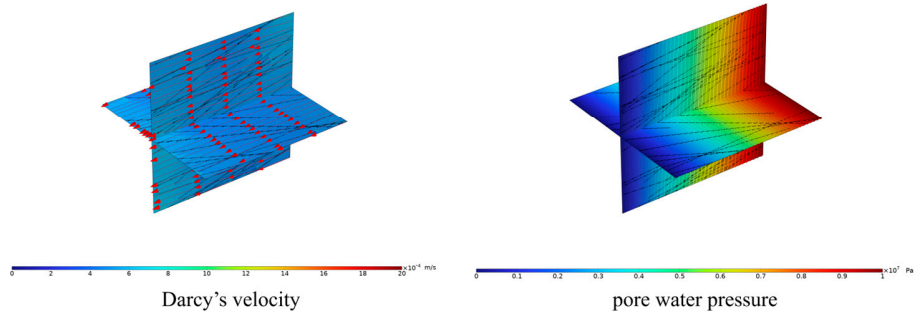
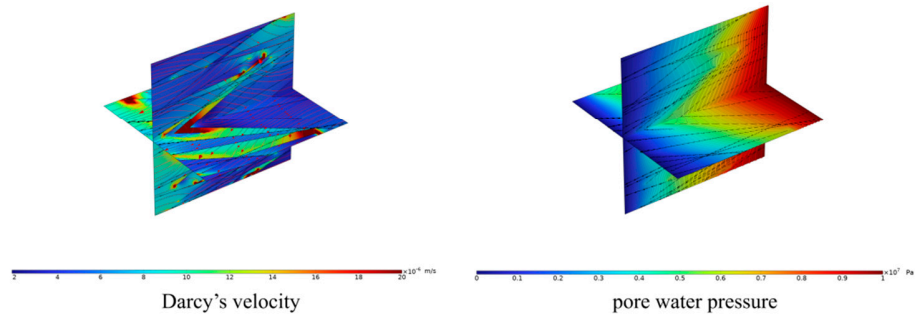


## supplementary materials

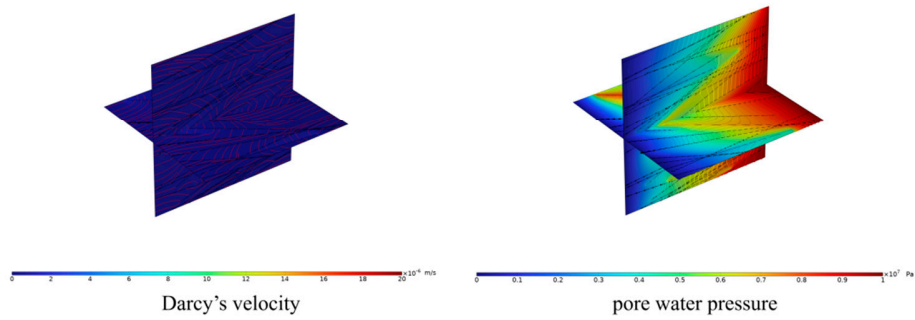
Matrix permeability:  $10^{-12} \text{m}^2$



