

Article

New Scientific Contribution on the 2-D Subdomain Technique in Polar Coordinates: Taking into Account of Iron Parts

Frédéric Dubas ^{1,*} and Kamel Boughrara ²

¹ Département ENERGIE, FEMTO-ST, CNRS, University Bourgogne Franche-Comté, F90000 Belfort, France

² Laboratoire de Recherche en Electrotechnique (LRE-ENP), 16200 Algiers, Algeria;
kamel.boughrara@g.enp.edu.dz

* Correspondence: frederic.dubas@univ-fcomte.fr; Tel.: +33-3-8457-8203

Received: 22 July 2017; Accepted: 23 October 2017; Published: 25 October 2017

Abstract: This paper presents a new scientific contribution to the two-dimensional red(2-D) subdomain technique in polar coordinates taking into account the finite relative permeability of the ferromagnetic material. The constant relative permeability corresponds to the linear part of the nonlinear $B(H)$ curve. As in the conventional technique, the separation of variables method and the Fourier series are used for the resolution of magnetostatic Maxwell equations in each region. The general solutions of the magnetic field in subdomains, as well as the boundary conditions (BCs) between regions are different from the conventional method. In the proposed method, the magnetic field solution in each subdomain is a superposition of two magnetic quantities in the two directions (i.e., r - and Θ -axis), and the BCs between two regions are also in both directions. For example, the scientific contribution has been applied to an air- or iron-cored coil supplied by a constant current. The distribution of local quantities (i.e., the magnetic vector potential and flux density) has been validated by a corresponding 2-D finite-element analysis (FEA). The obtained semi-analytical results are in very good agreement with those of the numerical method.

Keywords: air- or iron-cored coil; polar coordinates; Fourier analysis; two-dimensional; subdomain technique

1. Introduction

The full calculation of the magnetic field in electrical engineering applications is the first step for their design and optimization. The methods of magnetic field prediction can be classified into various categories [1]:

- Lehmann's graphical [2];
- Numerical (i.e., finite-element, finite-difference, boundary-element, etc.) [3–5];
- Equivalent circuit (i.e., electrical, thermal, magnetic, etc.) [6–8];
- Schwarz–Christoffel mapping (i.e., conformal transformation, complex permeance model, etc.) [9];
- Maxwell–Fourier [10–15].

Currently, the works on design are based on (semi-)analytical models (i.e., equivalent circuit, conformal transformation and Maxwell–Fourier methods). This type of model consists of a (non)linear system of N analytical equations solved analytically or numerically. In comparison with the other methods, under certain geometrical and physical assumptions, these models permit obtaining accurate analytical expressions of the magnetic field and are known as fast for the local/global electromagnetic performances prediction. At present, Maxwell–Fourier methods are one of the most used semi-analytical

approaches with very accurate results (i.e., error less than 5%) on the electromagnetic performances calculation. These models are based on the formal resolution of Maxwell's equations in Cartesian, cylindrical or spherical coordinates by using the separation of variables method and the Fourier's series. Taking into account iron parts and/or the effect of local/global saturation is still a scientific challenge in Maxwell–Fourier methods, which is rarely explored in the literature [16–18]. Recently, Dubas et al. (2017) [1] realized an overview of the existing (semi-)analytical models in Maxwell–Fourier methods with the effect of local/global saturation, which can thus be classified as follows:

- Multi-layer models (i.e., Carter's coefficient [19,20], saturation coefficient [21,22], concept wave impedance [23–26] and convolution theorem [27–30]);
- Eigenvalues model, viz., the method of truncation region eigenfunction expansions (TREE) [31,32];
- Subdomain technique [1,33,34];
- Hybrid models, viz., the analytical solution combined with numerical methods [35,36] or (non)linear magnetic equivalent circuit [37–39].

The consideration of the effect of local/global saturation appears in hybrid models, where the solution is established analytically in concentric regions of very low permeability (e.g., air-gap and magnets), and other methods (e.g., numerical or magnetic equivalent circuit) are sought in regions where the saturation effect cannot be neglected. The other models (i.e., multi-layers models, TREE method and subdomain technique) are more focused on the global saturation. Some details and (dis)advantages of these techniques can be found in [1]. In most semi-analytical models based on the subdomain technique, the iron parts are considered to be infinite permeable due to the variation of material proprieties in the various directions, so that the saturation effect is neglected [16–18]. The first paper introducing the iron parts in the magnetic field calculation by using the subdomain technique is [1], where the authors solve partial differential equations (PDEs) of the magnetic potential vector in Cartesian coordinates in which the subdomains connection is performed directly in both directions (i.e., x - and y -edges). The 2-D magnetostatic model has been applied to an air- or iron-cored coil supplied by a constant current. In [33], the authors propose a 2-D semi-analytical model in spoke-type magnet synchronous machines based on the subdomain technique in polar coordinates with the Taylor polynomial of degree three by focusing on the consideration of iron. The iron magnetic permeability is supposed constant corresponding to the linear zone of the nonlinear $B(H)$ curve. The subdomains' connection is carried out in both directions (i.e., r - and Θ -edges). The general solution of the magnetic field is obtained by using the traditional boundary condition (BCs), in addition to new radial BCs (e.g., between the magnets and the rotor teeth, between the teeth and the slots of the stator), which are traduced into a system of linear equations according to Taylor series expansion. In [34], this semi-analytical model has been extended taking into account the initial magnetization curve in each soft-magnetic subdomain by an iterative procedure.

In the literature, to the authors' knowledge, there exists no exact 2-D subdomain technique in polar coordinates taking into account iron parts with(out) the nonlinear $B(H)$ curve and not using the Taylor series expansion to satisfy the r -edges BCs. Thus, in this paper, the research work contributes to the continuous improvement of the 2-D subdomain technique. Moreover, it is an extension of [1] in polar coordinates (r, Θ). Section 2 presents this new scientific contribution. By applying the principle of superposition on the magnetic quantities in order to respect the BCs on the various edges, the general solution of the magnetic field is decomposed in Fourier's series into two general solutions in both directions (i.e., r - and Θ -edges). It allows the evaluation of the local distribution of flux densities in the iron parts with a global saturation, does not have numerical convergence problems contrary to others models and would easily introduce the current penetration effect in the conductive materials. The semi-analytical solution is exact as in [1] and does not use the Taylor polynomial to satisfy the r -edges BCs contrary to [33,34]. For example, it was applied to an air- or iron-cored coil supplied by a constant current. The iron magnetic permeability is constant corresponding to the linear zone of the nonlinear $B(H)$ curve [1,33]. Nevertheless, as in [29,30,34], the saturation effect could be taken into account by an iterative calculation considering, at each iteration, a constant relative magnetic

permeability according to the nonlinear $B(H)$ curve. However, this is beyond the scope of the paper. In Section 3, in order to confirm the effectiveness of the proposed technique, all semi-analytical results are then compared to those found by 2-D finite-element analysis (FEA) [40]. The comparisons are very satisfying in amplitudes and waveforms.

2. A 2-D Subdomain Technique of the Magnetic Field in Polar Coordinates

2.1. Model Description and Assumptions

Figure 1 represents the physical and geometrical parameters of an air- or iron-cored coil with N_t turns of copper wire supplied by a constant current I . The electromagnetic device is surrounded by an infinite box with a null value of magnetic vector potential at its boundaries.

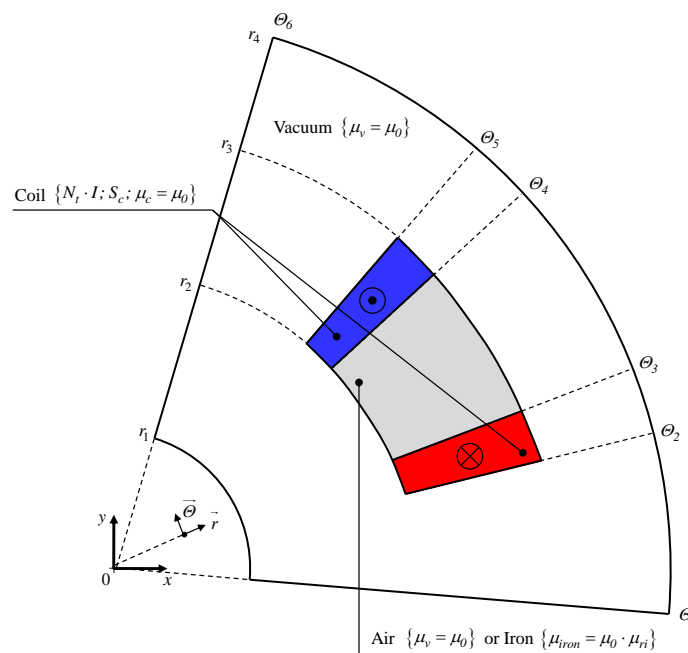


Figure 1. Physical and geometrical parameters (see Table 1) of air- or iron-cored coil where \otimes and \odot are respectively the forward and return conductor. The variables are: N_t the number of turns; I the supply current; S_c the conductor surface; μ_v the vacuum magnetic permeability; μ_c the copper magnetic permeability; and μ_{iron} the iron magnetic permeability.

The analytical prediction of the magnetic field based on the 2-D subdomain technique is done by solving magnetostatic Maxwell equations in polar coordinates (r, Θ) with the following assumptions:

- The magnetic vector potential has only one component along the z -axis (i.e., $\mathbf{A} = \{0; 0; A_z\}$), and then, the end-effects are not considered;
- All materials are isotropic, and the permeabilities are supposed as constants in both directions (i.e., r - and Θ -axis);
- All electrical conductivities of materials are supposed as nulls (i.e., the eddy-currents induced in the copper/iron are neglected).

2.2. Problem Discretization in Regions

In Figure 2, we present the studied electromagnetic device, which is divided into seven regions with $\mu = C^{st}$, viz.,

- Region 1 $\{\forall \Theta \wedge r \in [r_1, r_2]\}$, with $\mu_1 = \mu_v$;

- Region 2 $\{\forall \Theta \wedge r \in [r_3, r_4]\}$, with $\mu_2 = \mu_v$;
- Region 3 $\{\Theta \in [\Theta_1, \Theta_2] \wedge r \in [r_2, r_3]\}$, with $\mu_3 = \mu_v$;
- Region 4 $\{\Theta \in [\Theta_5, \Theta_6] \wedge r \in [r_2, r_3]\}$, with $\mu_4 = \mu_v$;
- Region 5 (i.e., the air or iron in the middle of the coil) $\{\Theta \in [\Theta_2, \Theta_3] \wedge r \in [r_2, r_3]\}$, with $\mu_5 = \mu_v$ for the air or $\mu_5 = \mu_{iron}$ for the iron;
- Region 6 (i.e., the forward conductor) $\{\Theta \in [\Theta_2, \Theta_3] \wedge r \in [r_2, r_3]\}$, with $\mu_6 = \mu_c$;
- Region 7 (i.e., the return conductor) $\{\Theta \in [\Theta_4, \Theta_5] \wedge r \in [r_2, r_3]\}$, with $\mu_7 = \mu_c$.

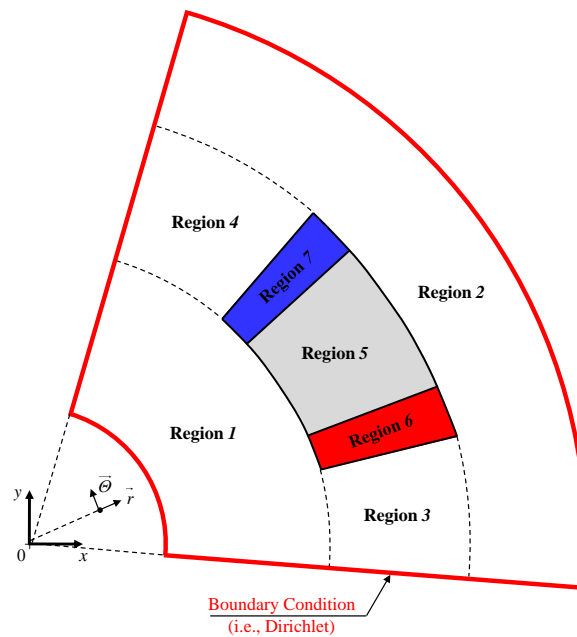


Figure 2. Definition of regions in the air- or iron-cored coil.

2.3. Governing PDEs in Polar Coordinates: Laplace’s and Poisson’s Equations

According to Equation (A1) (see Appendix A), the distribution of the magnetic vector potential in polar coordinates (r, Θ) is governed by:

$$\Delta A_{zj} = \frac{\partial^2 A_{zj}}{\partial r^2} + \frac{1}{r} \cdot \frac{\partial A_{zj}}{\partial r} + \frac{1}{r^2} \cdot \frac{\partial^2 A_{zj}}{\partial \Theta^2} = 0 \quad \text{for } j = \{1, \dots, 5\} \quad (\text{Laplace's equation}), \quad (1a)$$

$$\Delta A_{zk} = \frac{\partial^2 A_{zk}}{\partial r^2} + \frac{1}{r} \cdot \frac{\partial A_{zk}}{\partial r} + \frac{1}{r^2} \cdot \frac{\partial^2 A_{zk}}{\partial \Theta^2} = -\mu_k \cdot J_{zk} \quad \text{for } k = \{6, 7\} \quad (\text{Poisson's equation}), \quad (1b)$$

where J_{zk} is the current density of the coil defined by:

$$J_{zk} = C_k \cdot \frac{N_t \cdot I}{S_c}, \quad (2)$$

in which S_c is the conductor surface and C_k (with $C_6 = 1$ and $C_7 = -1$) is the coefficient that represents the current direction in the conductor.

According to Appendix A, the resolution of Laplace’s and Poisson’s equations by using the separation of variables method and Fourier’s series permit obtaining two potentials in both directions, viz., $A_{z\bullet}^\Theta$ for the Θ -edges (in Equation (A2b)) and $A_{z\bullet}^r$ for the r -edges (in Equation (A2c)). The spatial frequency (or periodicity) of $A_{z\bullet}^\Theta$ and $A_{z\bullet}^r$ is respectively defined by $\beta_{h\bullet}$ and $\lambda_{n\bullet}$ with $h\bullet$ and $n\bullet$ the spatial harmonic orders.

2.4. Definition of Boundary Conditions

In electromagnetics, the general solutions of various regions depend on the BCs at the interface of two surfaces, which are defined by the continuity of the normal flux density \mathbf{B}_\perp and parallel field intensity \mathbf{H}_\parallel [1]. On the outer BCs for $(\Theta_1 \wedge \Theta_6, \forall r)$ and $(\forall \Theta, r_1 \wedge r_4)$, A_z satisfies the Dirichlet BC (see Figure 2), viz., $A_z = 0$.

