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Optimization of Microwave Coupled Hot Air Drying for Chinese Yam Using Response Surface Methodology

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Abstract: The effect of microwave coupled hot air drying on rehydration ratio (RR) and total sugar content (TSC) of Chinese yam was investigated. Single factor test and response surface methodology were used for process parameter optimization with hot air temperature, hot air velocity, slice thickness, and microwave power density as variables and RR and TSC of dried products as responses. The effect of variables on RR followed the order: slice thickness > hot air temperature > microwave power density > hot air velocity. The effect of variables on TSC followed the order: slice thickness > microwave power density > hot air velocity > hot air temperature. The optimized process parameters were hot air velocity of 2.5 m/s, hot air temperature of 61.7 °C, slice thickness of 8.5 mm, and microwave power density of 5.9 W/g. Under the optimal conditions, the predicted values of RR and TSC were 1.90 g/g and 5.74 g/100 g, respectively, which is very close to corresponding actual values (1.83 g/g and 5.72 g/100 g). The desirability of 0.913 further validated the effectiveness of the model. The findings from this work may apply to other agricultural products.

Keywords: Chinese yam; microwave coupled hot air; process optimization; rehydration ratio; total sugar content

1. Introduction

Chinese yam is an edible food and also an herbal medicinal ingredient [1,2]. Chinese yam contains starch, protein, polysaccharides, dopamine, flavonoids, amino acids, allantoin, trace elements, and other active ingredients. Chinese yam has functions on prevention and treatment of diabetes and digestive system diseases as well as the improvement of human immune system [3,4]. However, same as other vegetables and fruits, fresh Chinese yam is easily damaged during the harvest and transportation because of its crispness and high moisture content, which shortens its shelf life. Fresh Chinese yam also easily gets molded during room temperature storage due to high moisture content, which causes a large amount of nutritional ingredients to be lost and thus lowers its quality and dietary properties [5,6]. To address these issues, drying is usually used to reduce the moisture content lower than a certain threshold value [7]. Dried yam can be used as an important component in Chinese traditional medicine or important ingredients in various food products such as candies, cakes, and soft drinks. However, the drying process can cause severe chemical and physical changes in the properties of dried materials. As a result, choosing a proper method is very important for drying of Chinese yam.

Recently, many drying methods for fruits and vegetables have been reported such as far-infrared radiation assisted freeze drying [5], hot air drying [2], far-infrared radiation and heat pump drying [8,9],

microwave freeze drying, microwave vacuum drying [10], and freeze drying, among which hot air drying is the most commonly applied for the postharvest preservation of Chinese yam and other agricultural products because of its simple processing and low-cost equipment. However, during hot air drying, the direction of heat transfer (from the surface of drying materials to the interior) is opposite to that of water transfer, which results in low heat transfer rate, long drying period, and high energy cost [11]. These disadvantages not only affect the color, flavor, texture, taste, and nutrients of dried materials but also reduce the density and water absorbance ability of dried products and the shift of solutes from the interior to the surface [12]. Compared to hot air drying, microwave drying technology is another method that has been widely used to dry various vegetables and fruits because of its high energy efficiency and high drying rate [13,14]. It is applicable for the drying of fruit and vegetable products especially with high moisture content (e.g., grape, carrot, and apple). Microwave drying is a volumetric drying method which can enhance heat transfer. In the drying process, the electromagnetic energy with high frequency is absorbed and directly transformed into kinetic energy of water molecules. The interior heat generated by “molecular friction” within the materials leads to water evaporation and subsequently creates a pressure environment with the pressure decreasing from the interior of drying materials to the surface. Thus, the pressure gradient can greatly speed up the drying process, shorten drying period, and improve energy efficiency [13,15]. Nevertheless, microwave drying is well known to cause non-uniform heating. The local temperature, especially along the edge and corner, can easily rise to a high level if not properly applied, resulting in gelatinization and off-flavor. In addition, the rapid moisture loss and mass transfer caused by microwave power may lead to the poor quality or the unfavorable structural changes such as puffing [16]. Based on the above analysis, the combination of microwave drying and hot air drying could be a great option to overcome the shortcomings associated with individual microwave drying and hot air drying.

The combination of hot air and microwave can not only reduce the drying time but also improve the final quality of food products. The combination has two forms: one is applying hot air and microwave drying in stages; the other, named as microwave coupled with hot air (MWHHA), simultaneously uses the two methods and has been considered as an innovative technique for drying fruits and vegetables [17]. In the MWHHA drying process, microwave energy absorbed by the drying materials is directly transformed into heat which can go throughout the drying materials. The moisture is driven by the volumetric heating, traveling from the inside of the drying materials to the surface, and then continuously evaporated by the moving hot air [18]. Therefore, the moisture removal of drying materials is affected by the interaction of hot air and microwave in the MWHHA drying process. In the past few years, some studies using the combination of hot air and microwave have been reported for drying food products including soybean [19], potato [20], longan [21], and orange peel [22]. However, up to date, no report has been found on the drying of Chinese yam using MWHHA.