Matrix permeability:  $10^{-14} \text{m}^2$

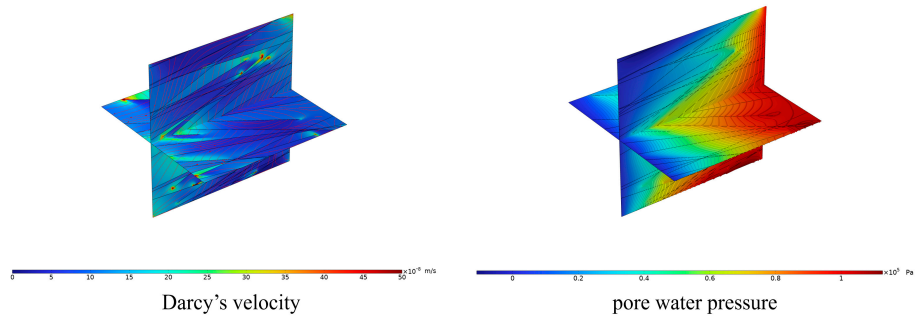


Matrix permeability:  $10^{-16} \text{m}^2$

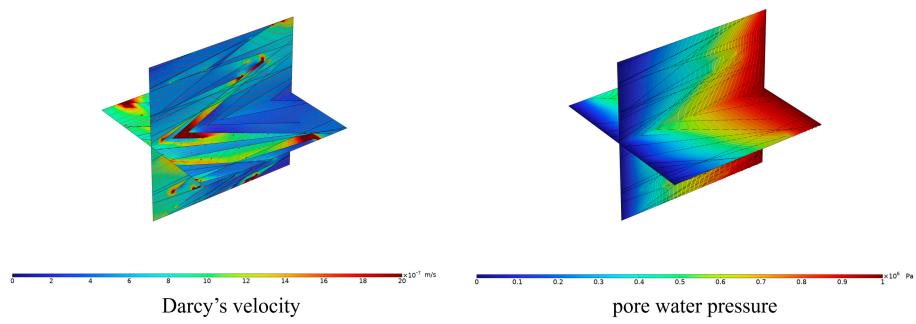


**Figure.S1** Darcy velocity and pore pressure cross-section diagrams at different matrix permeabilities

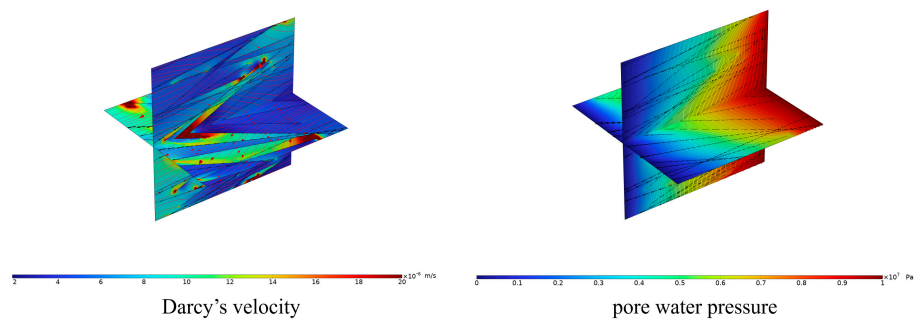
hydraulic pressure:  $10^5$  Pa



hydraulic pressure:  $10^7$  Pa

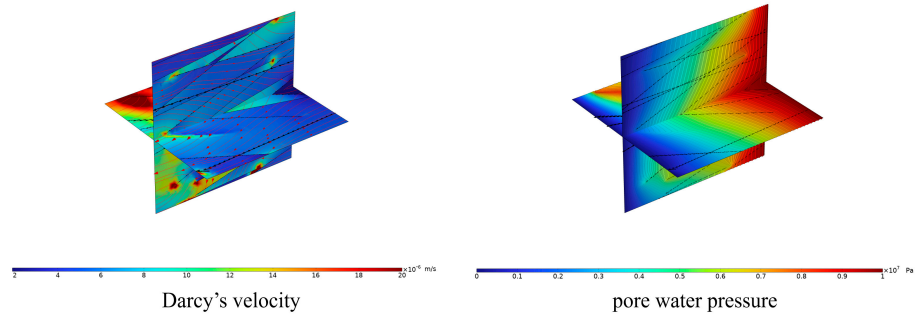


hydraulic pressure:  $10^9$  Pa

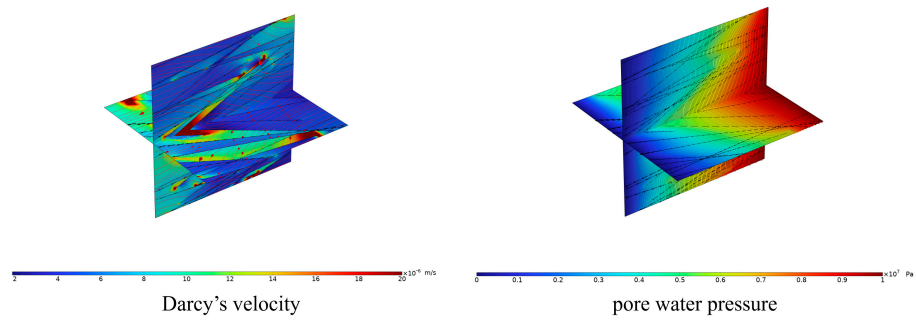


**Figure.S2** Darcy velocity and pore pressure cross-section diagrams under different water pressure conditions

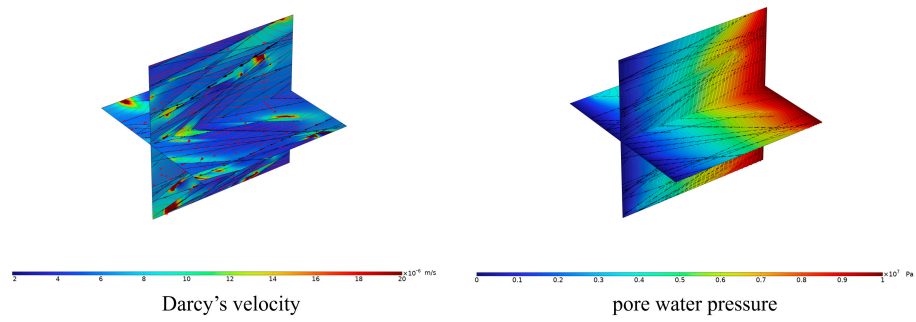
Fracture density :0.0025/m<sup>3</sup>



Fracture density :0.0050/m<sup>3</sup>

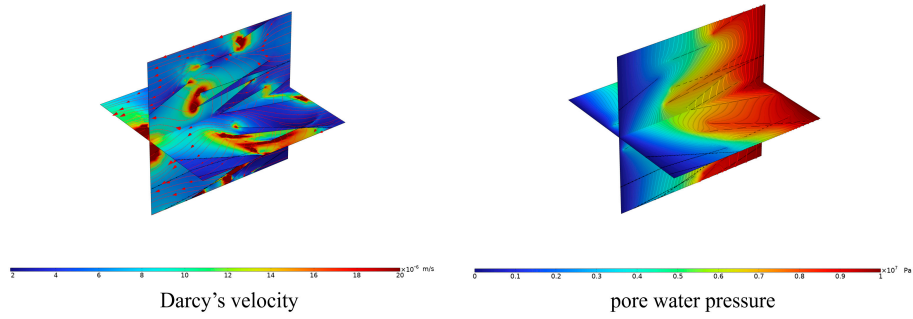


Fracture density :0.0075/m<sup>3</sup>

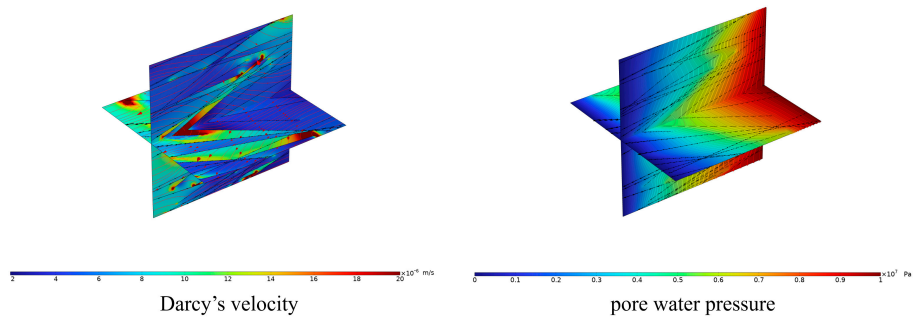


