen is more likely to be trapped by Cr [15,16] because of the stronger electronegativity difference between oxygen and chromium [17]. The dense chromium oxide barrier formed by Cr and O prevents further oxidation of Fe [8]. This is generally considered as the mechanism of corrosion resistance of stainless steel. But one of the costs is the depletion of Cr content on the surface in the oxygen-rich environment.

Similar to the case of no sorbents, both hydrogen and nitrogen atoms can be stably located at the interstices of  $\gamma$ -Fe, but their positions are different, as seen in Figure 4. In all cases, the charge is always transferred from iron to atomic oxygen, which is consistent with the previous literature [9], as shown in Table 2. Strong charge transfer exists between austenite and atomic oxygen to form chemical bonds. The adsorption energy of atomic oxygen on pure  $\gamma$ -Fe is between the adsorption energy of the bridge site and the hollow site, as reported in Ye's work [37]. This situation is reasonable due to different parameter selection. The hydrogen atom can be stably located close to the surface, while the nitrogen atom will penetrate deep into the austenite in order to be stable. Similarly, the hydrogen atoms are in the interstices, while the nitrogen atoms are located in the octahedral sites. There is a difference in the effect on adsorption energy although they behave similarly. The hydrogen atoms can break the metal bonds of the local environment thus weakening the stability of the system. At the same time, the small atomic radius [17] allows it to be present close to the surface. The force of the crystal field on the surface electrons is weakened when the electrons in the doped region are attracted by hydrogen, which will lead to higher activity of the surface electrons. As a result, the atomic oxygen will be more tightly adsorbed on the surface, as seen in Table 2. The action mechanism of the nitrogen atom is the opposite to that of hydrogen. It is located further away from the surface than hydrogen, but it is able to stabilize the FCC structure [62,67–69]. Atomic oxygen makes it difficult for the surface to undergo more severe lattice distortions when the structure of several atomic layers near the surface is strengthened by nitrogen. In this progress, the enhanced internal structure will weaken the crystal field force on the surface electrons because the local charge is tightly bound inside, which is consistent with the previous literature [37]. According to Ye's report [37], the adsorption energy will increase along with the nitrogen content. Therefore, the mechanism of increasing adsorption energy may be one of the reasons for rapid passivation and stabilization of the passivation film on nitrogen-containing austenitic stainless steel [40,41]. In other words, the introduction of appropriate nitrogen atoms may contribute to the rapid passivation and stability of the surface passivation film, which is beneficial to the corrosion resistance. However, the adsorption of atomic oxygen is also closely related to the coverage. High density coverage will lead to the repulsive interaction between atoms, which can significantly reduce the adsorption energy [11]. Therefore, the content of interstitial atoms and the coverage rate of atomic oxygen should be considered comprehensively when studying the oxidation resistance of stainless steel.

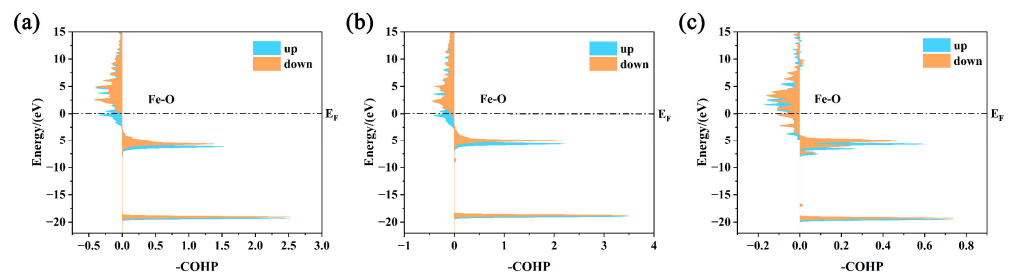
The DOS, ELF and COHP of these models adsorbed with atomic oxygen are shown in Figures 5–7, respectively.



**Figure 5.** DOS of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen. (a–c) are the DOS of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen, respectively.



**Figure 6.** ELF of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen. (a–c) are the 3D ELF of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen, respectively. (d–f) are the 2D ELF of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen, respectively.