Response surface methodology (RSM) has been widely employed to optimize and improve various processes. In multifactor tests, RSM is frequently employed to determine the interactions among tested variables as well as their influence ranges, and regression equations are employed to describe the effects of variables on the response [23–25]. Using this approach, a process or system can be efficiently explored. Therefore, RSM has been successfully applied to optimize the drying processes of okra [26], frozen sour cherries [27], hawthorn [28], quince [24], and olive leaves [25]. In this research, the process optimization of MWHHA drying for Chinese yam was investigated using RSM.

The objectives of this research were to determine the main effects of process variables (slice thickness, hot air temperature, microwave power density, and hot air velocity) on the quality of dried Chinese yam as well as to optimize the process parameters during MWHHA drying.

2. Materials and Methods

2.1. Materials

Fresh Chinese yams with similar shapes and sizes and initial moisture content of 78% (wet basis) were purchased from a local supermarket. For initial moisture content measurement, the fresh Chinese yams were sliced to a thickness of 11 mm and then dried using air-forced oven at 70 °C for 12 h [28]. All of the tested Chinese yams were free of disease, mechanical damage, and decay. After being washed and drained, the samples were cut into the designated thicknesses, put into plastic bags, and stored in a freezer at 4 ± 0.5 °C.

2.2. Experimental Apparatus

The MWAH dryer (YHMH900-100) used for this study was fabricated by the Heilongjiang Bayi Agricultural University (Daqing, China) (Figure 1).

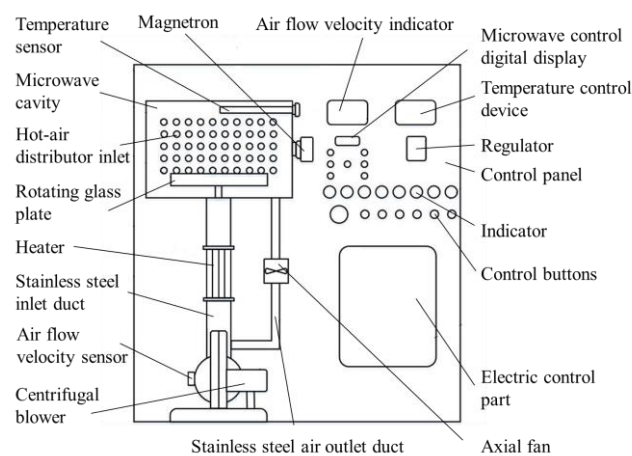


Figure 1. Schematic diagram of microwave coupled with hot air (MWAH) dryer.

The MWAH dryer which can be found in our previous paper mainly contains two drying systems: hot air and microwave [28]. In the hot-air drying system, the hot air velocity and hot air temperature are in the ranges of 0–5 m/s and 30–100 °C, respectively. The microwave input power of the microwave drying system is 1300 W, and the output power can be adjusted to 180–900 W with the interval of 180 W. The drying time can be controlled in the range of 0–180 min.

The mass change of the tested samples was measured using a digital balance (American Twin Brothers Co. Ltd., model T100, Shanghai, China) with a precision of 0.01 g.

2.3. Experimental Procedure

Fresh yams were cut into designated thicknesses with an approximately 60 mm diameter using a shelf-style sharp food slicer. Before each test, the hot air drying system was run 10–20 min to stabilize the hot air in microwave cavity at target temperature. The yam slices with the required thicknesses and weights were distributed uniformly on a plastic tray in the manner of thin layer, followed by putting into the microwave cavity and starting the microwave drying system. The tested sample weight was measured every 60 s during the drying process. Once the moisture content of dried Chinese yam slices reached around 8.0% (dry basis), the drying process was terminated. All experiments were conducted in triplicate. Dried samples were cooled down under ambient temperature for 10 min, followed by packing into plastic bags and storing in a freezer at 4 ± 0.5 °C for rehydration ratio (RR) and total sugar content (TSC) evaluation.

2.4. Determination of RR

RR, which represents the physical and chemical changes of dried products and capacity of being rehydrated before their final use, was evaluated by soaking 10 g of the dried Chinese yam slices in 300 mL of distilled water at 80 °C for 20 min [29]. After soaking, superficial water was removed by placing the samples on a fiber glass wire mesh for 3 min and then the samples were weighed. RR was calculated using Equation (1) [30,31]:

$$RR = \frac{W_1 - W_2}{W_2} \quad (1)$$

where RR is the rehydration ratio of the dried yam slices, g/g; W_1 is the weight of the sample after rehydration, g; W_2 is the weight of the sample before rehydration, g.

2.5. Determination of TSC

TSC was measured according to GB/T 10782-2006 [32]. After milling to fine powders, 10 g of each dried yam was soaked in 200 mL of distilled water for 2 h. The slurries were transferred in 250 mL volumetric flasks and then diluted to 250 mL. After that, the slurries were filtered to collect the filtrates. Ten milliliter of each filtrate, 30 mL of distilled water, 5 mL of hydrochloric acid (37%, v/v) were loaded in 250 mL flasks, heated to 68–70 °C and kept for 10 min, and then cooled down to room temperature. The filtrates were transferred in 250 mL volumetric flasks, followed by the addition of 2 drops of methyl red indicator (0.001 g/L). The filtrates were then neutralized by sodium hydroxide (0.3 g/L) and diluted to 250 mL. The neutralized filtrates were individually used to titrate the standard Fehling reagent (10 mL) and the consumed volumes of the filtrates were recorded to calculate TSC using Equation (2) [33]:

$$TSC = \frac{A \times 6250}{W_3 \times V} \times 100 \quad (2)$$

where TSC is total sugar content in the sample, g/100 g; 6250 is the dilution ratio; W_3 is the weight of the sample, g; A is 10 mL of Fehling reagent that equals to the glucose quality, g; V is the volume of the test solution consumed during the titration, mL.