**Figure.S3** Darcy velocity cross-section and pore water pressure cross-section under different fracture densities

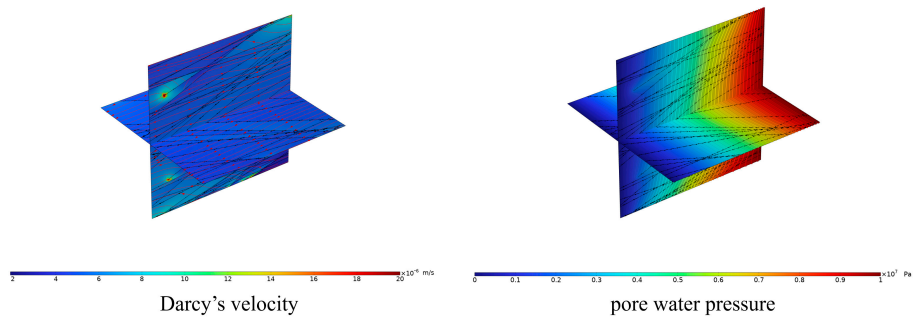
Length of Fracture:5.5-10m



Length of Fracture:11-20m



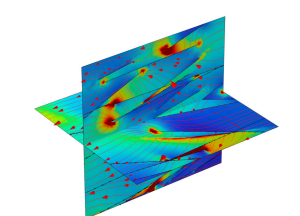
Length of Fracture:16.5-30m



**Figure.S4** Darcy velocity cross-section and pore water pressure cross-section under different fracture lengths

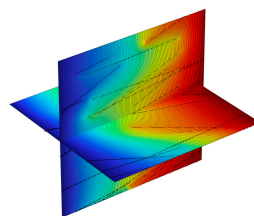


fracture length ratio:0.25



0 2 4 6 8 10 12 14 16 18 20  $\times 10^{-6}$  m/s

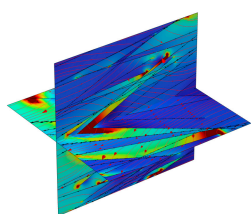
Darcy's velocity



0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1  $\times 10^7$  Pa

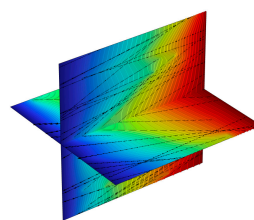
pore water pressure

fracture length ratio:0.55



0 2 4 6 8 10 12 14 16 18 20  $\times 10^{-6}$  m/s

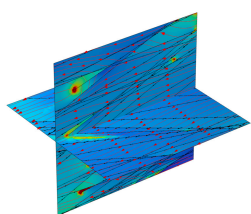
Darcy's velocity