**Figure 7.** COHP of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen. (a–c) are the COHP of pure  $\gamma$ -Fe and H/N-containing austenite adsorbed with atomic oxygen, respectively.

Figure 6d–f shows the charge enrichment caused by the doping of hydrogen and nitrogen and the adsorption of atomic oxygen. The DOS and COHP also confirmed these phenomena. Both oxygen and iron have corresponding occupied states in the energy range of  $-6.5$  to  $-4.5$  eV, as seen in Figure 6a–c. This indicates that the 2s orbital of oxygen and the 3d orbital of Fe overlap and form a chemical bond, which is consistent with previous studies [10,11]. At the same time, interstitial atoms and iron atoms have corresponding occupied states in the deep energy range of  $-7$  to  $-9$  eV. The 2s orbital of the oxygen atom becomes more dispersed in all cases because it can interact with multiple iron atoms, and this is also the case for the 2p orbital of the nitrogen atom. However, the 1s orbital of hydrogen is significantly spin polarized rather than dispersed because it only has one electron [17], as shown in Figure 5.

The peculiar one-electron structure of hydrogen atoms allows electrons from iron to accumulate around the hydrogen nucleus, which weakens the strength of the metal bonds within the crystal. The result is that the activity of the surface electrons increases due to the weakening of the crystal field force. On the contrary, nitrogen can enhance FCC stability, which has been demonstrated by a large number of studies [67–69]. The enhancement of internal local structure weakens the force between the surface and the interior. This also leads to increased activity of electrons on the surface. COHP confirmed this. As shown in COHP, the Fe-O bond in both the pure  $\gamma$ -Fe model and hydrogen-containing model has only anti-bonding components contributed by spin-up electrons, as seen in Figure 7a,b. On the contrary, the antibonding component is contributed by both the spin up and spin down electrons in the nitrogen-containing model. This is because nitrogen enhances the stability of the FCC structure, which makes the internal electrons tightly bound. This leads to the increased activity of electrons on the surface because the bonding between the interior and the surface is weakened. As a result, the system stability and adsorption energy increased. The phenomenon of nitrogen increasing adsorption energy has also been reported in the previous literature [37]. The mechanism of increasing adsorption energy may be one of the reasons for rapid passivation and stabilization of the passivation film on nitrogen-containing austenitic stainless steel [40,41]. Therefore, the introduction of appropriate nitrogen atoms may contribute to the rapid passivation and stability of the surface passivation film, which is beneficial to the corrosion resistance.

#### 4. Conclusions

In this study, we have investigated the adsorption of atomic oxygen on the surface of pure  $\gamma$ -Fe and H/N-containing austenitic stainless steels using first principles. The conclusions are summarized as follows:

- (1) Atomic oxygen can be stably adsorbed on the surface of pure  $\gamma$ -Fe and H/N-containing austenitic because of huge adsorption energies ( $>6$  eV);
- (2) Both interstitial atoms H and N can enhance the adsorption of atomic oxygen on the surface, but their mechanism of action is in opposition. Hydrogen enhances adsorption by breaking metal bonds near the surface, while nitrogen enhances adsorption by enhancing structural stability;
- (3) The enhancement effect of hydrogen on adsorption energy ( $-6.7629$  eV) is stronger than that of nitrogen ( $-6.6374$  eV), but hydrogen will lead to the decrease of the stability of the system;
- (4) The introduction of appropriate nitrogen atoms may contribute to the rapid passivation and stability of the surface passivation film, which is beneficial to the corrosion resistance.

This study provides valid data and a unique perspective on the erosion protection of atomic oxygen on austenitic surfaces.

**Author Contributions:** Conceptualization, X.Z. (Xinghua Zhu) and Y.X.; Software, Q.F.; Data curation, X.Z. (Xinghua Zhu), Z.L. and L.X.; Funding acquisition, Y.X., N.W., X.Z. (Xiaoyang Zhu) and Z.H.; Investigation, X.Z. (Xinghua Zhu), Z.L. and J.H.; Resources, Q.F.; Writing—original draft preparation, X.Z. (Xinghua Zhu); Writing—review and editing, Y.X.; Supervision, Y.X.; Visualization, Y.X. and Z.H. All authors have read and agreed to the published version of the manuscript.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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