2.6. Experimental Design, Statistical Analysis, and Optimization

In this study, process variables slice thickness (S_t), hot air velocity (H_v), hot air temperature (H_t), and microwave power density (M_d) were represented with codes x_1 , x_2 , x_3 , and x_4 . Single factor experiments were first conducted to determine the rational ranges of variables in preparation for RSM experiments. The process variables and levels used in single factor experiments are shown in Table 1.

Table 1. Variables and levels in single factorial design.

Variables	Levels							
Slice Thickness/ S_t (mm)	4.0	6.0	8.0	10.0	12.0	14.0	16.0	
Hot air velocity/ H_v (m/s)	1.5	2.0	2.5	3.0	3.5	4.0	4.5	
Hot air temperature/ H_t (°C)	45.0	50.0	55.0	60.0	65.0	70.0	75.0	
Microwave power density/ M_d (W/g)	3.0	4.0	5.0	6.0	7.0	8.0	9.0	

Based on the results from single factor experiments, the relative contributions of variables to the responses RR and TSC were determined using RSM. A central composite rotatable design was employed to investigate the optimal conditions of MWHA drying process, and 31 experiments with 7 replicates at the center point were carried out. The experimental variables and levels used in the RSM design are listed in Table 2.

Table 2. The independent variables and levels for the Response surface methodology (RSM) design.

Independent Variables	Symbols	Levels				
		−2	−1	0	+1	+2
Slice thickness/ S_t (mm)	x_1	6.0	8.0	10.0	12.0	14.0
Hot-air velocity/ H_v (m/s)	x_2	1.5	2.0	2.5	3.0	3.5
Hot-air temperature/ H_t (°C)	x_3	50.0	55.0	60.0	65.0	70.0
Microwave power density/ M_d (W/g)	x_4	2.0	4.0	6.0	8.0	10.0

Due to the extraneous factors, all of the experiments were randomized with the purpose of minimizing the effects of unexplained variability on the observed responses. The experimental data was analyzed using a statistical software Design Expert with the version of 8.0.5b, and RSM was performed to obtain 3D surface graphs between variables and response.

The following second-order polynomial of Equation (3) was applied to fit the experimental data [34,35]:

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i < j=1}^k \beta_{ij} x_i x_j \quad (3)$$

where y values are investigated responses (RR and TSC); β_0 , β_i , β_{ii} , and β_{ij} are constant regression coefficients of intercept, linear, quadratic, and interaction terms, respectively; x_i and x_j are the coded independent variables.

At the significance level of $p = 0.05$, the analysis of variance (ANOVA) was used to statistically test the experimental results. In addition, p value and the coefficient of determination (R^2) was employed to evaluate the adequacy of the model [36].

Several response variables are normally optimized to describe the system performance and quality characteristics during the optimization of various industrial processes. Some of these response variables require being minimized while others require being maximized. Under certain circumstances, these response variables are competitive, that is, when changing one response, the opposite effect may yield on another one, which makes the situation more complicated. Usually, three ways can be employed to solve the problem. Desirability function is the most common method to solve the problem [25].

Specific steps for optimizing the desirable functions are as following: (1) making response variables dimensionless, (2) determining weighting coefficient, (3) constructing desirability function and solution, (4) optimizing the model using the fuzzy similar preceding ratio method [37].

In this work, desirability function was developed with maximizing RR and TSC as the criteria.

3. Results and Discussion

3.1. Single Factorial Experiment

3.1.1. Effects of Independent Variables on RR

The effects of process variables (S_t , H_v , H_t , and M_d) on RR of dried yam products are shown in Figure 2. RR increased first and then decreased when the slice thickness is 10 mm, microwave power density is 6 W/g, and the velocity and temperature of hot air are 2.5 m/s and 60 °C, respectively. Based on the results, the value ranges of process variables that are suitable for the RSM can be confirmed as slice thickness of 8–12 mm, hot-air velocity and temperature of 2.0–3.0 m/s and 55–65 °C, and microwave power density of 5–7 W/g with the principle of maximizing RR.