0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1  $\times 10^7$  Pa

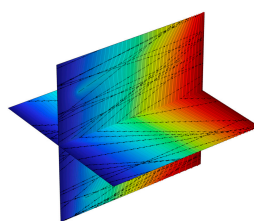
pore water pressure

fracture length ratio:0.85



0 2 4 6 8 10 12 14 16 18 20  $\times 10^{-6}$  m/s

Darcy's velocity

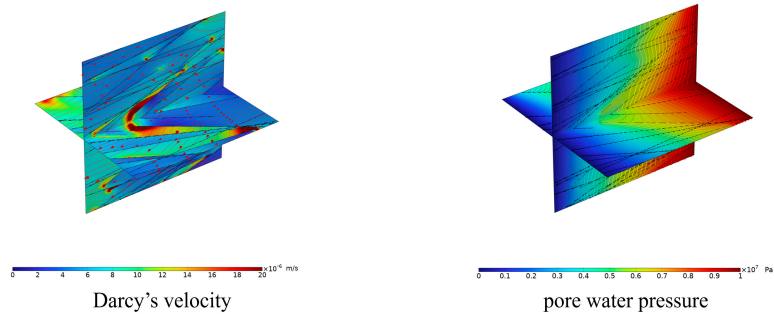


0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1  $\times 10^7$  Pa

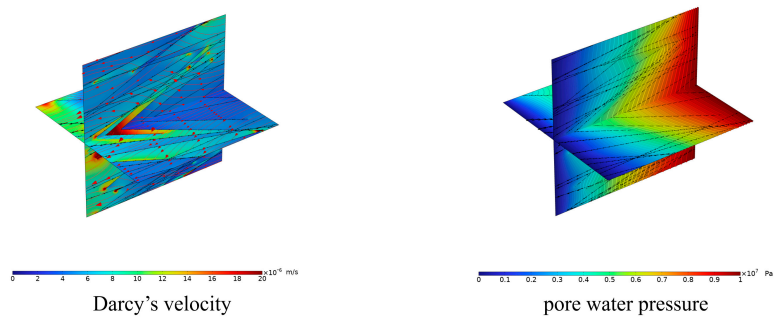
pore water pressure

**Figure.S5** Darcy velocity cross-section and pore water pressure cross-section under different fracture length ratios

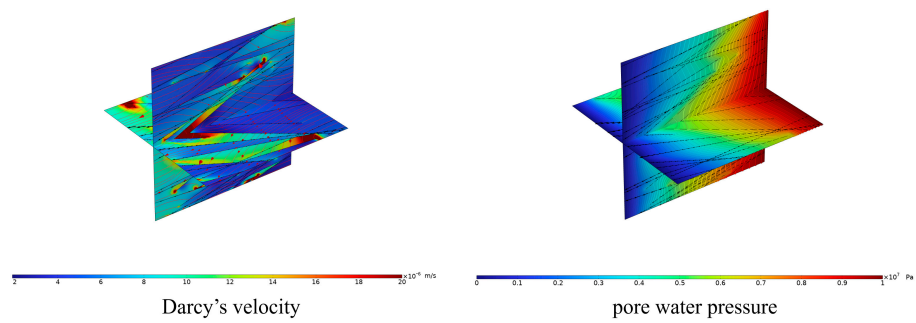
fracture length power law:2



fracture length power law:5

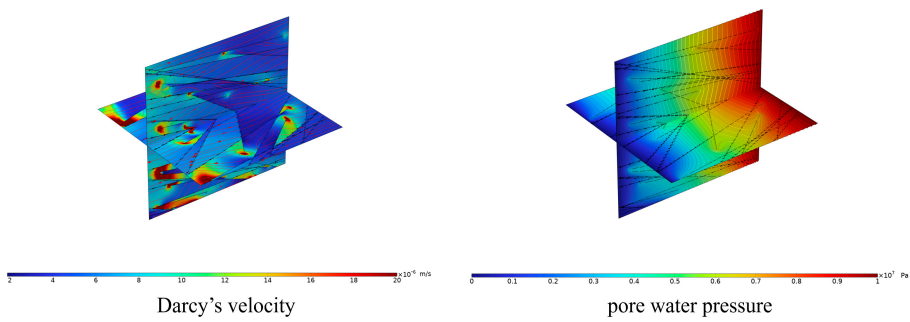


fracture length power law:8

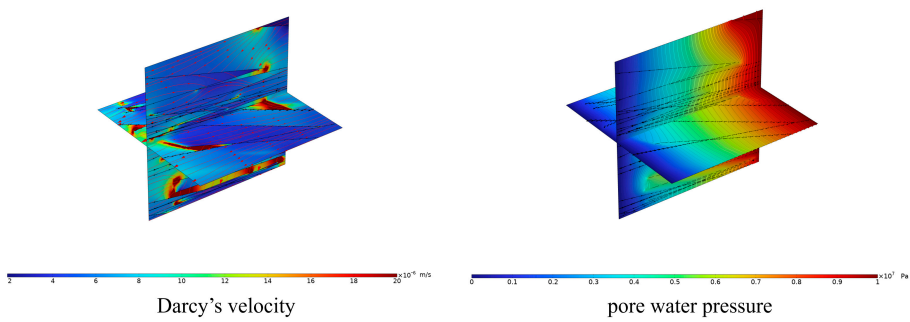


**Figure.S6** Darcy velocity cross-section and pore water pressure cross-section under different fracture length power law