Figure 3 represents the respective BCs at the interface between the various regions in both directions (i.e., r - and Θ -edges).

2.5. General Solutions of Various Regions

2.5.1. Region 1

The solutions of A_{z1} , B_{r1} and $B_{\Theta1}$ are determined by Case-Study No. 1 (i.e., A_z imposed on all edges of a region) in Appendix B. The BCs on the r -edges of the region (see Figure 3a) are met by posing $c_h^\Theta = 0$ in Equation (A11). Therefore, A_{z1} satisfying the BCs of Figure 3a and the solution of Equation (1a) is given by:

$$A_{z1} = - \sum_{h1=1}^{\infty} d1_{h1}^\Theta \cdot \frac{r_2}{\beta1_{h1}} \cdot \frac{E_\phi(\beta1_{h1}, r, r_1)}{P_\phi(\beta1_{h1}, r_2, r_1)} \cdot \sin[\beta1_{h1} \cdot (\Theta - \Theta_1)], \tag{3}$$

the components of $\mathbf{B}_1 = \{B_{r1}; B_{\Theta1}; 0\}$ by:

$$B_{r1} = - \sum_{h1=1}^{\infty} d1_{h1}^\Theta \cdot \frac{r_2}{r} \cdot \frac{E_\phi(\beta1_{h1}, r, r_1)}{P_\phi(\beta1_{h1}, r_2, r_1)} \cdot \cos[\beta1_{h1} \cdot (\Theta - \Theta_1)], \tag{4}$$

$$B_{\Theta1} = \sum_{h1=1}^{\infty} d1_{h1}^\Theta \cdot \frac{r_2}{r} \cdot \frac{P_\phi(\beta1_{h1}, r, r_1)}{P_\phi(\beta1_{h1}, r_2, r_1)} \cdot \sin[\beta1_{h1} \cdot (\Theta - \Theta_1)], \tag{5}$$

where $E_\phi(w, x, y)$ and $P_\phi(w, x, y)$ are defined in Equation (A9), $h1$ the spatial harmonic orders in Region 1, $d1_{h1}^\Theta$ the integration constant and $\beta1_{h1} = h1 \cdot \pi / \tau_{\Theta1}$ with $\tau_{\Theta1} = \Theta_6 - \Theta_1$.

Using a Fourier series expansion of $F_1(\Theta)$ (see Figure 3a) over the interval $\Theta = [\Theta_1, \Theta_6] = [\Theta_1, \Theta_1 + \tau_{\Theta1}]$, the integration constant $d1_{h1}^\Theta$ is determined in Appendix C with:

$$d1_{h1}^\Theta = \frac{2}{\tau_{\Theta1}} \cdot \int_{\Theta_1}^{\Theta_1 + \tau_{\Theta1}} F_1(\Theta) \cdot \sin[\beta1_{h1} \cdot (\Theta - \Theta_1)] \cdot d\Theta. \tag{6}$$

2.5.2. Region 2

The same method as Region 1 is used to define the general solution in Region 2. By posing $d_h^\Theta = 0$ in Equation (A11) (see Appendix B), A_{z2} satisfying the BCs of Figure 3b and the solution of Equation (1a) is given by:

$$A_{z2} = \sum_{h2=1}^{\infty} c2_{h2}^\Theta \cdot \frac{r_3}{\beta2_{h2}} \cdot \frac{E_\phi(\beta2_{h2}, r_4, r)}{P_\phi(\beta2_{h2}, r_4, r_3)} \cdot \sin[\beta2_{h2} \cdot (\Theta - \Theta_1)], \tag{7}$$

the components of $\mathbf{B}_2 = \{B_{r2}; B_{\Theta2}; 0\}$ by:

$$B_{r2} = \sum_{h2=1}^{\infty} c2_{h2}^\Theta \cdot \frac{r_3}{r} \cdot \frac{E_\phi(\beta2_{h2}, r_4, r)}{P_\phi(\beta2_{h2}, r_4, r_3)} \cdot \cos[\beta2_{h2} \cdot (\Theta - \Theta_1)], \tag{8}$$

$$B_{\Theta2} = \sum_{h2=1}^{\infty} c2_{h2}^\Theta \cdot \frac{r_3}{r} \cdot \frac{P_\phi(\beta2_{h2}, r_4, r)}{P_\phi(\beta2_{h2}, r_4, r_3)} \cdot \sin[\beta2_{h2} \cdot (\Theta - \Theta_1)], \tag{9}$$

where h_2 is the spatial harmonic orders in Region 2, $c_{h_2}^\Theta$ the integration constant and $\beta_{2h_2} = h_2 \cdot \pi / \tau_{\Theta_2}$ with $\tau_{\Theta_2} = \Theta_6 - \Theta_1$.

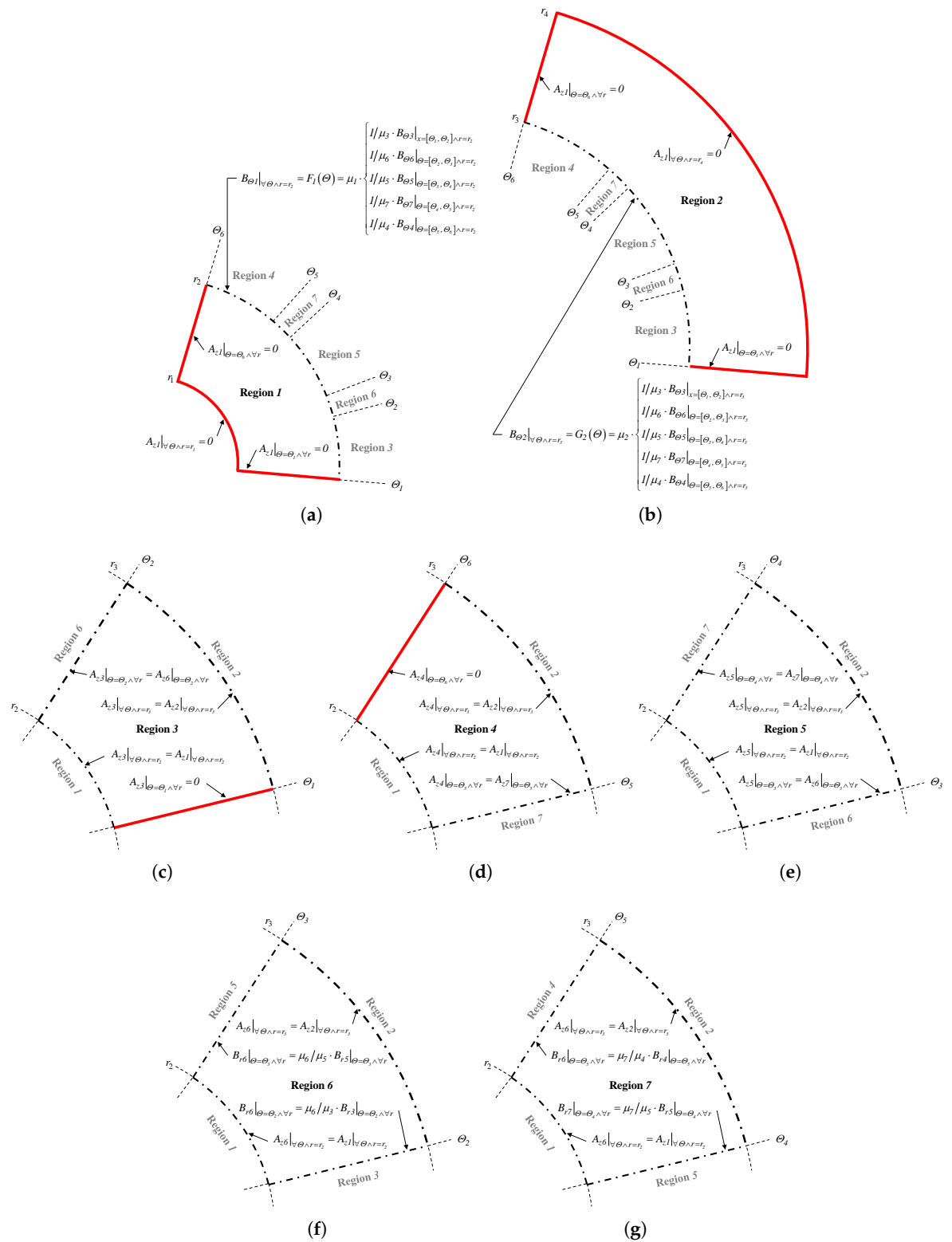


Figure 3. Boundary Conditions (BCs) in both directions (i.e., r - and Θ -edges): (a) Region 1; (b) Region 2; (c) Region 3; (d) Region 4; (e) Region 5; (f) Region 6; and (g) Region 7.

Using a Fourier series expansion of $G_2(\Theta)$ (see Figure 3b) over the interval $\Theta = [\Theta_1, \Theta_6] = [\Theta_1, \Theta_1 + \tau_{\Theta 2}]$, the integration constant $c2_{h2}^{\Theta}$ is determined in Appendix C with:

$$c2_{h2}^{\Theta} = \frac{2}{\tau_{\Theta 2}} \cdot \int_{\Theta_1}^{\Theta_1 + \tau_{\Theta 2}} G_2(\Theta) \cdot \sin[\beta 2_{h2} \cdot (\Theta - \Theta_1)] \cdot d\Theta. \tag{10}$$

2.5.3. Region 3

The solutions of A_{z3} , B_{r3} and $B_{\Theta 3}$ are determined by the Case-Study No. 1 (i.e., A_z imposed on all edges of a region) in Appendix B. The BCs on the Θ -edges of the region (see Figure 3c) are met by posing $e_n^r = 0$ in Equations (A6)–(A8). Therefore, A_{z3} satisfying the BCs of Figure 3c and the solution of Equation (1a) is given by:

$$A_{z3} = A_{z3}^{\Theta} + A_{z3}^r, \tag{11a}$$

$$A_{z3}^{\Theta} = \sum_{h3=1}^{\infty} \left[c3_{h3}^{\Theta} \cdot r_2 \cdot \frac{E_{\phi}(\beta 3_{h3}, r_3, r)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} + d3_{h3}^{\Theta} \cdot r_3 \cdot \frac{E_{\phi}(\beta 3_{h3}, r, r_2)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} \right] \cdot \sin[\beta 3_{h3} \cdot (\Theta - \Theta_1)], \tag{11b}$$

$$A_{z3}^r = \sum_{n3=1}^{\infty} f3_{n3}^r \cdot r_2 \cdot \frac{sh[\lambda 3_{n3} \cdot (\Theta - \Theta_1)]}{sh(\lambda 3_{n3} \cdot \tau_{\Theta 3})} \cdot \sin\left[\lambda 3_{n3} \cdot \ln\left(\frac{r}{r_2}\right)\right], \tag{11c}$$

the r -component of \mathbf{B}_3 by:

$$B_{r3} = B_{r3}^{\Theta} + B_{r3}^r, \tag{12a}$$

$$B_{r3}^{\Theta} = \sum_{h3=1}^{\infty} \beta 3_{h3} \cdot \left[c3_{h3}^{\Theta} \cdot \frac{r_2}{r} \cdot \frac{E_{\phi}(\beta 3_{h3}, r_3, r)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} + d3_{h3}^{\Theta} \cdot \frac{r_3}{r} \cdot \frac{E_{\phi}(\beta 3_{h3}, r, r_2)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} \right] \cdot \cos[\beta 3_{h3} \cdot (\Theta - \Theta_1)], \tag{12b}$$

$$B_{r3}^r = \sum_{n3=1}^{\infty} \lambda 3_{n3} \cdot f3_{n3}^r \cdot \frac{r_2}{r} \cdot \frac{ch[\lambda 3_{n3} \cdot (\Theta - \Theta_1)]}{sh(\lambda 3_{n3} \cdot \tau_{\Theta 3})} \cdot \sin\left[\lambda 3_{n3} \cdot \ln\left(\frac{r}{r_2}\right)\right], \tag{12c}$$

the Θ -component of \mathbf{B}_3 by:

$$B_{\Theta 3} = B_{\Theta 3}^{\Theta} + B_{\Theta 3}^r, \tag{13a}$$

$$B_{\Theta 3}^{\Theta} = \sum_{h3=1}^{\infty} \beta 3_{h3} \cdot \left[c3_{h3}^{\Theta} \cdot \frac{r_2}{r} \cdot \frac{P_{\phi}(\beta 3_{h3}, r_3, r)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} - d3_{h3}^{\Theta} \cdot \frac{r_3}{r} \cdot \frac{P_{\phi}(\beta 3_{h3}, r, r_2)}{E_{\phi}(\beta 3_{h3}, r_3, r_2)} \right] \cdot \sin[\beta 3_{h3} \cdot (\Theta - \Theta_1)], \tag{13b}$$

$$B_{\Theta 3}^r = - \sum_{n3=1}^{\infty} \lambda 3_{n3} \cdot f3_{n3}^r \cdot \frac{r_2}{r} \cdot \frac{sh[\lambda 3_{n3} \cdot (\Theta - \Theta_1)]}{sh(\lambda 3_{n3} \cdot \tau_{\Theta 3})} \cdot \cos\left[\lambda 3_{n3} \cdot \ln\left(\frac{r}{r_2}\right)\right], \tag{13c}$$

where $h3$ and $n3$ are the spatial harmonic orders in Region 3; $c3_{h3}^{\Theta}$, $d3_{h3}^{\Theta}$ and $f3_{n3}^r$ the integration constants; $\beta 3_{h3} = h3 \cdot \pi / \tau_{\Theta 3}$ with $\tau_{\Theta 3} = \Theta_2 - \Theta_1$; and $\lambda 3_{n3} = n3 \cdot \pi / \tau_{r3}$ with $\tau_{r3} = \ln(r_3 / r_2)$.