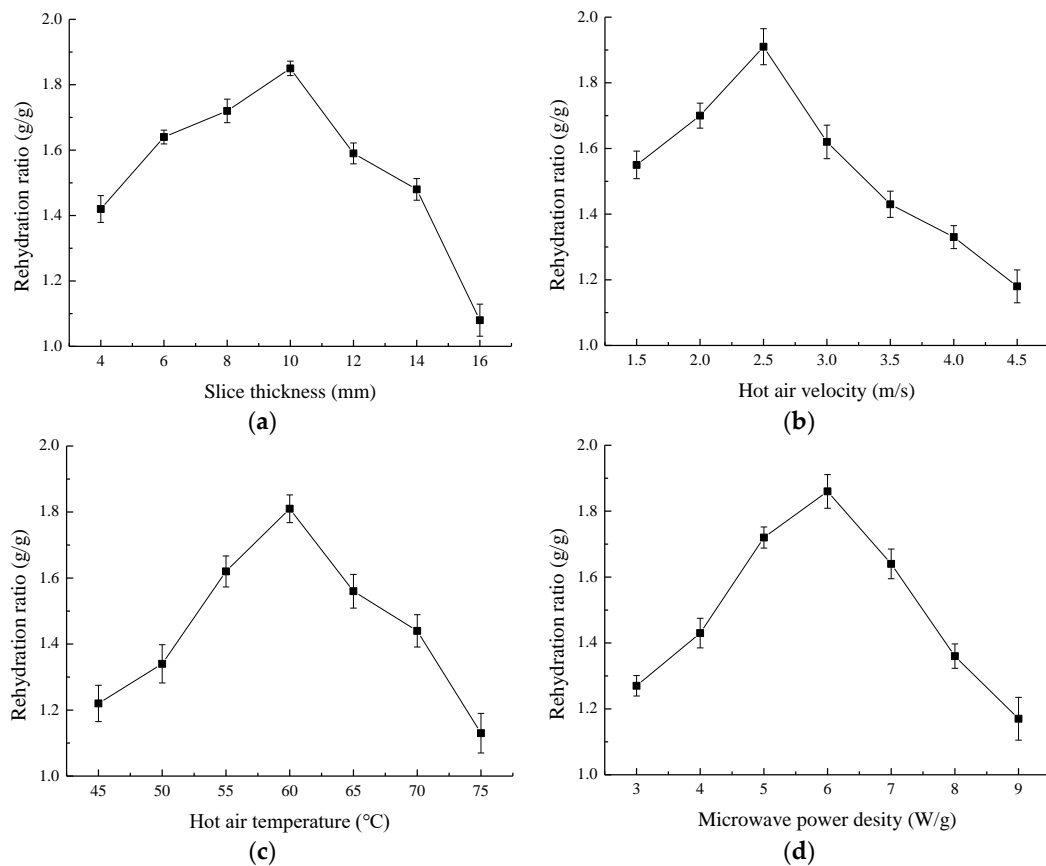


Figure 2. The effects of independent variables on rehydration ratio (RR). (a) Effect of slice thickness of yam slices on RR; (b) Effect of hot air velocity on RR; (c) Effect of hot air temperature on RR; (d) Effect of microwave power density on RR.

3.1.2. Effects of Independent Variables on TSC

The effects of process variables on TSC of dried yam products are shown in Figure 3. TSC decreased as slice thickness increased. However, TSC increased first and then decreased at the hot air temperature of 60 °C, microwave power density of 6 W/g, and hot air velocity of 2.5 m/s. Consequently, according to the criteria of maximizing TSC, the rational value ranges of process variables for the RSM can be identified as slice thickness of more than 4 mm, microwave power density of 5–7 W/g, hot-air velocity and temperature of 2.0–3.0 m/s and 55–65 °C, respectively.

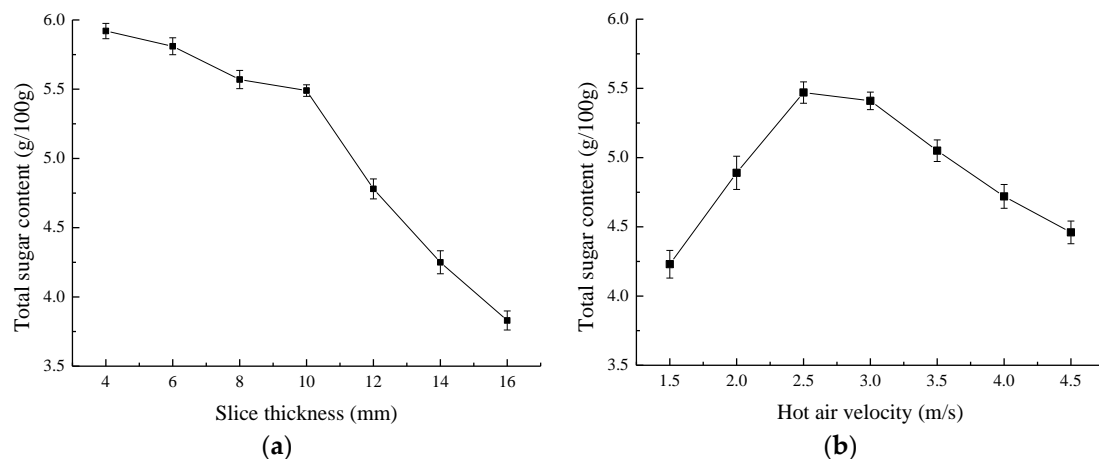


Figure 3. Cont.