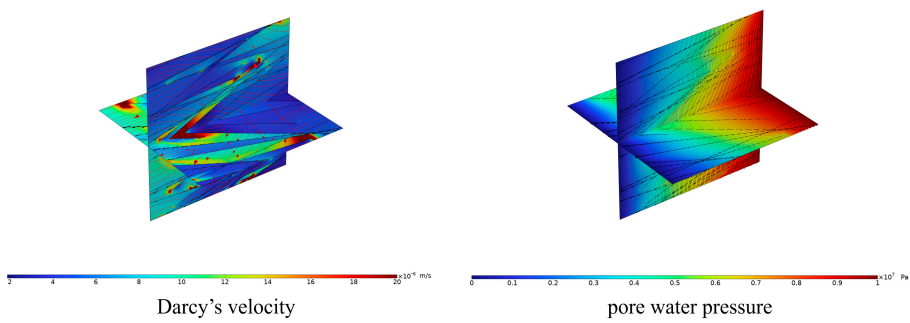
fracture Strike: 0° fracture Dip: 45°



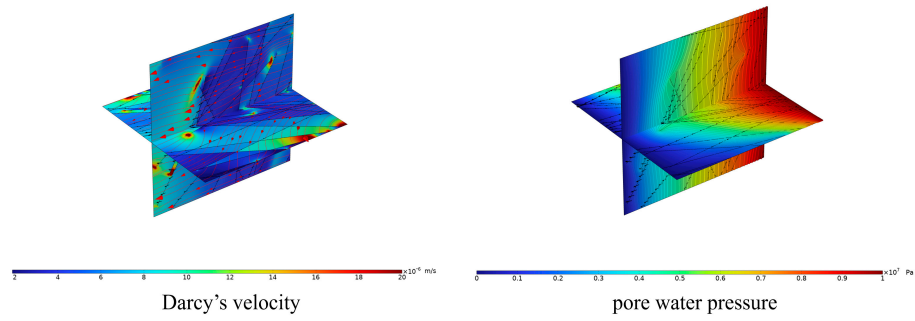
fracture Strike: 45° fracture Dip: 0°



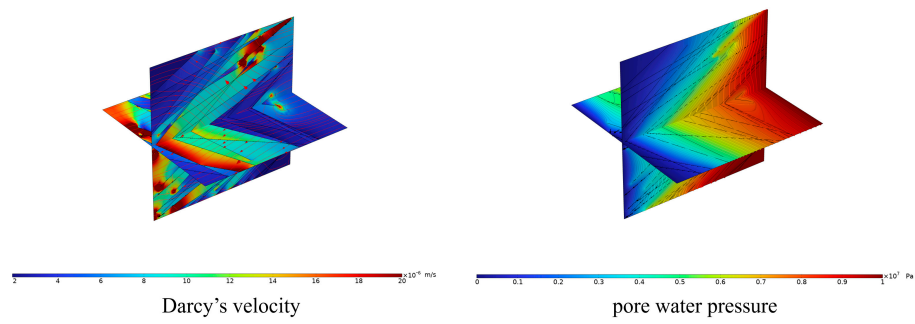
fracture Strike: 45° fracture Dip: 45°



fracture Strike:  $45^\circ$  fracture Dip:  $90^\circ$

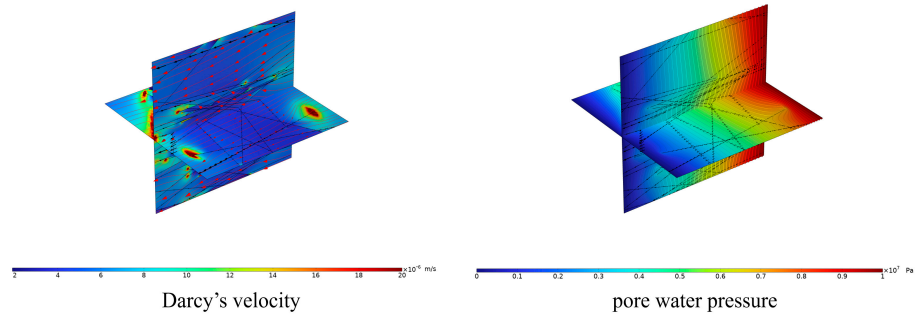


fracture Strike:  $90^\circ$  fracture Dip:  $45^\circ$

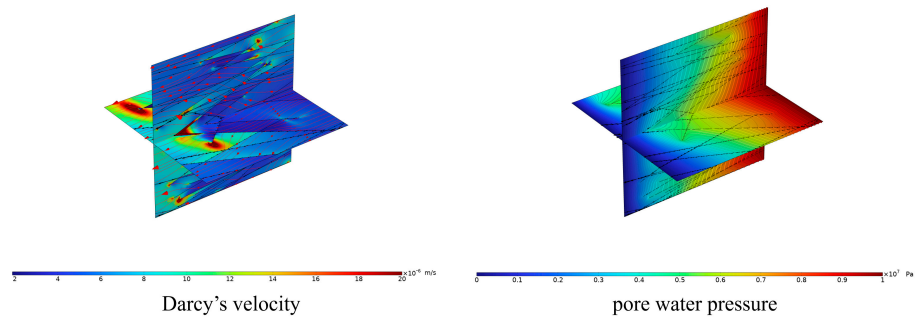


**Figure.S7** Darcy velocity cross-section and pore water pressure cross-section under different strike and dip of fracture angles