Using Fourier series expansion of $A_{z1}|_{\forall \Theta \wedge r=r_2}$ and $A_{z2}|_{\forall \Theta \wedge r=r_3}$ (see Figure 3c) over the interval $\Theta = [\Theta_1, \Theta_2] = [\Theta_1, \Theta_1 + \tau_{\Theta 3}]$, the integration constants $c3_{h3}^{\Theta}$ and $d3_{h3}^{\Theta}$ are determined in Appendix C with:

$$c3_{h3}^{\Theta} = \frac{2}{\tau_{\Theta 3}} \cdot \int_{\Theta_1}^{\Theta_1 + \tau_{\Theta 3}} \frac{A_{z1}|_{r=r_2}}{r_2} \cdot \sin[\beta 3_{h3} \cdot (\Theta - \Theta_1)] \cdot d\Theta, \tag{14a}$$

$$d3_{h3}^{\Theta} = \frac{2}{\tau_{\Theta 3}} \cdot \int_{\Theta_1}^{\Theta_1 + \tau_{\Theta 3}} \frac{A_{z2}|_{r=r_3}}{r_3} \cdot \sin[\beta 3_{h3} \cdot (\Theta - \Theta_1)] \cdot d\Theta. \tag{14b}$$

With a weighting function $g(r) = r^{-1}$ and using a Fourier series expansion of $A_{z6}|_{\Theta=\Theta_2 \wedge \forall r}$ (see Figure 3c) over the interval $r = [r_2, r_3]$, the integration constant $f3_{n3}^r$ is determined in Appendix C with:

$$f3_{n3}^r = \frac{2}{\tau_{r3}} \cdot \int_{r_2}^{r_3} \frac{1}{r} \cdot \frac{A_{z6}|_{\Theta=\Theta_2}}{r_2} \cdot \sin \left[\lambda_{3n3} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr. \tag{15}$$

2.5.4. Region 4

The solution in Region 4 is obtained using the same development as Region 3. By posing $f_n^r = 0$ in Equations (A6)–(A8) (see Appendix B), A_{z4} satisfying the BCs of Figure 3d and the solution of Equation (1a) is given by:

$$A_{z4} = A_{z4}^\ominus + A_{z4}^r, \tag{16a}$$

$$A_{z4}^\ominus = \sum_{h4=1}^\infty \left[c4_{h4}^\ominus \cdot r_2 \cdot \frac{E_f(\beta_{4h4}, r_3, r)}{E_f(\beta_{4h4}, r_3, r_2)} + d4_{h4}^\ominus \cdot r_3 \cdot \frac{E_f(\beta_{4h4}, r, r_2)}{E_f(\beta_{4h4}, r_3, r_2)} \right] \cdot \sin [\beta_{4h4} \cdot (\Theta - \Theta_5)], \tag{16b}$$

$$A_{z4}^r = \sum_{n4=1}^\infty e4_{n4}^r \cdot r_2 \cdot \frac{sh [\lambda_{4n4} \cdot (\Theta_6 - \Theta)]}{sh (\lambda_{4n4} \cdot \tau_{\Theta4})} \cdot \sin \left[\lambda_{4n4} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{16c}$$

the r -component of \mathbf{B}_4 by:

$$B_{r4} = B_{r4}^\ominus + B_{r4}^r, \tag{17a}$$

$$B_{r4}^\ominus = \sum_{h4=1}^\infty \beta_{4h4} \cdot \left[c4_{h4}^\ominus \cdot \frac{r_2}{r} \cdot \frac{E_f(\beta_{4h4}, r_3, r)}{E_f(\beta_{4h4}, r_3, r_2)} + d4_{h4}^\ominus \cdot \frac{r_3}{r} \cdot \frac{E_f(\beta_{4h4}, r, r_2)}{E_f(\beta_{4h4}, r_3, r_2)} \right] \cdot \cos [\beta_{4h4} \cdot (\Theta - \Theta_5)], \tag{17b}$$

$$B_{r4}^r = - \sum_{n4=1}^\infty \lambda_{4n4} \cdot e4_{n4}^r \cdot \frac{r_2}{r} \cdot \frac{ch [\lambda_{4n4} \cdot (\Theta_6 - \Theta)]}{sh (\lambda_{4n4} \cdot \tau_{\Theta4})} \cdot \sin \left[\lambda_{4n4} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{17c}$$

the Θ -component of \mathbf{B}_4 by:

$$B_{\Theta4} = B_{\Theta4}^\ominus + B_{\Theta4}^r, \tag{18a}$$

$$B_{\Theta4}^\ominus = \sum_{h4=1}^\infty \beta_{4h4} \cdot \left[c4_{h4}^\ominus \cdot \frac{r_2}{r} \cdot \frac{P_f(\beta_{4h4}, r_3, r)}{E_f(\beta_{4h4}, r_3, r_2)} - d4_{h4}^\ominus \cdot \frac{r_3}{r} \cdot \frac{P_f(\beta_{4h4}, r, r_2)}{E_f(\beta_{4h4}, r_3, r_2)} \right] \cdot \sin [\beta_{4h4} \cdot (\Theta - \Theta_5)], \tag{18b}$$

$$B_{\Theta4}^r = - \sum_{n4=1}^\infty \lambda_{4n4} \cdot e4_{n4}^r \cdot \frac{r_2}{r} \cdot \frac{sh [\lambda_{4n4} \cdot (\Theta_6 - \Theta)]}{sh (\lambda_{4n4} \cdot \tau_{\Theta4})} \cdot \cos \left[\lambda_{4n4} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{18c}$$

where $h4$ and $n4$ are the spatial harmonic orders in Region 4; $c4_{h4}^\ominus$, $d4_{h4}^\ominus$ and $e4_{n4}^r$ the integration constants; $\beta_{4h4} = h4 \cdot \pi / \tau_{\Theta4}$ with $\tau_{\Theta4} = \Theta_6 - \Theta_5$; and $\lambda_{4n4} = n4 \cdot \pi / \tau_{r4}$ with $\tau_{r4} = \ln (r_3 / r_2)$.

Using Fourier series expansion of $A_{z1}|_{\forall \Theta \wedge r=r_2}$ and $A_{z2}|_{\forall \Theta \wedge r=r_3}$ (see Figure 3d) over the interval $\Theta = [\Theta_5, \Theta_6] = [\Theta_5, \Theta_5 + \tau_{\Theta4}]$, the integration constants $c4_{h4}^\ominus$ and $d4_{h4}^\ominus$ are determined in Appendix B with:

$$c4_{h4}^\ominus = \frac{2}{\tau_{\Theta4}} \cdot \int_{\Theta_5}^{\Theta_5 + \tau_{\Theta4}} \frac{A_{z1}|_{r=r_2}}{r_2} \cdot \sin [\beta_{4h4} \cdot (\Theta - \Theta_5)] \cdot d\Theta, \tag{19a}$$

$$d4_{h4}^\ominus = \frac{2}{\tau_{\Theta4}} \cdot \int_{\Theta_5}^{\Theta_5 + \tau_{\Theta4}} \frac{A_{z2}|_{r=r_3}}{r_3} \cdot \sin [\beta_{4h4} \cdot (\Theta - \Theta_5)] \cdot d\Theta. \tag{19b}$$

With a weighting function $g(r) = r^{-1}$ and using a Fourier series expansion of $A_{z7}|_{\Theta=\Theta_5 \wedge \forall r}$ (see Figure 3d) over the interval $r = [r_2, r_3]$, the integration constant $e4_{n4}^r$ is determined in Appendix C with:

$$e4_{n4}^r = \frac{2}{\tau_{r4}} \cdot \int_{r_2}^{r_3} \frac{1}{r} \cdot \frac{A_{z7}|_{\Theta=\Theta_5}}{r_2} \cdot \sin \left[\lambda_{4n4} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr. \tag{20}$$

2.5.5. Region 5

For Region 5, the general solution is given according to the BCs of Case-Study No. 1 (i.e., A_z imposed on all edges of a region) in Appendix B. Therefore, A_{z5} satisfying the BCs of Figure 3e and the solution of Equation (1a) is given by:

$$A_{z5} = A_{z5}^\ominus + A_{z5}^r, \tag{21a}$$

$$A_{z5}^\ominus = \sum_{h5=1}^\infty \left[c5_{h5}^\ominus \cdot r_2 \cdot \frac{E_\phi(\beta5_{h5}, r_3, r)}{E_\phi(\beta5_{h5}, r_3, r_2)} + d5_{h5}^\ominus \cdot r_3 \cdot \frac{E_\phi(\beta5_{h5}, r, r_2)}{E_\phi(\beta5_{h5}, r_3, r_2)} \right] \cdot \sin [\beta5_{h5} \cdot (\Theta - \Theta_3)], \tag{21b}$$

$$A_{z5}^r = \sum_{n5=1}^\infty \left\{ e5_{n5}^r \cdot \frac{sh[\lambda5_{n5} \cdot (\Theta_4 - \Theta)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} + f5_{n5}^r \cdot \frac{sh[\lambda5_{n5} \cdot (\Theta - \Theta_3)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} \right\} \cdot r_2 \cdot \sin \left[\lambda5_{n5} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{21c}$$

the r -component of \mathbf{B}_5 by:

$$B_{r5} = B_{r5}^\ominus + B_{r5}^r, \tag{22a}$$

$$B_{r5}^\ominus = \sum_{h5=1}^\infty \beta5_{h5} \cdot \left[c5_{h5}^\ominus \cdot \frac{r_2}{r} \cdot \frac{E_\phi(\beta5_{h5}, r_3, r)}{E_\phi(\beta5_{h5}, r_3, r_2)} + d5_{h5}^\ominus \cdot \frac{r_3}{r} \cdot \frac{E_\phi(\beta5_{h5}, r, r_2)}{E_\phi(\beta5_{h5}, r_3, r_2)} \right] \cdot \cos [\beta5_{h5} \cdot (\Theta - \Theta_3)], \tag{22b}$$

$$B_{r5}^r = \sum_{n5=1}^\infty \lambda5_{n5} \cdot \left\{ -e5_{n5}^r \cdot \frac{ch[\lambda5_{n5} \cdot (\Theta_4 - \Theta)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} + f5_{n5}^r \cdot \frac{ch[\lambda5_{n5} \cdot (\Theta - \Theta_3)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} \right\} \cdot \frac{r_2}{r} \cdot \sin \left[\lambda5_{n5} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{22c}$$

the Θ -component of \mathbf{B}_5 by:

$$B_{\Theta5} = B_{\Theta5}^\ominus + B_{\Theta5}^r, \tag{23a}$$

$$B_{\Theta5}^\ominus = \sum_{h5=1}^\infty \beta5_{h5} \cdot \left[c5_{h5}^\ominus \cdot \frac{r_2}{r} \cdot \frac{P_\phi(\beta5_{h5}, r_3, r)}{E_\phi(\beta5_{h5}, r_3, r_2)} - d5_{h5}^\ominus \cdot \frac{r_3}{r} \cdot \frac{P_\phi(\beta5_{h5}, r, r_2)}{E_\phi(\beta5_{h5}, r_3, r_2)} \right] \cdot \sin [\beta5_{h5} \cdot (\Theta - \Theta_3)], \tag{23b}$$

$$B_{\Theta5}^r = - \sum_{n5=1}^\infty \lambda5_{n5} \cdot \left\{ e5_{n5}^r \cdot \frac{sh[\lambda5_{n5} \cdot (\Theta_4 - \Theta)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} + f5_{n5}^r \cdot \frac{sh[\lambda5_{n5} \cdot (\Theta - \Theta_3)]}{sh(\lambda5_{n5} \cdot \tau_{\Theta5})} \right\} \cdot \frac{r_2}{r} \cdot \cos \left[\lambda5_{n5} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{23c}$$

where $h5$ and $n5$ are the spatial harmonic orders in Region 5; $c5_{h5}^\ominus$, $d5_{h5}^\ominus$, $e5_{n5}^r$ and $f5_{n5}^r$ the integration constants; $\beta5_{h5} = h5 \cdot \pi / \tau_{\Theta5}$ with $\tau_{\Theta5} = \Theta_4 - \Theta_3$; and $\lambda5_{n5} = n5 \cdot \pi / \tau_{r5}$ with $\tau_{r5} = \ln(r_3 / r_2)$.

Using Fourier series expansion of $A_{z1}|_{\forall \Theta \wedge r=r_2}$ and $A_{z2}|_{\forall \Theta \wedge r=r_3}$ (see Figure 3e) over the interval $\Theta = [\Theta_3, \Theta_4] = [\Theta_3, \Theta_3 + \tau_{\Theta5}]$, the integration constants $c5_{h5}^\ominus$ and $d5_{h5}^\ominus$ are determined in Appendix C with:

$$c5_{h5}^\ominus = \frac{2}{\tau_{\Theta5}} \cdot \int_{\Theta_3}^{\Theta_3 + \tau_{\Theta5}} \frac{A_{z1}|_{r=r_2}}{r_2} \cdot \sin [\beta5_{h5} \cdot (\Theta - \Theta_3)] \cdot d\Theta, \tag{24a}$$

$$d5_{h5}^\ominus = \frac{2}{\tau_{\Theta5}} \cdot \int_{\Theta_3}^{\Theta_3 + \tau_{\Theta5}} \frac{A_{z2}|_{r=r_3}}{r_3} \cdot \sin [\beta5_{h5} \cdot (\Theta - \Theta_3)] \cdot d\Theta. \tag{24b}$$

With a weighting function $g(r) = r^{-1}$ and using a Fourier series expansion of $A_{z6}|_{\Theta=\Theta_3 \wedge \forall r}$ and $A_{z7}|_{\Theta=\Theta_4 \wedge \forall r}$ (see Figure 3e) over the interval $r = [r_2, r_3]$, the integration constants $e5_{n5}^r$ and $f5_{n5}^r$ are determined in Appendix C with:

$$e5_{n5}^r = \frac{2}{\tau_{r5}} \cdot \int_{r_2}^{r_3} \frac{1}{r} \cdot \frac{A_{z6}|_{\Theta=\Theta_3}}{r_2} \cdot \sin \left[\lambda5_{n5} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr, \tag{25a}$$

$$f5_{n5}^r = \frac{2}{\tau_{r5}} \cdot \int_{r_2}^{r_3} \frac{1}{r} \cdot \frac{A_{z7}|_{\Theta=\Theta_4}}{r_2} \cdot \sin \left[\lambda5_{n5} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr. \tag{25b}$$