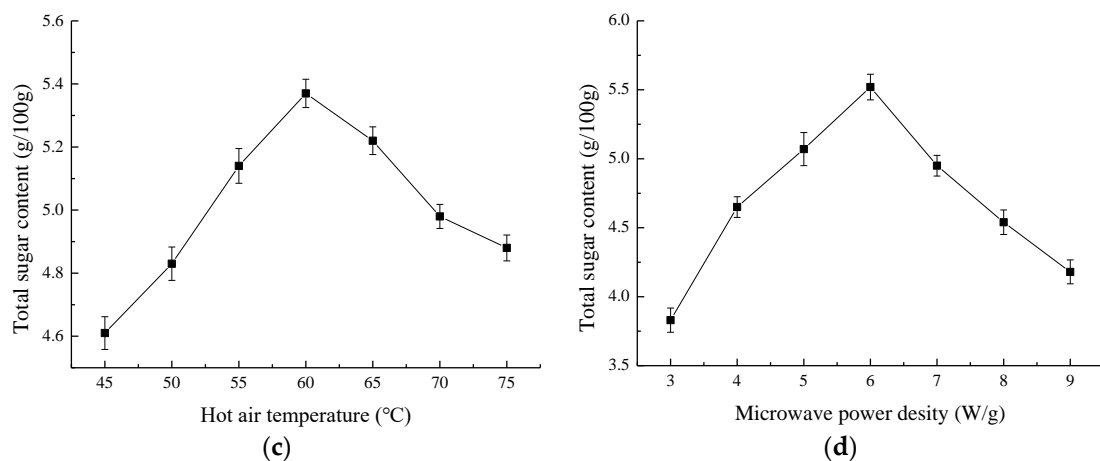


Figure 3. The effects of independent variables on total sugar content (TSC). (a) Effect of slice thickness of yam slices on TSC; (b) Effect of hot-air velocity on TSC; (c) Effect of hot-air temperature on TSC; (d) Effect of microwave power density on TSC.

Based on the comprehensive consideration regarding the single factor experiment results, the values of process variables at zero level for RSM were finally determined to be slice thickness of 10 mm, microwave power density of 6 W/g, hot air velocity and temperature of 2.5 m/s and 60 °C, respectively.

3.2. RSM Experiment

Experimental design of RSM is listed in Table 3. By conducting ANOVA, the significant effects of all process variables on each response was determined and the experimental data was fitted to second-order polynomial models (Table 4).

Table 3. Experimental design and RR and TSC values from response surface analysis.

Run	Variable Levels				RR, y_1 (g/g)	TSC, y_2 (g/100g)
	x_1	x_2	x_3	x_4		
1	-1	-1	-1	-1	1.57	4.25
2	1	-1	-1	-1	1.24	3.75
3	-1	1	-1	-1	1.21	5.01
4	1	1	-1	-1	1.02	4.12
5	-1	-1	1	-1	1.82	4.87
6	1	-1	1	-1	1.56	4.03
7	-1	1	1	-1	1.65	5.19
8	1	1	1	-1	1.31	4.52
9	-1	-1	-1	1	1.33	5.17
10	1	-1	-1	1	1.02	4.13
11	-1	1	-1	1	1.22	5.43
12	1	1	-1	1	1.02	4.39
13	-1	-1	1	1	1.34	5.48
14	1	-1	1	1	1.18	4.52
15	-1	1	1	1	1.25	5.55
16	1	1	1	1	1.16	4.61
17	-2	0	0	0	1.52	5.89
18	2	0	0	0	1.01	3.75
19	0	-2	0	0	1.55	4.25
20	0	2	0	0	1.33	5.02
21	0	0	-2	0	1.26	4.86

Table 3. Cont.

Run	Variable Levels				RR, y_1 (g/g)	TSC, y_2 (g/100g)
	x_1	x_2	x_3	x_4		
22	0	0	2	0	1.43	4.95
23	0	0	0	-2	1.18	3.65
24	0	0	0	2	1.16	4.13
25	0	0	0	0	1.96	5.69
26	0	0	0	0	2.01	5.52
27	0	0	0	0	1.83	5.29
28	0	0	0	0	1.84	5.61
29	0	0	0	0	1.79	5.45
30	0	0	0	0	1.92	5.39
31	0	0	0	0	1.85	5.22

Table 4. ANOVA evaluation of linear, quadratic, and interaction terms for each response variable and coefficient of prediction models.

Source	df	RR			TSC		
		Coefficient	Sum of Squares	p -Value	Coefficient	Sum of Squares	p -Value
Model	14	1.89	2.79	<0.0001	5.45	12.08	<0.0001
x_1	1	-0.12	0.35	<0.0001	-0.47	5.19	<0.0001
x_2	1	-0.069	0.11	0.0024	0.17	0.72	0.0002
x_3	1	0.082	0.16	0.0006	0.11	0.3	0.0075
x_4	1	-0.079	0.15	0.0008	0.19	0.84	0.0001
x_1x_2	1	0.015	0.0036	0.5331	-0.013	0.0025	0.7848
x_1x_3	1	0.011	0.002	0.6392	0.00375	0.000225	0.9346
x_1x_4	1	0.023	0.0081	0.3535	-0.068	0.073	0.1532
x_2x_3	1	0.01	0.0016	0.6767	-0.043	0.029	0.3592
x_2x_4	1	0.049	0.038	0.0549	-0.079	0.099	0.0994
x_3x_4	1	-0.06	0.058	0.0215	-0.028	0.012	0.5499
x_1^2	1	-0.15	0.69	<0.0001	-0.14	0.54	0.0009
x_2^2	1	-0.11	0.35	<0.0001	-0.18	0.96	<0.0001
x_3^2	1	-0.13	0.52	<0.0001	-0.12	0.38	0.0033
x_4^2	1	-0.18	0.91	<0.0001	-0.37	3.91	<0.0001
Residual	16		0.14			0.52	
Lack of fit	10		0.1	0.2779		0.35	0.4169
Pure error	6		0.038			0.17	
Total	30		2.93			12.6	
R^2		0.9516			0.9588		
CV/%		6.55			3.73		

Note: CV means coefficient of variation.