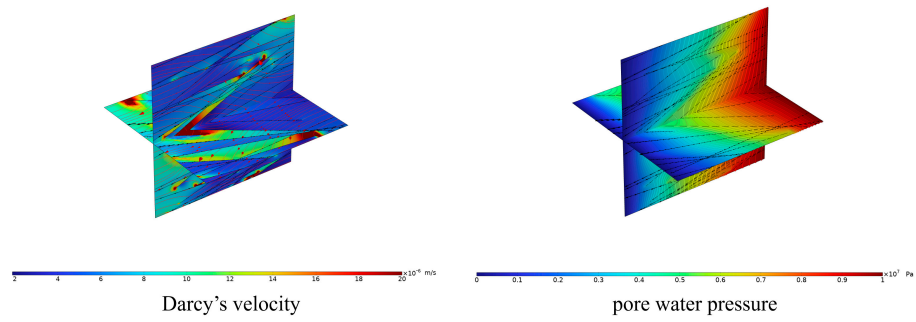
dispersion coefficient: 0.1



dispersion coefficient: 4.075

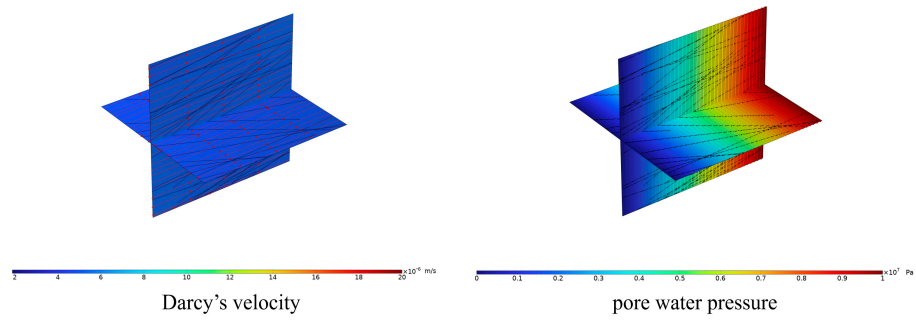


dispersion coefficient: 8.05

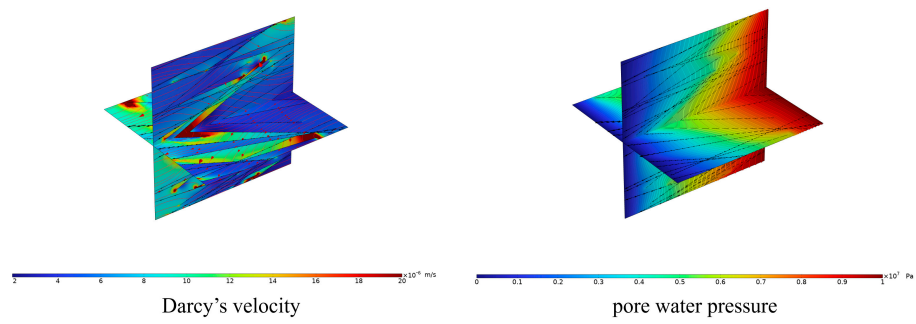


**Figure.S8** Darcy velocity cross-section and pore water pressure cross-section under different fracture dispersion coefficients