2.5.6. Region 6

For Region 6, the general solution is given according to the BCs of Case-Study No. 2 (i.e., B_r and A_z are respectively imposed on r - and Θ -edges of a region) in Appendix B. Therefore, A_{z6} satisfying the BCs of Figure 3f and the solution of Equation (1b) is given by:

$$A_{z6} = A_{z6}^\Theta + A_{z6}^r + A_{zP6}, \tag{26a}$$

$$A_{z6}^\Theta = \left[c6_0^\Theta \cdot r_2 \cdot \frac{\ln(r_3/r_2)}{\ln(r_3/r_2)} + d6_0^\Theta \cdot r_3 \cdot \frac{\ln(r/r_2)}{\ln(r_3/r_2)} \right. \\ \left. \cdots + \sum_{h6=1}^\infty \left[c6_{h6}^\Theta \cdot r_2 \cdot \frac{E_f(\beta6_{h6}, r_3, r)}{E_f(\beta6_{h6}, r_3, r_2)} + d6_{h6}^\Theta \cdot r_3 \cdot \frac{E_f(\beta6_{h6}, r, r_2)}{E_f(\beta6_{h6}, r_3, r_2)} \right] \cdot \cos [\beta6_{h6} \cdot (\Theta - \Theta_2)] \right], \tag{26b}$$

$$A_{z6}^r = \sum_{n6=1}^\infty \left\{ e6_{n6}^r \cdot \frac{ch[\lambda6_{n6} \cdot (\Theta - \Theta_2)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} - f6_{n6}^r \cdot \frac{ch[\lambda6_{n6} \cdot (\Theta_3 - \Theta)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} \right\} \cdot \frac{r_2}{\lambda6_{n6}} \cdot \sin \left[\lambda6_{n6} \cdot \ln \left(\frac{r}{r_2} \right) \right]. \tag{26c}$$

Considering Equations (26b) and (26c), as well as the form of the current density distribution, i.e., Equation (2), a particular solution A_{zP6} can be found. The following particular solution is proposed:

$$A_{zP6} = -\frac{1}{4} \cdot r^2 \cdot \mu_6 \cdot J_{z6}. \tag{26d}$$

The r -component of \mathbf{B}_6 is defined by:

$$B_{r6} = B_{r6}^\Theta + B_{r6}^r + B_{rP6}, \tag{27a}$$

$$B_{r6}^\Theta = - \sum_{h6=1}^\infty \beta6_{h6} \cdot \left[c6_{h6}^\Theta \cdot \frac{r_2}{r} \cdot \frac{E_f(\beta6_{h6}, r_3, r)}{E_f(\beta6_{h6}, r_3, r_2)} + d6_{h6}^\Theta \cdot \frac{r_3}{r} \cdot \frac{E_f(\beta6_{h6}, r, r_2)}{E_f(\beta6_{h6}, r_3, r_2)} \right] \cdot \sin [\beta6_{h6} \cdot (\Theta - \Theta_2)], \tag{27b}$$

$$B_{r6}^r = \sum_{n6=1}^\infty \left\{ e6_{n6}^r \cdot \frac{sh[\lambda6_{n6} \cdot (\Theta - \Theta_2)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} + f6_{n6}^r \cdot \frac{sh[\lambda6_{n6} \cdot (\Theta_3 - \Theta)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} \right\} \cdot \frac{r_2}{r} \cdot \sin \left[\lambda6_{n6} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{27c}$$

$$B_{rP6} = \frac{1}{r} \cdot \frac{\partial A_{zP6}}{\partial \Theta} = 0, \tag{27d}$$

and the Θ -component of \mathbf{B}_6 by:

$$B_{\Theta6} = B_{\Theta6}^\Theta + B_{\Theta6}^r + B_{\Theta P6}, \tag{28a}$$

$$B_{\Theta6}^\Theta = \left[c6_0^\Theta \cdot \frac{r_2}{r} \cdot \frac{1}{\ln(r_3/r_2)} - d6_0^\Theta \cdot \frac{r_3}{r} \cdot \frac{1}{\ln(r_3/r_2)} \right. \\ \left. \cdots + \sum_{h6=1}^\infty \beta6_{h6} \cdot \left[c6_{h6}^\Theta \cdot \frac{r_2}{r} \cdot \frac{P_f(\beta6_{h6}, r_3, r)}{E_f(\beta6_{h6}, r_3, r_2)} - d6_{h6}^\Theta \cdot \frac{r_3}{r} \cdot \frac{P_f(\beta6_{h6}, r, r_2)}{E_f(\beta6_{h6}, r_3, r_2)} \right] \cdot \cos [\beta6_{h6} \cdot (\Theta - \Theta_2)] \right], \tag{28b}$$

$$B_{\Theta6}^r = - \sum_{n6=1}^\infty \left\{ e6_{n6}^r \cdot \frac{ch[\lambda6_{n6} \cdot (\Theta - \Theta_2)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} - f6_{n6}^r \cdot \frac{ch[\lambda6_{n6} \cdot (\Theta_3 - \Theta)]}{sh(\lambda6_{n6} \cdot \tau_{\Theta6})} \right\} \cdot \frac{r_2}{r} \cdot \cos \left[\lambda6_{n6} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{28c}$$

$$B_{\Theta P6} = -\frac{\partial A_{zP6}}{\partial r} = \frac{1}{2} \cdot r \cdot \mu_6 \cdot J_{z6}, \tag{28d}$$

where $h6$ and $n6$ are the spatial harmonic orders in Region 6; $c6_0^\Theta$, $d6_0^\Theta$, $c6_{h6}^\Theta$, $d6_{h6}^\Theta$, $e6_{n6}^r$ and $f6_{n6}^r$ the integration constants; $\beta6_{h6} = h6 \cdot \pi / \tau_{\Theta6}$ with $\tau_{\Theta6} = \Theta_3 - \Theta_2$; and $\lambda6_{n6} = n6 \cdot \pi / \tau_{r6}$ with $\tau_{r6} = \ln(r_3/r_2)$.

Using Fourier series expansion of $A_{z1}|_{\forall \Theta \wedge r=r_2}$ and $A_{z2}|_{\forall \Theta \wedge r=r_3}$ (see Figure 3f) over the interval $\Theta = [\Theta_2, \Theta_3] = [\Theta_2, \Theta_2 + \tau_{\Theta6}]$, the integration constants $c6_0^\Theta$ and $c6_{h6}^\Theta$ and $d6_0^\Theta$ and $d6_{h6}^\Theta$ are determined in Appendix C with:

$$c6_0^\Theta = \frac{1}{\tau_{\Theta6}} \cdot \int_{\Theta_2}^{\Theta_2 + \tau_{\Theta6}} \frac{1}{r_2} \cdot \left[A_{z1}|_{r=r_2} - A_{zP6}|_{r=r_2} \right] \cdot d\Theta, \tag{29a}$$

$$c6_{h6}^x = \frac{2}{\tau_{\Theta 6}} \cdot \int_{\Theta_2}^{\Theta_2 + \tau_{\Theta 6}} \frac{1}{r_2} \cdot [A_{z1}|_{r=r_2} - A_{zP6}|_{r=r_2}] \cdot \cos [\beta 6_{h6} \cdot (\Theta - \Theta_2)] \cdot d\Theta, \tag{29b}$$

$$d6_0^{\Theta} = \frac{1}{\tau_{\Theta 6}} \cdot \int_{\Theta_2}^{\Theta_2 + \tau_{\Theta 6}} \frac{1}{r_3} \cdot [A_{z2}|_{r=r_3} - A_{zP6}|_{r=r_3}] \cdot d\Theta, \tag{29c}$$

$$d6_{h6}^x = \frac{2}{\tau_{\Theta 6}} \cdot \int_{\Theta_2}^{\Theta_2 + \tau_{\Theta 6}} \frac{1}{r_3} \cdot [A_{z2}|_{r=r_3} - A_{zP6}|_{r=r_3}] \cdot \cos [\beta 6_{h6} \cdot (\Theta - \Theta_2)] \cdot d\Theta. \tag{29d}$$

Using a Fourier series expansion of $\mu_6/\mu_5 \cdot B_{r5}|_{\Theta=\Theta_3 \wedge \forall r}$ and $\mu_6/\mu_3 \cdot B_{r3}|_{\Theta=\Theta_2 \wedge \forall r}$ (see Figure 3f) over the interval $r = [r_2, r_3]$, the integration constants $e6_{n6}^r$ and $f6_{n6}^r$ are determined in Appendix C with:

$$e6_{n6}^r = \frac{2}{\tau_{r6}} \cdot \int_{r_2}^{r_3} \frac{1}{r_2} \cdot \left[\frac{\mu_6}{\mu_5} \cdot B_{r5}|_{\Theta=\Theta_3} - B_{rP6}|_{\Theta=\Theta_3} \right] \cdot \sin \left[\lambda 6_{n6} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr, \tag{30a}$$

$$f6_{n6}^r = \frac{2}{\tau_{r6}} \cdot \int_{r_2}^{r_3} \frac{1}{r_2} \cdot \left[\frac{\mu_6}{\mu_3} \cdot B_{r3}|_{\Theta=\Theta_2} - B_{rP6}|_{\Theta=\Theta_2} \right] \cdot \sin \left[\lambda 6_{n6} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr. \tag{30b}$$

2.5.7. Region 7

The solution in Region 7 is using the same development as Region 6. Thus, A_{z7} satisfying the BCs of Figure 3g and the solution of Equation (2) is defined by:

$$A_{z7} = A_{z7}^{\Theta} + A_{z7}^r + A_{zP7}, \tag{31a}$$

$$A_{z7}^{\Theta} = \left[c7_0^{\Theta} \cdot r_2 \cdot \frac{\ln(r_3/r)}{\ln(r_3/r_2)} + d7_0^{\Theta} \cdot r_3 \cdot \frac{\ln(r/r_2)}{\ln(r_3/r_2)} \right. \\ \left. \cdots + \sum_{h7=1}^{\infty} \left[c7_{h7}^{\Theta} \cdot r_2 \cdot \frac{E_{\psi}(\beta 7_{h7}, r_3, r)}{E_{\psi}(\beta 7_{h7}, r_3, r_2)} + d7_{h7}^{\Theta} \cdot r_3 \cdot \frac{E_{\psi}(\beta 7_{h7}, r, r_2)}{E_{\psi}(\beta 7_{h7}, r_3, r_2)} \right] \cdot \cos [\beta 7_{h7} \cdot (\Theta - \Theta_4)] \right], \tag{31b}$$

$$A_{z7}^r = \sum_{n7=1}^{\infty} \left\{ e7_{n7}^r \cdot \frac{ch[\lambda 7_{n7} \cdot (\Theta - \Theta_4)]}{sh(\lambda 7_{n7} \cdot \tau_{\Theta 7})} - f7_{n7}^r \cdot \frac{ch[\lambda 7_{n7} \cdot (\Theta_5 - \Theta)]}{sh(\lambda 7_{n7} \cdot \tau_{\Theta 7})} \right\} \cdot \frac{r_2}{\lambda 7_{n7}} \cdot \sin \left[\lambda 7_{n7} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{31c}$$

$$A_{zP7} = -\frac{1}{4} \cdot r^2 \cdot \mu_7 \cdot J_{z7}. \tag{31d}$$

The r -component of \mathbf{B}_7 is defined by:

$$B_{r7} = B_{r7}^{\Theta} + B_{r7}^r + B_{rP7}, \tag{32a}$$

$$B_{r7}^{\Theta} = - \sum_{h7=1}^{\infty} \beta 7_{h7} \cdot \left[c7_{h7}^{\Theta} \cdot \frac{r_2}{r} \cdot \frac{E_{\psi}(\beta 7_{h7}, r_3, r)}{E_{\psi}(\beta 7_{h7}, r_3, r_2)} + d7_{h7}^{\Theta} \cdot \frac{r_3}{r} \cdot \frac{E_{\psi}(\beta 7_{h7}, r, r_2)}{E_{\psi}(\beta 7_{h7}, r_3, r_2)} \right] \cdot \sin [\beta 7_{h7} \cdot (\Theta - \Theta_4)], \tag{32b}$$

$$B_{r7}^r = \sum_{n7=1}^{\infty} \left\{ e7_{n7}^r \cdot \frac{sh[\lambda 7_{n7} \cdot (\Theta - \Theta_4)]}{sh(\lambda 7_{n7} \cdot \tau_{\Theta 7})} + f7_{n7}^r \cdot \frac{sh[\lambda 7_{n7} \cdot (\Theta_5 - \Theta)]}{sh(\lambda 7_{n7} \cdot \tau_{\Theta 7})} \right\} \cdot \frac{r_2}{r} \cdot \sin \left[\lambda 7_{n7} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{32c}$$

$$B_{rP7} = \frac{1}{r} \cdot \frac{\partial A_{zP7}}{\partial \Theta} = 0, \tag{32d}$$

and the Θ -component of \mathbf{B}_7 by:

$$B_{\Theta 7} = B_{\Theta 7}^{\Theta} + B_{\Theta 7}^r + B_{\Theta P7}, \tag{33a}$$

$$B_{\Theta 7}^{\Theta} = \left[c7_0^{\Theta} \cdot \frac{r_2}{r} \cdot \frac{1}{\ln(r_3/r_2)} - d7_0^{\Theta} \cdot \frac{r_3}{r} \cdot \frac{1}{\ln(r_3/r_2)} \right. \\ \left. \dots + \sum_{h7=1}^{\infty} \beta7_{h7} \cdot \left[c7_{h7}^{\Theta} \cdot \frac{r_2}{r} \cdot \frac{P_4(\beta7_{h7}, r, r_2)}{E_4^*(\beta7_{h7}, r_3, r_2)} - d7_{h7}^{\Theta} \cdot \frac{r_3}{r} \cdot \frac{P_4(\beta7_{h7}, r, r_2)}{E_4^*(\beta7_{h7}, r_3, r_2)} \right] \cdot \cos [\beta7_{h7} \cdot (\Theta - \Theta_4)] \right], \tag{33b}$$

$$B_{\Theta 7}^r = - \sum_{n7=1}^{\infty} \left\{ e7_{n7}^r \cdot \frac{ch[\lambda7_{n7} \cdot (\Theta - \Theta_4)]}{sh(\lambda7_{n7} \cdot \tau_{\Theta 7})} - f7_{n7}^r \cdot \frac{ch[\lambda7_{n7} \cdot (\Theta_5 - \Theta)]}{sh(\lambda7_{n7} \cdot \tau_{\Theta 7})} \right\} \cdot \frac{r_2}{r} \cdot \cos \left[\lambda7_{n7} \cdot \ln \left(\frac{r}{r_2} \right) \right], \tag{33c}$$

$$B_{\Theta P7} = - \frac{\partial A_{zP7}}{\partial r} = \frac{1}{2} \cdot r \cdot \mu_7 \cdot J_{z7}, \tag{33d}$$

where $h7$ and $n7$ are the spatial harmonic orders in Region 7; $c7_0^{\Theta}$, $d7_0^{\Theta}$, $c7_{h7}^{\Theta}$, $d7_{h7}^{\Theta}$, $e7_{n7}^r$ and $f7_{n7}^r$ the integration constants; $\beta7_{h7} = h7 \cdot \pi / \tau_{\Theta 7}$ with $\tau_{\Theta 7} = \Theta_5 - \Theta_4$; and $\lambda7_{n7} = n7 \cdot \pi / \tau_{r7}$ with $\tau_{r7} = \ln(r_3/r_2)$.