Table 4 indicates that the two regression models for RR and TSC were observed to be statistically significant at 1% level of significance ($p \leq 0.01$), indicating that the experimental data were consistent with the second-order polynomial response surface models and the predicted models y_1 and y_2 could well fit the actual situation. The R^2 values of the two prediction models were 0.9516 and 0.9588 for RR and TSC, respectively, demonstrating that the experimental values can be reasonably represented by the prediction models. Therefore, the responses could be sufficiently explained by the models [38]. Meanwhile, the values of coefficient of variation (CV) were 6.55% for RR and 3.73% for TSC, which are less than 10%, indicating that the variation of the test values was within a rational range [39]. Table 4 also shows that the p -values of the lack of fit were 0.2779 and 0.4169, which were not statistically significant at 5% level, indicating that the prediction models were adequately accurate for predicting these responses.

3.2.1. Analysis of RR

RR was in the range of 1.01–2.01 g/g under various conditions (Table 3). According to ANOVA results (Table 4), all of the drying parameters (S_t , H_v , H_t , and M_d) had extremely significant effects on RR ($p \leq 0.01$). The p -values of variables indicate that slice thickness had the most effect on RR, followed by hot air temperature, microwave power density, and hot air velocity. Thus, slice thickness was a major factor that influenced the rehydration attribute of dried yam slices. However, the effects of all the interaction terms on RR were not statistically significant ($p \geq 0.05$) except for the interaction effect of hot air temperature and microwave power density at statistical level of $p \leq 0.05$. The quadratic level of all the process variables had significant effects on RR at statistical level of $p \leq 0.01$. By removing the statistically insignificant items of x_1x_2 , x_1x_3 , x_1x_4 , x_2x_3 , x_2x_4 at the level of $\alpha = 5\%$, Equation (4) was given with R^2 of 0.9516, indicating a good model fit.

$$\begin{aligned} \text{RR} = & -25.057 + 0.576S_t + 1.404H_v + 0.679H_t + 0.679M_d - 0.006H_tM_d - 0.039S_t^2 \\ & - 0.445H_v^2 - 0.006H_t^2 - 0.045M_d^2 \end{aligned} \quad (4)$$

To intuitively understand the combined effects of each two variables on RR, the response surface and contour plots were plotted for each of the fitted models as the function of two independent variables while other variables were kept at central values (Figure 4).

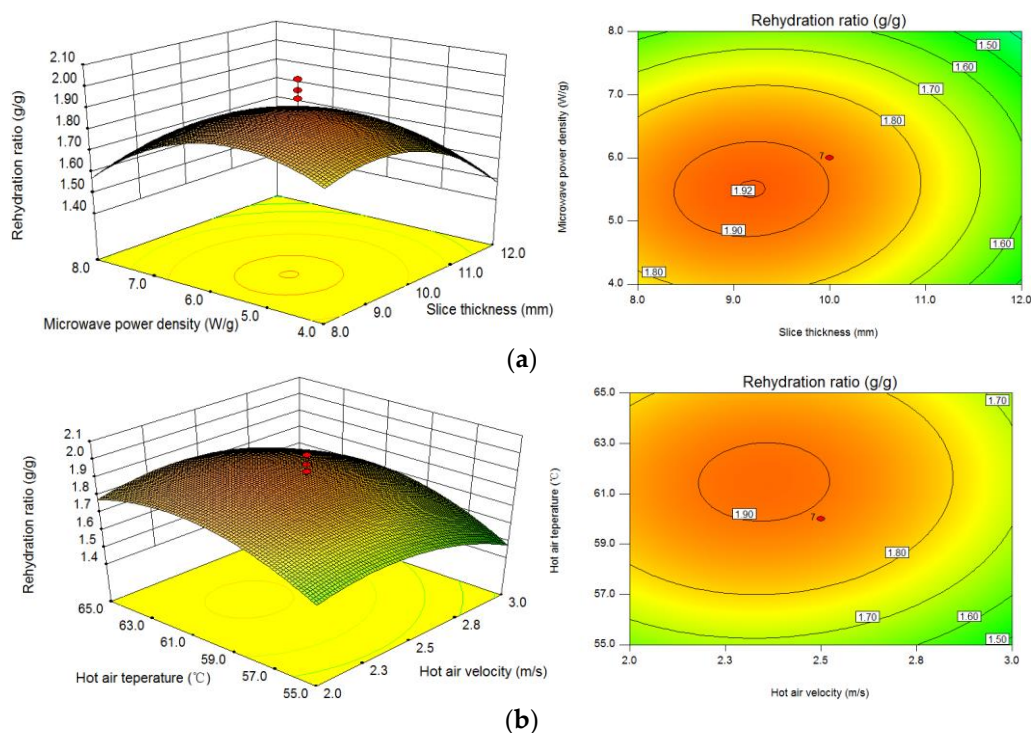


Figure 4. Response surface plots of RR between variables. (a) Slice thickness and microwave power density; (b) Hot air velocity and hot air temperature.