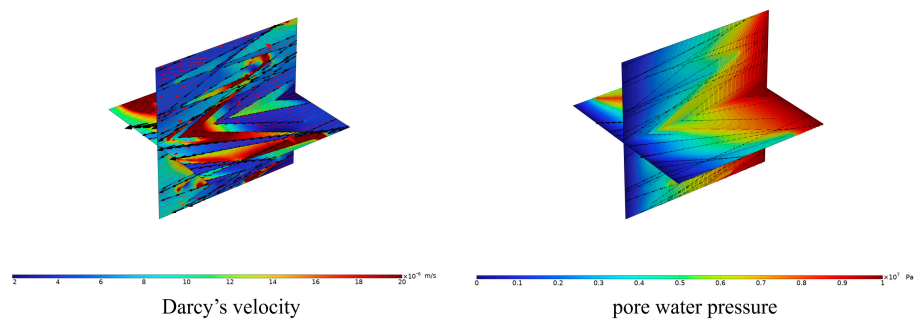
Fracture Aperture: 0.01-0.06mm



Fracture Aperture: 0.1-0.6mm

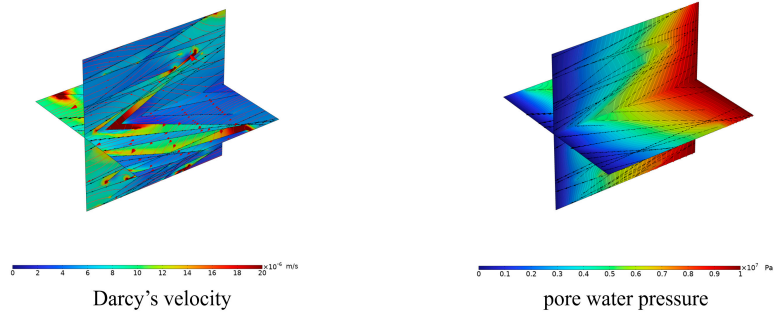


Fracture Aperture: 1-6mm

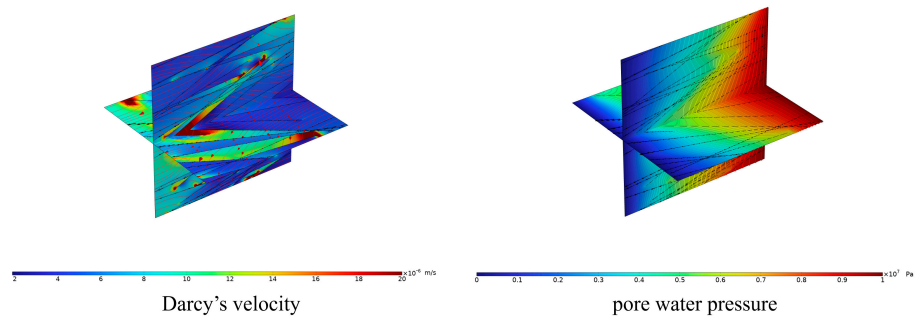


**Figure.S9** Darcy velocity cross-section and pore water pressure cross-section under different fracture Aperture

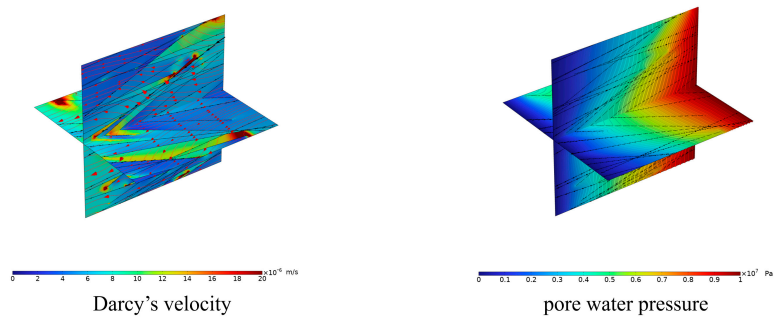
Aperture ratio: 3



Aperture ratio: 6

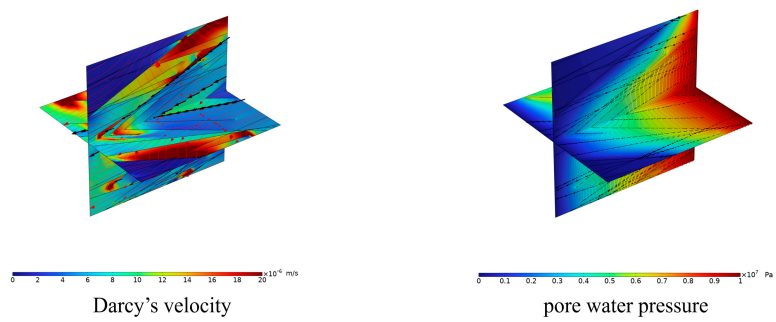


Aperture ratio: 9

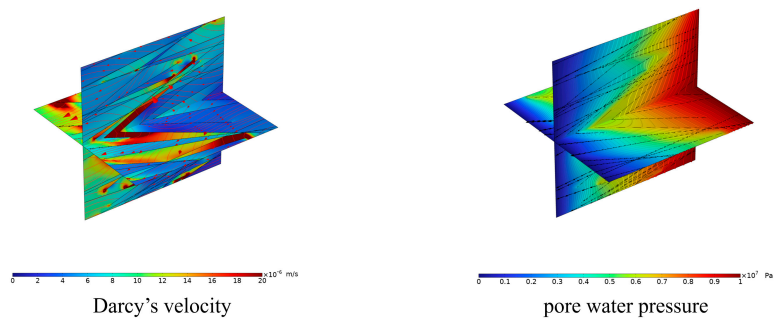


**Figure.S10** Darcy velocity cross-sectional map and pore water pressure cross-sectional map under different aperture ratio

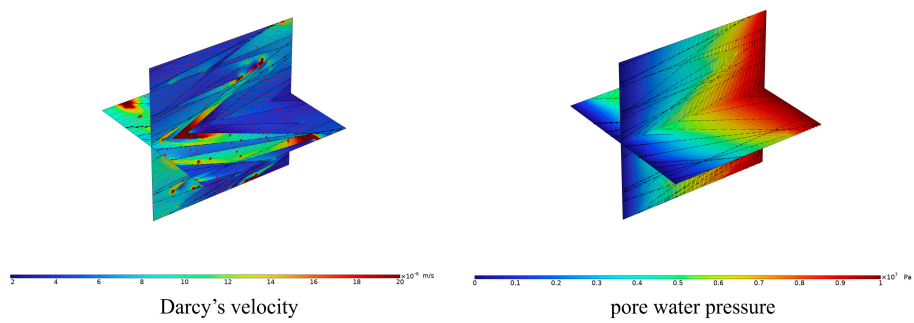
Aperture power law: 2



Aperture power law: 8



Aperture power law: 14



**Figure.S11** Darcy velocity cross-sectional map and pore water pressure cross-sectional map under different fracture aperture power law