Using Fourier series expansion of $A_{z1}|_{\forall \Theta \wedge r=r_2}$ and $A_{z2}|_{\forall \Theta \wedge r=r_3}$ (see Figure 3g) over the interval $\Theta = [\Theta_4, \Theta_5] = [\Theta_4, \Theta_4 + \tau_{\Theta 7}]$, the integration constants $c7_0^{\Theta}$ and $c7_{h7}^{\Theta}$ and $d7_0^{\Theta}$ and $d7_{h7}^{\Theta}$ are determined in Appendix C with:

$$c7_0^{\Theta} = \frac{1}{\tau_{\Theta 7}} \cdot \int_{\Theta_4}^{\Theta_4 + \tau_{\Theta 7}} \frac{1}{r_2} \cdot [A_{z1}|_{r=r_2} - A_{zP7}|_{r=r_2}] \cdot d\Theta, \tag{34a}$$

$$c7_{h7}^{\Theta} = \frac{2}{\tau_{\Theta 7}} \cdot \int_{\Theta_4}^{\Theta_4 + \tau_{\Theta 7}} \frac{1}{r_2} \cdot [A_{z1}|_{r=r_2} - A_{zP7}|_{r=r_2}] \cdot \cos [\beta7_{h7} \cdot (\Theta - \Theta_4)] \cdot d\Theta, \tag{34b}$$

$$d7_0^{\Theta} = \frac{1}{\tau_{\Theta 7}} \cdot \int_{\Theta_4}^{\Theta_4 + \tau_{\Theta 7}} \frac{1}{r_3} \cdot [A_{z2}|_{r=r_3} - A_{zP7}|_{r=r_3}] \cdot d\Theta, \tag{34c}$$

$$d7_{h7}^{\Theta} = \frac{2}{\tau_{\Theta 7}} \cdot \int_{\Theta_4}^{\Theta_4 + \tau_{\Theta 7}} \frac{1}{r_3} \cdot [A_{z2}|_{r=r_3} - A_{zP7}|_{r=r_3}] \cdot \cos [\beta7_{h7} \cdot (\Theta - \Theta_4)] \cdot d\Theta. \tag{34d}$$

Using a Fourier series expansion of $\mu_7/\mu_4 \cdot B_{r4}|_{\Theta=\Theta_5 \wedge \forall r}$ and $\mu_7/\mu_5 \cdot B_{r5}|_{\Theta=\Theta_4 \wedge \forall r}$ (see Figure 3g) over the interval $r = [r_2, r_3]$, the integration constants $e7_{n7}^r$ and $f7_{n7}^r$ are determined in Appendix C with:

$$e7_{n7}^r = \frac{2}{\tau_{r7}} \cdot \int_{r_2}^{r_3} \frac{1}{r_2} \cdot \left[\frac{\mu_7}{\mu_4} \cdot B_{r4}|_{\Theta=\Theta_5} - B_{rP7}|_{\Theta=\Theta_5} \right] \cdot \sin \left[\lambda7_{n7} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr, \tag{35a}$$

$$f7_{n7}^r = \frac{2}{\tau_{r7}} \cdot \int_{r_2}^{r_3} \frac{1}{r_2} \cdot \left[\frac{\mu_7}{\mu_5} \cdot B_{r5}|_{\Theta=\Theta_4} - B_{rP7}|_{\Theta=\Theta_4} \right] \cdot \sin \left[\lambda7_{n7} \cdot \ln \left(\frac{r}{r_2} \right) \right] \cdot dr. \tag{35b}$$

3. Validation of the Semi-Analytic Method with Finite-Element Analysis

3.1. Introduction

The objective of this section is to validate the 2-D subdomain technique in polar coordinates (r, Θ) on the magnetic field distribution in relation to the numerical method. The physical and geometrical parameters of studied electromagnetic device are given in Table 1.

Table 1. Physical and geometrical parameters of the air- or iron-cored coil.

Parameters, Symbols (Units)	Values
Number of turns of the coil, N_t (-)	60
Supply current, I (A)	20
Conductor surface, S_c (mm ²)	120
Current density of the coil, J_{zk} (A/mm ²)	± 10
Effective axial length, L_z (mm)	60
Geometrical parameters in the Θ -axis, $\{\Theta_1; \Theta_2; \Theta_3; \Theta_4; \Theta_5; \Theta_6\}$ (deg.)	$\{0; 17; 21; 29; 33; 50\}$
Geometrical parameters in the r -axis, $\{r_1; r_2; r_3; r_4\}$ (mm)	$\{21; 81; 100; 160\}$
Relative magnetic permeability of the iron, μ_{iron} (-)	1,500
Number of harmonics for Region 1, $H1_{max}$ (-)	260
Number of harmonics for Region 2, $H2_{max}$ (-)	260
Number of harmonics for Region 3, $\{H3_{max}; N3_{max}\}$ (-)	$\{88; 124\}$
Number of harmonics for Region 4, $\{H4_{max}; N4_{max}\}$ (-)	$\{88; 124\}$
Number of harmonics for Region 5, $\{H5_{max}; N5_{max}\}$ (-)	$\{42; 124\}$
Number of harmonics for Region 6, $\{H6_{max}; N6_{max}\}$ (-)	$\{21; 124\}$
Number of harmonics for Region 7, $\{H7_{max}; N7_{max}\}$ (-)	$\{21; 124\}$

For this validation, the air- or iron-cored coil has been modeled using Cedrat’s Flux2D (Version 10.2.1, Altair Engineering, Meylan Cedex, France) software package (i.e., an advanced finite-element method-based numeric field analysis program) [40]. FEA is done with the same assumptions as the semi-analytical model (see Section 2.1). The linear system is given in Appendix C and has been implemented in MATLAB® (R2015a, MathWorks, Natick, MA, USA) by using the sparse matrix/vectors. A discussion of the numerical problems (viz., harmonics and ill-conditioned systems) of such semi-analytical models has been clarified in [1]. The Maxwell–Fourier methods exhibit a similar problem to the numerical methods due to the periodicity of Fourier series and, consequently, to the finite number of harmonics. Hence, A_z and $\mathbf{B} = \{B_r; B_\Theta; 0\}$ in the various regions (see Section 2.5) have been computed with a finite number of spatial harmonics terms $H1_{max}$ – $H7_{max}$ (for the Θ -edges) and $N3_{max}$ – $N7_{max}$ (for the r -edges). As indicated in [41,42], these spatial harmonics terms, given in Table 1, have been imposed according to an optimal ratio, i.e., for $H1_{max}$ given,

$$H_{\bullet max} = H1_{max} \cdot \frac{\tau_{\Theta \bullet}}{\tau_{\Theta 1}} \quad \text{and} \quad N_{\bullet max} = H_{\bullet max} \cdot \frac{\tau_{\Theta \bullet}}{\tau_{r \bullet}}. \tag{36}$$

The linear system size depends on the number of: (i) regions; (ii) BCs; and (iii) harmonics of each subdomain. In our study, the linear system named Equation (A17) consists of 2036 elements, which is much smaller than the 2-D FEA mesh having 3,081 surfaces elements of second order (viz., the triangles number of system) with the number of excellent quality elements equal to 100%. For information, the 2-D FEA mesh for an air- or iron-cored coil is illustrated in Figure 4. The personal computer used for this comparison has the following characteristics: HP Z800 Intel(R) Xeon(R) CPU @ 2.4 GHz (with two processors) RAM 16 Go 64 bits. The computation time of 2-D subdomain model is divided by two (viz., 0.5 s for 2-D subdomain model and 1 s for the 2-D FEA).

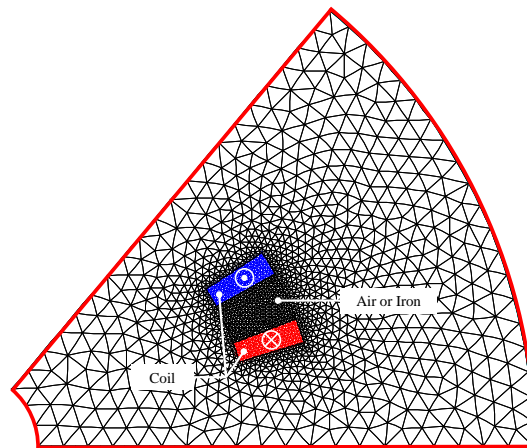


Figure 4. 2-D Finite-Element Analysis (FEA) mesh for the air- or iron-cored coil.

3.2. Results Discussion

The validation paths of A_z and $\mathbf{B} = \{B_r; B_\Theta; 0\}$ for the semi-analytic and numeric comparison are given in Figure 5.

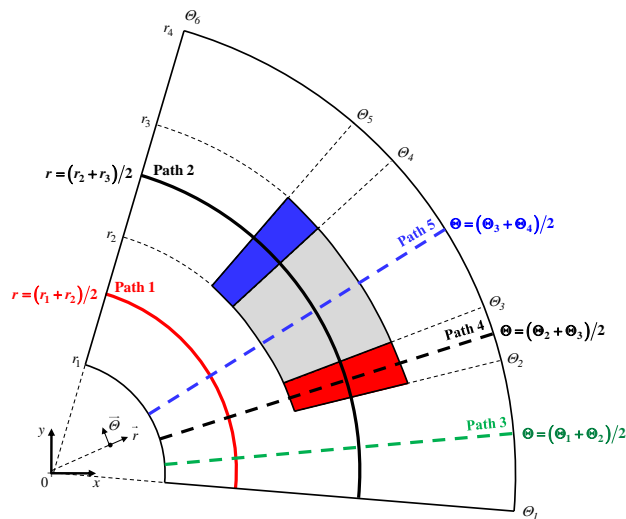


Figure 5. Validation paths for the semi-analytic and numeric comparison.

The waveforms of global quantities are shown on different paths in Figure 6 for A_z and in Figures 7–11 for the components of \mathbf{B} . The solid lines represent the global quantities computed by the 2-D FEA, and the circles correspond to the 2-D subdomain model. Comparing those results with 2-D FEA, it can be shown that a very good evaluation is obtained for A_z and for the components of \mathbf{B} , whatever the paths, for both the air- and iron-core. This confirms that the effect of global saturation can be taken into account accurately. According to the concept of symmetry, it can be seen that in polar coordinates, there is only one symmetry of A_z on Path 5 (viz., $B_r \neq 0$ and $B_\Theta = 0$ in Figure 11) unlike the same electromagnetic device in Cartesian coordinates. Indeed, in Cartesian coordinates, there exist two symmetry axes of A_z on Path 2 and Path 5 [1]. In polar coordinates, Path 2 does not correspond to a symmetry axis of A_z ; consequently, $B_r \neq 0$ and $B_\Theta \neq 0$ in Figure 8. It will be noted that the r -component of \mathbf{B} in Region 5 is more intense with the magnetic core (see Figure 8a) and that the magnetic leakages in the middle of the device in the Θ -axis are equivalent for an air- and iron-cored coil (see Figure 8b). It is interesting to note that numerical peaks appear in the FEA results

(see Figures 6e, 7, 8b and 11b), which are mainly due to the mesh. The relative error is less than 1.5% for the various global quantities (see Figure 6a,c for the maximum error).

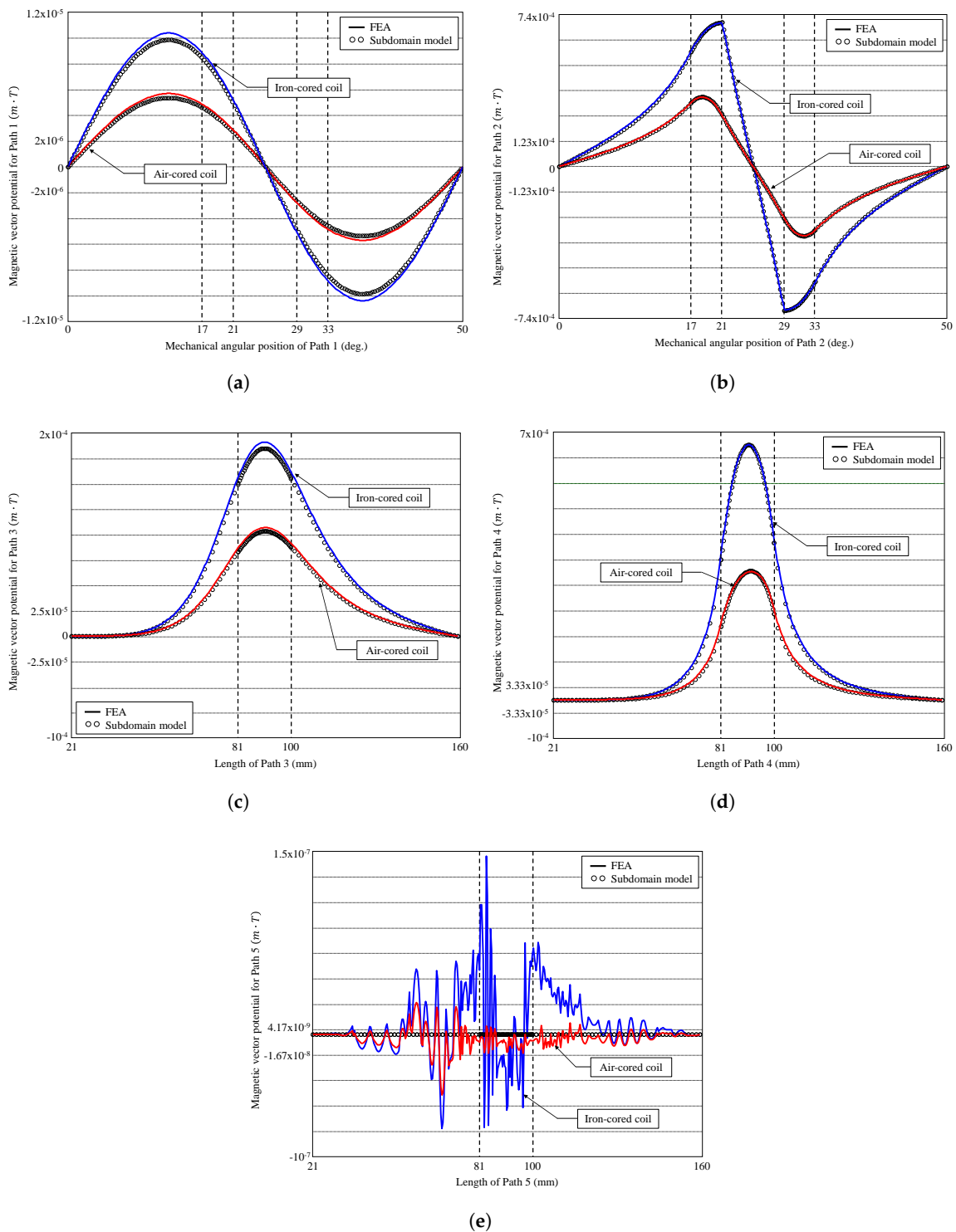


Figure 6. Waveforms of A_z for: (a) Path 1; (b) Path 2; (c) Path 3; (d) Path 4; and (e) Path 5.