Figure 4a shows the interaction effect of slice thickness and microwave power density on RR with constant hot air velocity and hot air temperature at 2.5 m/s and 60 °C, respectively. When slice thickness was less than 10 mm and microwave power density was lower than 6 W/g, the correlation between RR and the variables was positive. RR could reach up to a level higher than 1.9 g/g at slice thickness and microwave power density ranging from 6 to 10 mm and 2 to 6 W/g, respectively. This behavior is because when the slice thickness was at a thinner level, the rate of water transfer from the interior of drying Chinese yam slices to the surface was much faster than that of water evaporation on the surface, which resulted in a sharp rise in the temperature of the interior of drying materials and then caused

volume shrinkage and case hardening, subsequently decreasing the rehydration capacity of dried yam slices. RR increased as slice thickness gradually increased to a certain level, which is probably because water transfer and evaporation rates tended to be balanced with the increase of slice thickness. However, the balance was disrupted when slice thickness was thicker than 10 mm, leading to lower rehydration properties. A similar result was reported in the study of microwave-vacuum drying for button mushroom [38]. The high RR at high microwave power density may be due to the formation of high pressure in the interior of drying yams caused by high microwave power density. The interior water rapidly evaporated with the quick absorption of microwave energy and thus generated many pores in the interior of drying yams, which benefited in preventing the volume shrinkage and case hardening of dried yams, thereby, enhancing RR. This finding is consistent with a previous study [40]. Nevertheless, RR decreased when microwave power density exceeded 6 W/g, which is due to the damage of cellular structures caused by excessive power density [41].

Figure 4b represents that the relationship between RR and hot air velocity and hot air temperature was a quadratic function. RR increased first and then decreased at hot air velocity and temperature of 2.5 m/s and 60 °C [24], respectively, which demonstrates that the increase of hot air temperature and velocity at low levels could promote the evaporation rate of water on the surface and enhance the pressure gradient between the interior and the surface of drying materials. The enhanced pressure gradient contributed to the rapid escape of water from the interior to the surface and formed some capillary channels, which benefited by improving RR. However, when hot air velocity and temperature exceeded rational ranges ($H_v \geq 2.5$ m/s and $H_t \geq 60$ °C), the excessive dehydration led to structure destruction, severe volume shrinkage, and case hardening, thus worsening rehydration characteristics.

3.2.2. Analysis of TSC

As shown in Table 3, TSC of dried yam slices ranged from 3.65 to 5.89 g/100 g under various conditions. For the linear items, all process variables were significant in the model ($p \leq 0.01$, Table 4). The p -values of each variable illustrated that slice thickness had the most effect on TSC, followed by microwave power density, hot air velocity, and hot air temperature. Thus, slice thickness was a major factor that influenced the TSC of dried yam slices. According to the p -values, all of the interaction effects were not statistically significant ($p \geq 0.05$), while their quadratic levels were significant ($p \leq 0.01$). By removing the statistically insignificant items of x_1x_2 , x_1x_3 , x_1x_4 , x_2x_3 , x_2x_4 , x_3x_4 at the level of $\alpha = 5\%$, Equation (5) was given with R^2 of 0.9588, indicating a good model fit.

$$\begin{aligned} \text{TSC} = & -28.857 + 0.563S_t + 5.633H_v + 0.634H_t + 1.733M_d - 0.034S_t^2 - 0.734H_v^2 - 0.004H_t^2 \\ & - 0.092M_d^2 \end{aligned} \quad (5)$$

To intuitively understand the combined effects of each two variables on TSC, the response surface and contour plots were also plotted for each of the fitted models as the function of two independent variables while keeping other variables at central values (Figure 5). Figure 5a indicates the interaction effect of slice thickness and microwave power density on TSC with constant hot air velocity and temperature at 2.5 m/s and 60 °C, respectively. TSC was negatively correlated with slice thickness, which is because the increase of slice thickness increased the transfer distance of water from the interior to the surface and thus required longer drying time, which increased total sugar loss. However, TSC was positively correlated with microwave power density at the level below 7.0 W/g, which is because the increased absorption of microwave energy enhanced the evaporation and transfer rates of water, thus effectively shortening drying time and reducing the undesired chemical reactions of sugars themselves as well as sugars with other ingredients. In addition, although the microwave power density of greater than 7.0 W/g further shortened drying time, the temperature of drying materials rose sharply, which intensified the Maillard and caramelization reactions of polysaccharides.