**Table.S1** ANOVA for Quadratic model



**Response 1: K**

Transform: Base 10 Log

Constant: 0

Source	Sum of Squares	df	Mean Square	F-value	p-value
<b>Model</b>	11.96	44	0.2718	54.56	< 0.0001 significant
A-fracture length	1.93	1	1.93	387.50	< 0.0001
B-fracture length ratio	4.31	1	4.31	864.59	< 0.0001
C-fracture length power law	0.0812	1	0.0812	16.29	0.0002
D- Strike	0.0296	1	0.0296	5.94	0.0190
E-Dip	0.6894	1	0.6894	138.36	< 0.0001
F-dispersion coefficient	0.0798	1	0.0798	16.01	0.0002
G-Aperture ratio	0.0045	1	0.0045	0.9131	0.3445
H-Aperture power law	0.5276	1	0.5276	105.90	< 0.0001
AB	0.1097	1	0.1097	22.02	< 0.0001
AC	0.0057	1	0.0057	1.14	0.2908
AD	0.0166	1	0.0166	3.34	0.0744
AE	0.0017	1	0.0017	0.3395	0.5631
AF	0.0049	1	0.0049	0.9755	0.3287
AG	0.0086	1	0.0086	1.73	0.1955
AH	0.0196	1	0.0196	3.93	0.0537
BC	0.1135	1	0.1135	22.79	< 0.0001
BD	0.0189	1	0.0189	3.79	0.0579
BE	0.0038	1	0.0038	0.7622	0.3874
BF	0.0166	1	0.0166	3.33	0.0749
BG	0.0120	1	0.0120	2.40	0.1286
BH	6.789E-07	1	6.789E-07	0.0001	0.9907
CD	0.0001	1	0.0001	0.0163	0.8991
CE	0.0308	1	0.0308	6.18	0.0168
CF	0.0055	1	0.0055	1.09	0.3011
CG	0.0000	1	0.0000	0.0040	0.9502
CH	0.0240	1	0.0240	4.81	0.0337
DE	0.0419	1	0.0419	8.41	0.0058
DF	0.0044	1	0.0044	0.8869	0.3514
DG	0.0000	1	0.0000	0.0071	0.9334

DH	0.0173	1	0.0173	3.47	0.0690
EF	0.0115	1	0.0115	2.31	0.1355
EG	0.0002	1	0.0002	0.0353	0.8519
EH	0.0066	1	0.0066	1.32	0.2561
FG	0.0029	1	0.0029	0.5898	0.4466
FH	0.0000	1	0.0000	0.0037	0.9517
GH	0.0047	1	0.0047	0.9410	0.3373
A <sup>2</sup>	1.55	1	1.55	311.72	< 0.0001
B <sup>2</sup>	0.7761	1	0.7761	155.77	< 0.0001
C <sup>2</sup>	0.0050	1	0.0050	1.01	0.3196
D <sup>2</sup>	0.0903	1	0.0903	18.12	0.0001
E <sup>2</sup>	0.0383	1	0.0383	7.68	0.0082
F <sup>2</sup>	0.0546	1	0.0546	10.95	0.0019
G <sup>2</sup>	0.0081	1	0.0081	1.62	0.2104
H <sup>2</sup>	0.0265	1	0.0265	5.33	0.0258
<b>Residual</b>	0.2192	44	0.0050		
Lack of Fit	0.2192	35	0.0063		
Pure Error	0.0000	9	0.0000		
<b>Cor Total</b>	12.18	88			

Factor coding is **Coded**.

Sum of squares is **Type III - Partial**

The **Model F-value** of 54.56 implies the model is significant. There is only a 0.01% chance that an F-value this large could occur due to noise.

**P-values** less than 0.0500 indicate model terms are significant. In this case A, B, C, D, E, F, H, AB, BC, CE, CH, DE, A<sup>2</sup>, B<sup>2</sup>, D<sup>2</sup>, E<sup>2</sup>, F<sup>2</sup>, H<sup>2</sup> are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. If there are many insignificant model terms (not counting those required to support hierarchy), model reduction may improve your model.

#### Table.S2 Fit Statistics

<b>Std. Dev.</b>	0.0706	<b>R<sup>2</sup></b>	0.9820
<b>Mean</b>	-12.06	<b>Adjusted R<sup>2</sup></b>	0.9640
<b>C.V. %</b>	0.5855	<b>Predicted R<sup>2</sup></b>	0.9084
<b>Adeq Precision</b>		43.0790	

The **Predicted  $R^2$**  of 0.9084 is in reasonable agreement with the **Adjusted  $R^2$**  of 0.9640; i.e. the difference is less than 0.2.

**Adeq Precision** measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 43.079 indicates an adequate signal. This model can be used to navigate the design space.