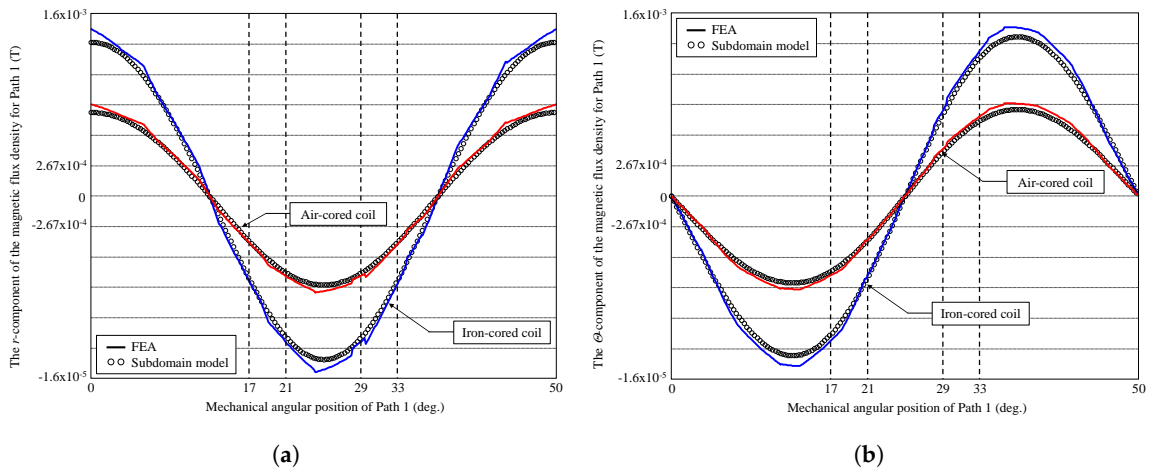


Figure 7. Waveforms of \mathbf{B} for Path 1: (a) r - and (b) Θ -component.

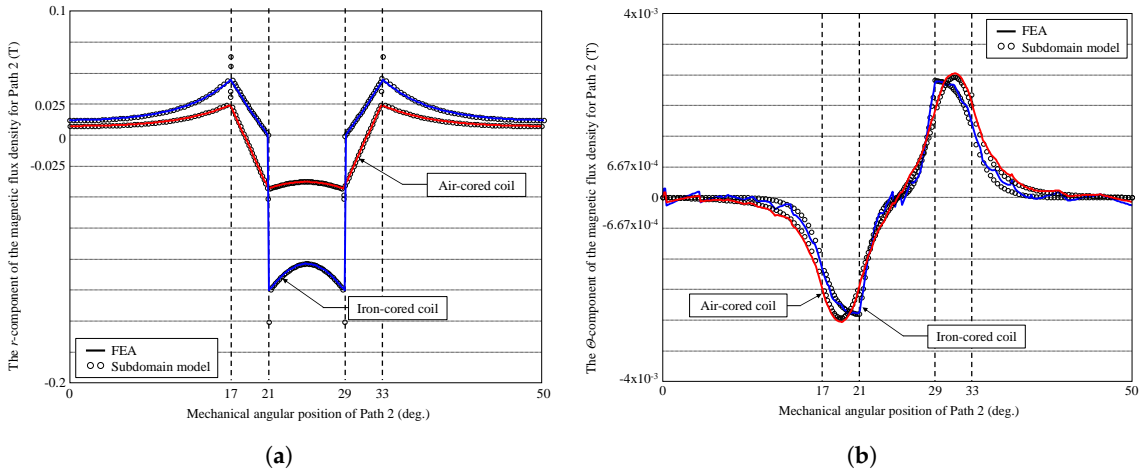


Figure 8. Waveforms of \mathbf{B} for Path 2: (a) r - and (b) Θ -component.

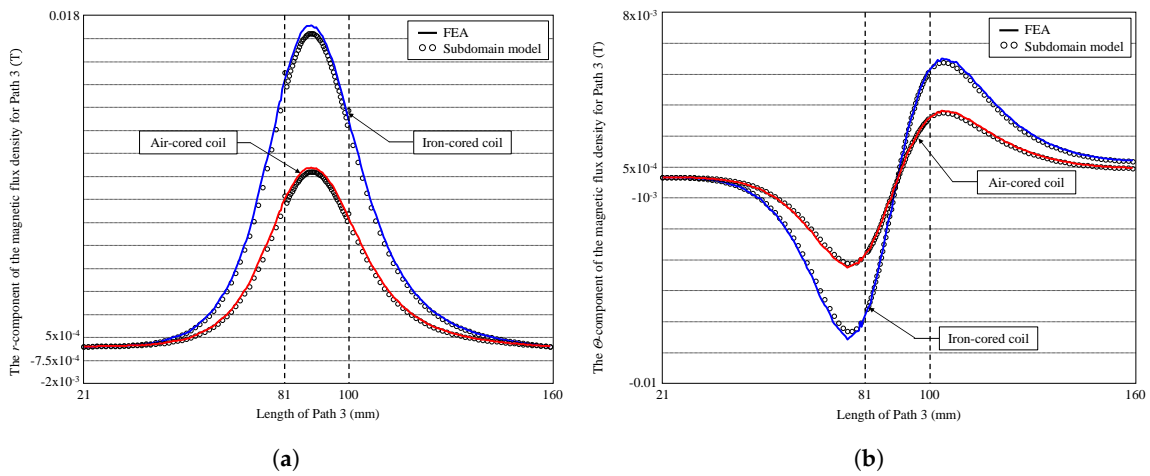


Figure 9. Waveforms of \mathbf{B} for Path 3: (a) r - and (b) Θ -component.

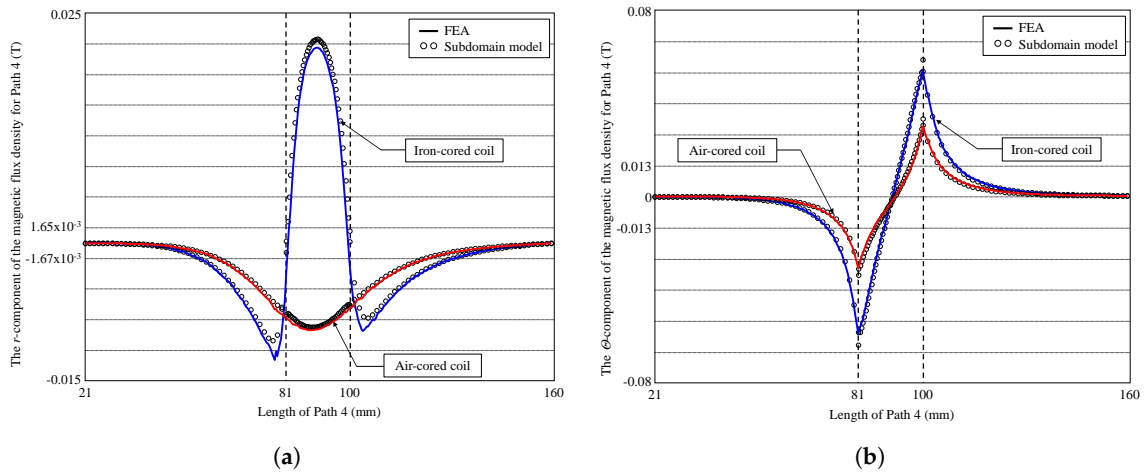


Figure 10. Waveforms of B for Path 4: (a) r - and (b) Θ -component.

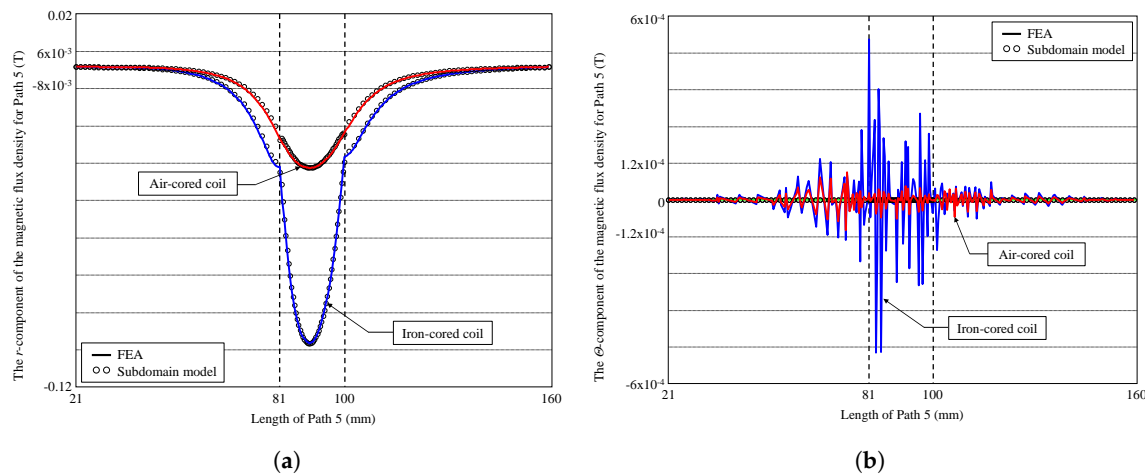


Figure 11. Waveforms of B for Path 5: (a) r - and (b) Θ -component.

4. Conclusions

It has been demonstrated that there exists no exact semi-analytical model based on the 2-D subdomain technique in polar coordinates taking into account iron parts with(out) the nonlinear $B(H)$ curve. An improved 2-D subdomain method in polar coordinates (r, Θ) to study the magnetic field distribution in the iron parts with a finite relative permeability has been presented in this paper. Nevertheless, the research work is an extension of [1] in polar coordinates (r, Θ) .

The proposed new subdomain model is applied to an air- or iron-cored coil supplied by a constant current. The magnetic field solutions in the subdomains and the BCs between regions are carried out in the two directions (i.e., r - and Θ -axis). The iron relative permeability used in this model is constant and corresponds to the linear part of the nonlinear $B(H)$ curve. However, the whole $B(H)$ curve of the magnetic material can be applied with an iterative algorithm as in [29,30,34]. The proposed subdomain method in polar coordinates (r, Θ) takes less computing time than the FEA (approximately two-fold versus to FEA). It is very suitable for the design and optimization of the electromechanical systems in general and electrical machines in particular. The semi-analytical results have been validated with FEA, and good agreement has been obtained in both amplitudes and waveforms.

The major scientific contribution could be applied to rotating electrical machines (e.g., radial-flux machines) in polar coordinates with(out) magnets supplied by a direct or alternate current (with any waveforms). Moreover, one advantage of this technique would be their exploitation in

three-dimensional studies in order to reduce the computation time, which remains a major problem in this numerical method.

Author Contributions: The work presented here was carried out in cooperation among all authors, which have written the paper and have gave advice for the manuscripts.

Conflicts of Interest: The authors declare no conflict of interest.

Appendix A. The 2-D General Solution of PDEs (i.e., Laplace’s and Poisson’s Equations) in Polar Coordinates

Using the magnetostatic Maxwell’s equations (viz., the Maxwell–Ampere law, the Maxwell–Thomson law and the magnetic material equation) [1], the general PDEs in terms of magnetic vector potential $\mathbf{A} = \{0; 0; A_z\}$ with $\mu = C^{st}$ can be expressed in polar coordinates (r, Θ) by:

$$\Delta A_z = \frac{\partial^2 A_z}{\partial r^2} + \frac{1}{r} \cdot \frac{\partial A_z}{\partial r} + \frac{1}{r^2} \cdot \frac{\partial^2 A_z}{\partial \Theta^2} = ES, \tag{A1a}$$

$$ES = - \left[\mu \cdot J_z + \frac{\mu_0}{r} \cdot \left(M_\Theta + r \cdot \frac{\partial M_\Theta}{\partial r} - \frac{\partial M_r}{\partial \Theta} \right) \right]. \tag{A1b}$$

where $\mathbf{J} = \{0; 0; J_z\}$ is the current density (due to supply currents) vector, $\mathbf{M} = \{M_r; M_\Theta; 0\}$ is the magnetization vector (with $\mathbf{M} = 0$ for the vacuum/iron or $\mathbf{M} \neq 0$ for the magnets according to the magnetization direction [43]) and $\mu = \mu_0 \cdot \mu_r$ is the absolute magnetic permeability of the magnetic material in which μ_0 and μ_r are respectively the vacuum permeability and the relative permeability of the magnetic material (with $\mu_r = 1$ for the vacuum or $\mu_r \neq 1$ for the magnets/iron).