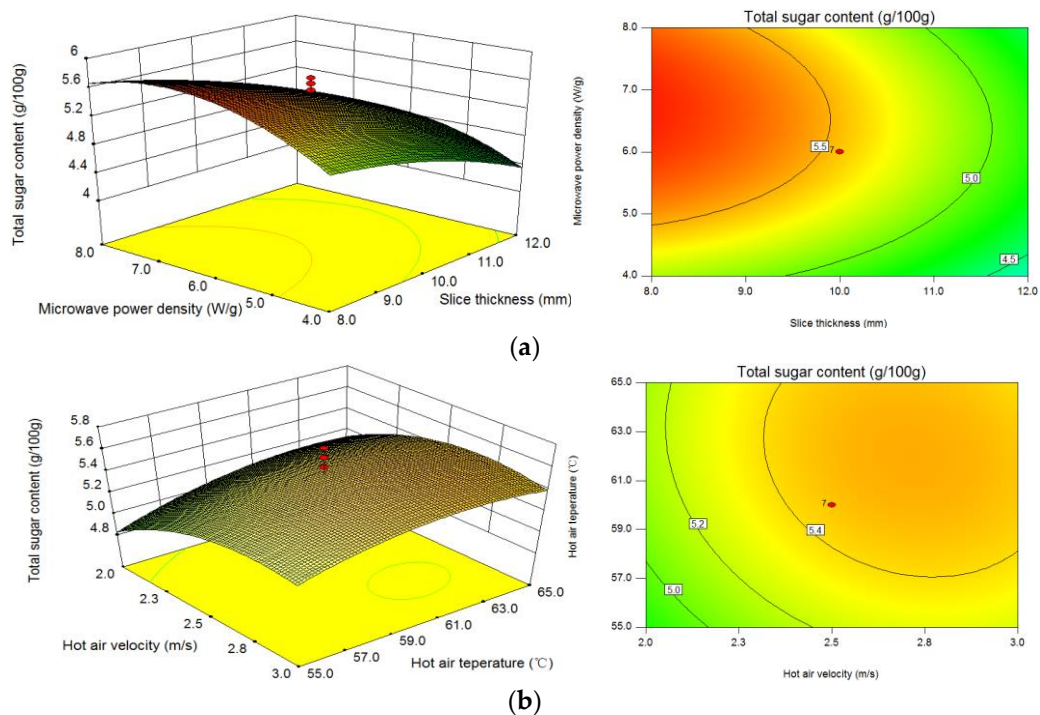


Figure 5. Response surface plots of TSC between variables. (a) Slice thickness and microwave power density; (b) Hot air velocity and hot air temperature.

Figure 5b shows the interactive effect of hot air velocity and hot air temperature on TSC with constant slice thickness and microwave power density at 10 mm and 6 W/g, respectively. TSC increased first and then decreased at the hot air velocity and temperature of 2.8 m/s and 63.0 °C, respectively. The main reason for this variation was that at the tested levels, the rational increase of hot air velocity and hot air temperature not only shortened drying time but also controlled the temperature of drying materials at a low level, thus improving TSC. However, when hot air velocity and temperature exceeded rational values ($H_v \geq 2.8$ m/s and $H_t \geq 60$ °C), hot air accelerated evaporation rate of water on the surface of drying Chinese yam slices at the initial drying period, causing case hardening. The case hardening was intensified over drying time, which in turn reduced water transfer rate. The reduced water transfer rate centralized a large amount of heat in the interior of drying yams and thus caused a sharp rise in the temperature of the interior of drying yams, decreasing TSC due to the occurrence of Maillard and caramelization reactions.

4. Optimization and Model Verification

The optimal condition process for the drying of yam slices using MWA was determined to obtain maximum RR and TSC. Second-order polynomial models obtained in the study were used for each response to investigate the specified optimum drying condition. These regression models were only valid in the selected experimental domain. All factors including process variables and responses variables were equally weighed. By applying the desirability function method, the optimal conditions were obtained with the slice thickness of 8.5 mm, hot air velocity of 2.5 m/s, hot air temperature of 61.7 °C, and microwave power density of 5.9 W/g. Under the optimal conditions, the predicted values for RR and TSC were 1.90 g/g and 5.74 g/100 g, respectively, which are very close to the test values (Table 5). The desirability of 0.913 under the optimal conditions further confirmed the validation of models.

Table 5. Predicted and test values of response variables under optimal conditions.

Optimal Drying Conditions	Response Variable	Test Value	Predicted Value
Slice thickness/8.5 mm Hot air velocity/2.5 m/s Hot air temperature/61.7 °C Microwave power density/5.9 W/g	RR/(g/g)	1.83	1.90
	TSC/(g/100 g)	5.72	5.74

5. Conclusions

In this work, the optimal conditions of MWA drying for Chinese yam slices was obtained using RSM. Results showed that the second-order polynomial model with the R^2 value higher than 0.95 adequately described and predicted the responses RR and TSC under the tested conditions. According to the p -values, the effects of variables on RR followed the order: slice thickness > hot air temperature > microwave power density > hot air velocity; and the effects of variables on TSC followed the order: slice thickness > microwave power density > hot air velocity > hot air temperature. The optimal conditions were obtained with the slice thickness of 8.5 mm, hot air velocity of 2.5 m/s, hot air temperature of 61.7 °C, and microwave power density of 5.9 W/g. The experimental data and predicted values of response variables were extremely close with a desirability of 0.913. Therefore, the developed second-order polynomial model is powerful.

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