The magnetic vector potential A_z is governed by Poisson’s equation (i.e., $ES \neq 0$) or Laplace’s equation (i.e., $ES = 0$). Using the separation of variables method, the 2-D general solution of A_z in both directions (i.e., r - and Θ -edges) can be written as Fourier’s series:

$$A_z = A_z^\Theta + A_z^r + A_{zP}, \tag{A2a}$$

$$A_z^\Theta = \left[\begin{array}{l} [C_0^\Theta + D_0^\Theta \cdot \ln(r)] \cdot (E_0^\Theta + F_0^\Theta \cdot \Theta) \\ \dots + \sum_{h=1}^\infty \left(\begin{array}{l} C_h^\Theta \cdot r^{\beta_h} \\ \dots + D_h^\Theta \cdot r^{-\beta_h} \end{array} \right) \cdot \left[\begin{array}{l} E_h^\Theta \cdot \cos(\beta_h \cdot \Theta) \\ \dots + F_h^\Theta \cdot \sin(\beta_h \cdot \Theta) \end{array} \right] \end{array} \right], \tag{A2b}$$

$$A_z^r = \left[\begin{array}{l} [C_0^r + D_0^r \cdot \ln(r)] \cdot (E_0^r + F_0^r \cdot \Theta) \\ \dots + \sum_{n=1}^\infty \left\{ \begin{array}{l} C_n^r \cdot \cos[\lambda_n \cdot \ln(r)] \\ \dots + D_n^r \cdot \sin[\lambda_n \cdot \ln(r)] \end{array} \right\} \cdot \left[\begin{array}{l} E_n^r \cdot ch(\lambda_n \cdot \Theta) \\ \dots + F_n^r \cdot sh(\lambda_n \cdot \Theta) \end{array} \right] \end{array} \right], \tag{A2c}$$

where A_{zP} is the particular solution of A_z respecting the second member ES in Equation (A1), C_0^Θ – F_h^Θ and C_0^r – F_h^r the integration constants, β_h and λ_n the spatial frequency (or periodicity) of A_z^Θ and A_z^r and h and n the spatial harmonic orders.

Using $\mathbf{B} = \nabla \times \mathbf{A}$, the components of magnetic flux density $\mathbf{B} = \{B_r; B_\Theta; 0\}$ can be deduced by:

$$B_r = \frac{1}{r} \cdot \frac{\partial A_z}{\partial \Theta} \quad \text{and} \quad B_\Theta = -\frac{\partial A_z}{\partial r} \tag{A3}$$

which leads to:

$$B_r = B_r^\Theta + B_r^r + \frac{1}{r} \cdot \frac{\partial A_{zP}}{\partial \Theta}, \tag{A4a}$$

$$B_r^\Theta = \left[\begin{array}{l} \frac{F_0^\Theta}{r} \cdot [C_0^\Theta + D_0^\Theta \cdot \ln(r)] \\ \dots + \sum_{h=1}^\infty \frac{\beta_h}{r} \cdot \left(\begin{array}{l} C_h^\Theta \cdot r^{\beta_h} \\ \dots + D_h^\Theta \cdot r^{-\beta_h} \end{array} \right) \cdot \left[\begin{array}{l} -E_h^\Theta \cdot \sin(\beta_h \cdot \Theta) \\ \dots + F_h^\Theta \cdot \cos(\beta_h \cdot \Theta) \end{array} \right] \end{array} \right], \tag{A4b}$$

$$B_r^r = \left[\begin{array}{c} \frac{F_0^r}{r} \cdot [C_0^r + D_0^r \cdot \ln(r)] \\ \dots + \sum_{n=1}^{\infty} \frac{\lambda_n}{r} \cdot \left\{ \begin{array}{c} C_n^r \cdot \cos[\lambda_n \cdot \ln(r)] \\ \dots + D_n^r \cdot \sin[\lambda_n \cdot \ln(r)] \end{array} \right\} \cdot \left[\begin{array}{c} E_n^r \cdot sh(\lambda_n \cdot \Theta) \\ \dots + F_n^r \cdot ch(\lambda_n \cdot \Theta) \end{array} \right] \end{array} \right], \tag{A4c}$$

and:

$$B_{\Theta} = B_{\Theta}^{\Theta} + B_{\Theta}^r - \frac{\partial A_z P}{\partial r}, \tag{A5a}$$

$$B_{\Theta}^{\Theta} = - \left[\begin{array}{c} \frac{D_0^{\Theta}}{r} \cdot (E_0^{\Theta} + F_0^{\Theta} \cdot \Theta) \\ \dots + \sum_{h=1}^{\infty} \frac{\beta_h}{r} \cdot \left(\begin{array}{c} C_h^{\Theta} \cdot r^{\beta_h} \\ \dots - D_h^{\Theta} \cdot r^{-\beta_h} \end{array} \right) \cdot \left[\begin{array}{c} E_h^{\Theta} \cdot \cos(\beta_h \cdot \Theta) \\ \dots + F_h^{\Theta} \cdot \sin(\beta_h \cdot \Theta) \end{array} \right] \end{array} \right], \tag{A5b}$$

$$B_{\Theta}^r = - \left[\begin{array}{c} \frac{D_0^r}{r} \cdot (E_0^r + F_0^r \cdot \Theta) \\ \dots + \sum_{n=1}^{\infty} \frac{\lambda_n}{r} \cdot \left\{ \begin{array}{c} -C_n^r \cdot \sin[\lambda_n \cdot \ln(r)] \\ \dots + D_n^r \cdot \cos[\lambda_n \cdot \ln(r)] \end{array} \right\} \cdot \left[\begin{array}{c} E_n^r \cdot ch(\lambda_n \cdot \Theta) \\ \dots + F_n^r \cdot sh(\lambda_n \cdot \Theta) \end{array} \right] \end{array} \right]. \tag{A5c}$$

Appendix B. Simplification of Laplace’s Equations According to Imposed BCs

Appendix B.1. Case-Study No. 1: A_z Imposed on all Edges of a Region

Figure A1a shows a region (for $\Theta \in [\Theta_r, \Theta_l]$ and $r \in [r_l, r_t]$) whose A_z is imposed on all edges. By respecting the BCs and applying the principle of superposition on the magnetic quantities, Figure A1a is redefined by Figure A1b.

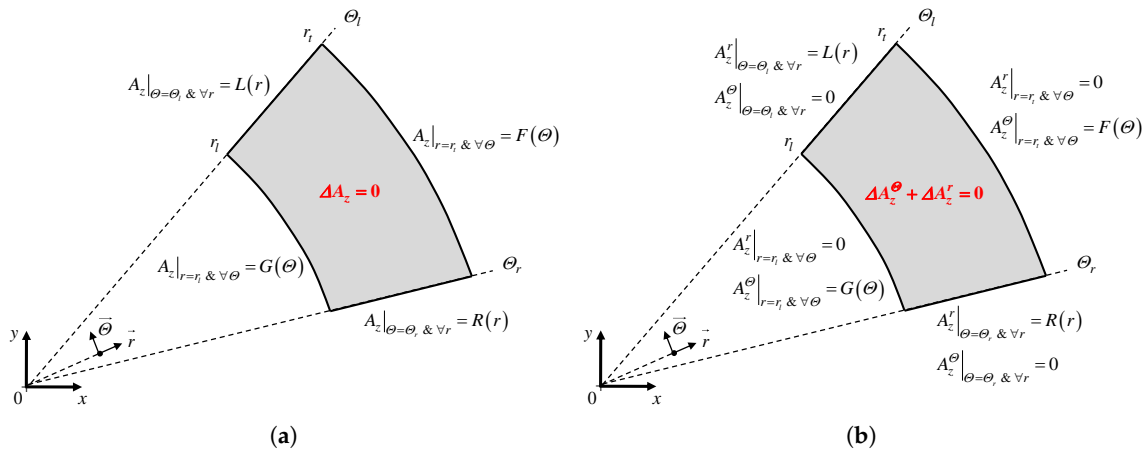


Figure A1. A_z imposed on all edges of a region: (a) general and (b) principle of superposition.

In Case-Study No. 1, $A_z = A_z^{\Theta} + A_z^r$, i.e., Equation (A2), is redefined by:

$$A_z^{\Theta} = \sum_{h=1}^{\infty} \left[c_h^{\Theta} \cdot r_l \cdot \frac{E_{\not{f}}(\beta_h, r_t, r)}{E_{\not{f}}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot r_t \cdot \frac{E_{\not{f}}(\beta_h, r, r_l)}{E_{\not{f}}(\beta_h, r_t, r_l)} \right] \cdot \sin[\beta_h \cdot (\Theta - \Theta_r)], \tag{A6a}$$

$$A_z^r = \sum_{n=1}^{\infty} \left\{ e_n^r \cdot \frac{sh[\lambda_n \cdot (\Theta_l - \Theta)]}{sh(\lambda_n \cdot \tau_{\Theta})} + f_n^r \cdot \frac{sh[\lambda_n \cdot (\Theta - \Theta_r)]}{sh(\lambda_n \cdot \tau_{\Theta})} \right\} \cdot r_l \cdot \sin \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \tag{A6b}$$

the component $B_r = B_r^{\Theta} + B_r^r$ of \mathbf{B} , i.e., Equation (A4), by:

$$B_r^{\Theta} = \sum_{h=1}^{\infty} \beta_h \cdot \left[c_h^{\Theta} \cdot \frac{r_l}{r} \cdot \frac{E_{\not{f}}(\beta_h, r_t, r)}{E_{\not{f}}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot \frac{r_t}{r} \cdot \frac{E_{\not{f}}(\beta_h, r, r_l)}{E_{\not{f}}(\beta_h, r_t, r_l)} \right] \cdot \cos[\beta_h \cdot (\Theta - \Theta_r)], \tag{A7a}$$

$$B_r^r = \sum_{n=1}^{\infty} \lambda_n \cdot \left\{ -e_n^r \cdot \frac{ch[\lambda_n \cdot (\Theta_l - \Theta)]}{sh(\lambda_n \cdot \tau_{\Theta})} + f_n^r \cdot \frac{ch[\lambda_n \cdot (\Theta - \Theta_r)]}{sh(\lambda_n \cdot \tau_{\Theta})} \right\} \cdot \frac{r_l}{r} \cdot \sin \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \quad (A7b)$$

and the component $B_{\Theta} = B_{\Theta}^{\Theta} + B_{\Theta}^r$ of \mathbf{B} , i.e., Equation (A5), by:

$$B_{\Theta}^{\Theta} = - \sum_{h=1}^{\infty} \beta_h \cdot \left[-c_h^{\Theta} \cdot \frac{r_l}{r} \cdot \frac{P_{\not\neq}(\beta_h, r_t, r)}{E_{\not\neq}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot \frac{r_t}{r} \cdot \frac{P_{\not\neq}(\beta_h, r, r_l)}{E_{\not\neq}(\beta_h, r_t, r_l)} \right] \cdot \sin [\beta_h \cdot (\Theta - \Theta_r)], \quad (A8a)$$

$$B_{\Theta}^r = - \sum_{n=1}^{\infty} \lambda_n \cdot \left\{ e_n^r \cdot \frac{sh[\lambda_n \cdot (\Theta_l - \Theta)]}{sh(\lambda_n \cdot \tau_{\Theta})} + f_n^r \cdot \frac{sh[\lambda_n \cdot (\Theta - \Theta_r)]}{sh(\lambda_n \cdot \tau_{\Theta})} \right\} \cdot \frac{r_l}{r} \cdot \cos \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \quad (A8b)$$

where c_h^{Θ} , d_h^{Θ} , e_n^r and f_n^r are new integration constants; $\beta_h = h \cdot \pi / \tau_{\Theta}$ with $\tau_{\Theta} = \Theta_l - \Theta_r$; $\lambda_n = n \cdot \pi / \tau_r$ with $\tau_r = \ln(r_t / r_l)$; and $E_{\not\neq}(w, x, y)$ and $P_{\not\neq}(w, x, y)$ are [44]:

$$E_{\not\neq}(w, x, y) = \left(\frac{x}{y} \right)^w - \left(\frac{y}{x} \right)^w \quad \text{and} \quad P_{\not\neq}(w, x, y) = \left(\frac{x}{y} \right)^w + \left(\frac{y}{x} \right)^w, \quad (A9)$$

with:

$$\frac{\partial E_{\not\neq}(w, x, y)}{\partial x} = \frac{w}{x} \cdot P_{\not\neq}(w, x, y) \quad \text{and} \quad \frac{\partial E_{\not\neq}(w, x, y)}{\partial y} = -\frac{w}{y} \cdot P_{\not\neq}(w, x, y), \quad (A10a)$$

$$\frac{\partial P_{\not\neq}(w, x, y)}{\partial x} = \frac{w}{x} \cdot E_{\not\neq}(w, x, y) \quad \text{and} \quad \frac{\partial P_{\not\neq}(w, x, y)}{\partial y} = -\frac{w}{y} \cdot E_{\not\neq}(w, x, y). \quad (A10b)$$

When $A_z = 0$ on Θ -edges and A_z imposed on r -edges (see Figure A2), A_z with $A_z^r = 0$ in Equation (A6) is expressed by:

$$A_z = \sum_{h=1}^{\infty} \left[c_h^{\Theta} \cdot r_l \cdot \frac{E_{\not\neq}(\beta_h, r_t, r)}{E_{\not\neq}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot r_t \cdot \frac{E_{\not\neq}(\beta_h, r, r_l)}{E_{\not\neq}(\beta_h, r_t, r_l)} \right] \cdot \sin [\beta_h \cdot (\Theta - \Theta_r)], \quad (A11a)$$

the r -component of \mathbf{B} with $B_r^r = 0$ in Equation (A7) by:

$$B_r = \sum_{h=1}^{\infty} \beta_h \cdot \left[c_h^{\Theta} \cdot \frac{r_l}{r} \cdot \frac{E_{\not\neq}(\beta_h, r_t, r)}{E_{\not\neq}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot \frac{r_t}{r} \cdot \frac{E_{\not\neq}(\beta_h, r, r_l)}{E_{\not\neq}(\beta_h, r_t, r_l)} \right] \cdot \cos [\beta_h \cdot (\Theta - \Theta_r)], \quad (A11b)$$

the Θ -component of \mathbf{B} with $B_{\Theta}^r = 0$ in Equation (A8) by:

$$B_{\Theta} = - \sum_{h=1}^{\infty} \beta_h \cdot \left[-c_h^{\Theta} \cdot \frac{r_l}{r} \cdot \frac{P_{\not\neq}(\beta_h, r_t, r)}{E_{\not\neq}(\beta_h, r_t, r_l)} + d_h^{\Theta} \cdot \frac{r_t}{r} \cdot \frac{P_{\not\neq}(\beta_h, r, r_l)}{E_{\not\neq}(\beta_h, r_t, r_l)} \right] \cdot \sin [\beta_h \cdot (\Theta - \Theta_r)]. \quad (A11c)$$

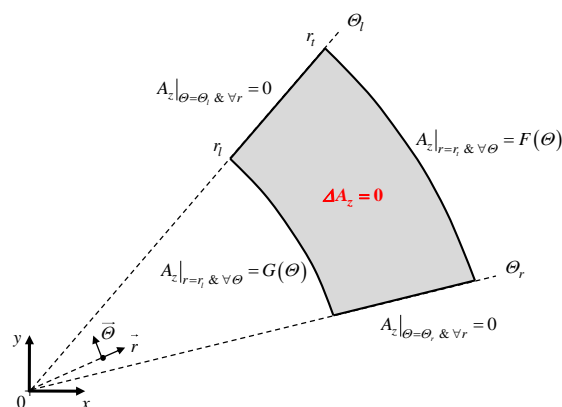


Figure A2. Particular case: $A_z = 0$ on Θ -edges and A_z imposed on r -edges of a region.

Appendix B.2. Case-Study No. 2: B_r and A_z Are Respectively Imposed on r - and Θ -Edges of a Region

Figure A3a shows a region (for $\Theta \in [\Theta_r, \Theta_l]$ and $r \in [r_l, r_t]$) whose B_r and A_z are respectively imposed on r - and Θ -edges. By respecting the BCs and applying the principle of superposition on the magnetic quantities, Figure A3a is redefined by Figure A3b.

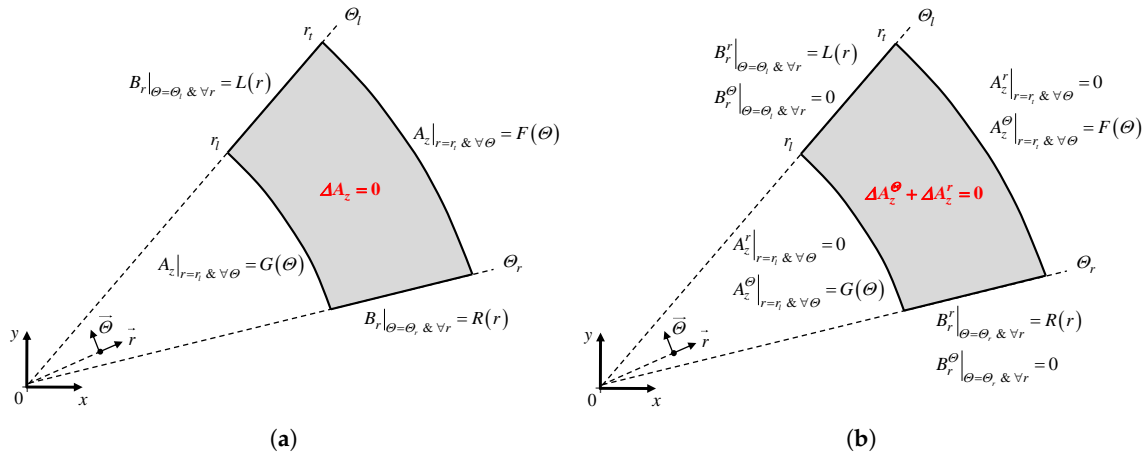


Figure A3. B_r imposed on r -edges and A_z imposed on Θ -edges of a region: (a) general and (b) principle of superposition.

In Case-Study No. 2, $A_z = A_z^\Theta + A_z^r$, i.e., Equation (A2), is redefined by:

$$A_z^\Theta = \left[c_0^\Theta \cdot r_l \cdot \frac{\ln(r_t/r)}{\ln(r_t/r_l)} + d_0^\Theta \cdot r_t \cdot \frac{\ln(r/r_l)}{\ln(r_t/r_l)} \right. \\ \left. \dots + \sum_{h=1}^{\infty} \left[c_h^\Theta \cdot r_l \cdot \frac{E_f(\beta_h, r_t, r)}{E_f(\beta_h, r_t, r_l)} + d_h^\Theta \cdot r_t \cdot \frac{E_f(\beta_h, r, r_l)}{E_f(\beta_h, r_t, r_l)} \right] \cdot \cos [\beta_h \cdot (\Theta - \Theta_r)] \right], \quad (A12a)$$

$$A_z^r = \sum_{n=1}^{\infty} \left\{ e_n^r \cdot \frac{ch [\lambda_n \cdot (\Theta - \Theta_r)]}{sh (\lambda_n \cdot \tau_\Theta)} - f_n^r \cdot \frac{ch [\lambda_n \cdot (\Theta_l - \Theta)]}{sh (\lambda_n \cdot \tau_\Theta)} \right\} \cdot \frac{r_l}{\lambda_n} \cdot \sin \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \quad (A12b)$$

the component $B_r = B_r^\Theta + B_r^r$ of \mathbf{B} , i.e., Equation (A4), by:

$$B_r^\Theta = - \sum_{h=1}^{\infty} \beta_h \cdot \left[c_h^\Theta \cdot \frac{r_l}{r} \cdot \frac{E_f(\beta_h, r_t, r)}{E_f(\beta_h, r_t, r_l)} + d_h^\Theta \cdot \frac{r_t}{r} \cdot \frac{E_f(\beta_h, r, r_l)}{E_f(\beta_h, r_t, r_l)} \right] \cdot \sin [\beta_h \cdot (\Theta - \Theta_r)], \quad (A13a)$$

$$B_r^r = \sum_{n=1}^{\infty} \left\{ e_n^r \cdot \frac{sh [\lambda_n \cdot (\Theta - \Theta_r)]}{sh (\lambda_n \cdot \tau_\Theta)} + f_n^r \cdot \frac{sh [\lambda_n \cdot (\Theta_l - \Theta)]}{sh (\lambda_n \cdot \tau_\Theta)} \right\} \cdot \frac{r_l}{r} \cdot \sin \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \quad (A13b)$$

and the component $B_\Theta = B_\Theta^\Theta + B_\Theta^r$ of \mathbf{B} , i.e., Equation (A5), by:

$$B_\Theta^\Theta = \left[c_0^\Theta \cdot \frac{r_l}{r} \cdot \frac{1}{\ln(r_t/r_l)} - d_0^\Theta \cdot \frac{r_t}{r} \cdot \frac{1}{\ln(r_t/r_l)} \right. \\ \left. \dots + \sum_{h=1}^{\infty} \beta_h \cdot \left[c_h^\Theta \cdot \frac{r_l}{r} \cdot \frac{P_f(\beta_h, r_t, r)}{E_f(\beta_h, r_t, r_l)} - d_h^\Theta \cdot \frac{r_t}{r} \cdot \frac{P_f(\beta_h, r, r_l)}{E_f(\beta_h, r_t, r_l)} \right] \cdot \cos [\beta_h \cdot (\Theta - \Theta_r)] \right], \quad (A14a)$$

$$B_\Theta^r = - \sum_{n=1}^{\infty} \left\{ e_n^r \cdot \frac{ch [\lambda_n \cdot (\Theta - \Theta_r)]}{sh (\lambda_n \cdot \tau_\Theta)} - f_n^r \cdot \frac{ch [\lambda_n \cdot (\Theta_l - \Theta)]}{sh (\lambda_n \cdot \tau_\Theta)} \right\} \cdot \frac{r_l}{r} \cdot \cos \left[\lambda_n \cdot \ln \left(\frac{r}{r_l} \right) \right], \quad (A14b)$$

where $c_0^\Theta, d_0^\Theta, c_h^\Theta, d_h^\Theta, e_n^r$ and f_n^r are new integration constants.

Appendix C. Solving of the Linear System

Appendix C.1. Calculation of General Integrals

For the determination of Fourier’s series coefficients, it is required to calculate general integrals of the form:

$$F_1^\ominus = \int_{l_l}^{l_l+w} \sin [\alpha_s \cdot (l - l_s)] \cdot dl, \tag{A15a}$$

$$F_2^\ominus = \int_{l_l}^{l_l+w} \cos [\alpha_c \cdot (l - l_c)] \cdot \sin [\alpha_s \cdot (l - l_s)] \cdot dl, \tag{A15b}$$

$$F_3^\ominus = \int_{l_l}^{l_l+w} \sin [\alpha_{s1} \cdot (l - l_{s1})] \cdot \sin [\alpha_{s2} \cdot (l - l_{s2})] \cdot dl, \tag{A15c}$$

$$F_4^\ominus = \int_{l_l}^{l_l+w} ch [\alpha_{ch} \cdot (l - l_{ch})] \cdot \sin [\alpha_s \cdot (l - l_s)] \cdot dl, \tag{A15d}$$

$$F_5^\ominus = \int_{l_l}^{l_l+w} sh [\alpha_{sh} \cdot (l - l_{sh})] \cdot \sin [\alpha_s \cdot (l - l_s)] \cdot dl, \tag{A15e}$$

$$F_1^r = \int_{r_l}^{r_t} \frac{1}{r} \cdot \sin \left[\alpha_{s1} \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot \sin \left[\alpha_{s2} \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr, \tag{A15f}$$

$$F_2^r = \int_{r_l}^{r_t} r \cdot \sin \left[\alpha_s \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr, \tag{A15g}$$

$$F_3^r = \int_{r_l}^{r_t} \frac{1}{r} \cdot \frac{\ln (r_t/r)}{\ln (r_t/r_l)} \cdot \sin \left[\alpha_s \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr, \tag{A15h}$$

$$F_4^r = \int_{r_l}^{r_t} \frac{1}{r} \cdot \frac{\ln (r/r_l)}{\ln (r_t/r_l)} \cdot \sin \left[\alpha_s \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr, \tag{A15i}$$

$$F_5^r = \int_{r_l}^{r_t} \frac{1}{r} \cdot \frac{E_\phi(w, r_t, r)}{E_\phi(w, r_t, r_l)} \cdot \sin \left[\alpha_s \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr, \tag{A15j}$$

$$F_6^r = \int_{r_l}^{r_t} \frac{1}{r} \cdot \frac{E_\phi(w, r, r_l)}{E_\phi(w, r_t, r_l)} \cdot \sin \left[\alpha_s \cdot \ln \left(\frac{r}{r_l} \right) \right] \cdot dr. \tag{A15k}$$

The Equations (A15) will be used in the expression of the integration constants. The expressions of Equations (A15a)–(A15e) have been given in [1,44]. The development of Equations (A15f)–(A15k) gives:

$$F_1^r (\alpha_{s1}, \alpha_{s2}, r_l, r_t) = \frac{\ln (r_t/r_l)}{2} \cdot \left\{ \operatorname{sinc} \left[(\alpha_{s1} - \alpha_{s2}) \cdot \ln \left(\frac{r_t}{r_l} \right) \right] - \operatorname{sinc} \left[(\alpha_{s1} + \alpha_{s2}) \cdot \ln \left(\frac{r_t}{r_l} \right) \right] \right\}, \tag{A16a}$$

$$F_2^r (\alpha_s, r_l, r_t) = r_t^2 \cdot \frac{\alpha_s}{\alpha_s^2 + 4} \cdot \left\{ 2 \cdot \ln \left(\frac{r_t}{r_l} \right) \cdot \operatorname{sinc} \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] + \left(\frac{r_l}{r_t} \right)^2 - \cos \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] \right\}, \tag{A16b}$$

$$F_3^r(\alpha_s, r_l, r_t) = \frac{1}{\alpha_s} \cdot \left\{ 1 - \text{sinc} \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] \right\}, \tag{A16c}$$

$$F_4^r(\alpha_s, r_l, r_t) = \frac{1}{\alpha_s} \cdot \left\{ \text{sinc} \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] - \cos \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] \right\}, \tag{A16d}$$

$$F_5^r(\alpha_s, r_l, r_t) = -\frac{\alpha_s}{w^2 + \alpha_s^2} \cdot \left\{ w \cdot \frac{2}{E_{\not{j}}(w, r_t, r_l)} \cdot \ln \left(\frac{r_t}{r_l} \right) \cdot \text{sinc} \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] - 1 \right\}, \tag{A16e}$$

$$F_6^r(\alpha_s, r_l, r_t) = \frac{\alpha_s}{w^2 + \alpha_s^2} \cdot \left\{ w \cdot \ln \left(\frac{r_t}{r_l} \right) \cdot \frac{P_{\not{j}}(w, r_t, r_l)}{E_{\not{j}}(w, r_t, r_l)} \cdot \text{sinc} \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] - \cos \left[\alpha_s \cdot \ln \left(\frac{r_t}{r_l} \right) \right] \right\}. \tag{A16f}$$

Appendix C.2. Determination of Integral Constants

The integration constants are determined by solving:

$$[IC] = [BC]^{-1} \cdot [ES] \quad (\text{i.e., Cramer's system}) \tag{A17}$$

which consists of:

$$X_{\max} = \left[\begin{array}{c} H1_{\max} + H2_{\max} + 2 \cdot H3_{\max} + N3_{\max} + 2 \cdot H4_{\max} + N4_{\max} \\ \dots + 2 \cdot (H5_{\max} + N5_{\max}) + 2 \cdot (H6_{\max} + N6_{\max} + 1) + 2 \cdot (H7_{\max} + N7_{\max} + 1) \end{array} \right] \tag{A18}$$

equations and unknowns [1], where $H1_{\max} - H7_{\max}$ (for the Θ -edges) and $N3_{\max} - N7_{\max}$ (for the r -edges) are the maximal number of spatial harmonics in the various regions for the computation of A_z and $\mathbf{B} = \{B_r; B_{\Theta}; 0\}$. To solve Equation (A17), a numerical matrix inversion is required for the calculation of $[IC]$. This set is implemented in MATLAB® (R2015a, MathWorks, Natick, MA, USA) by using the sparse matrix/vectors [1]. Usually, the two reasons for the possibility of including a finite number of harmonics is a limiting computational time and numerical accuracy [45].

The integration constants vector $[IC]$ (of dimension $X_{\max} \times 1$) is defined by:

$$[IC] = \left[[IC1] \quad [IC2] \quad [IC3] \quad [IC4] \quad [IC5] \quad [IC6] \quad [IC7] \right]^T, \tag{A19a}$$

$$[IC1] = \left[d1_{h1}^{\Theta} \right], \tag{A19b}$$

$$[IC2] = \left[c2_{h2}^{\Theta} \right], \tag{A19c}$$

$$[IC3] = \left[c3_{h3}^{\Theta} \quad d3_{h3}^{\Theta} \quad f3_{n3}^r \right], \tag{A19d}$$

$$[IC4] = \left[c4_{h4}^{\Theta} \quad d4_{h4}^{\Theta} \quad e4_{n4}^r \right], \tag{A19e}$$

$$[IC5] = \left[c5_{h5}^{\Theta} \quad d5_{h5}^{\Theta} \quad e5_{n5}^r \quad f5_{n5}^r \right], \tag{A19f}$$

$$[IC6] = \left[c6_0^{\Theta} \quad c6_{h6}^{\Theta} \quad d6_0^{\Theta} \quad d6_{h6}^{\Theta} \quad e6_{n6}^r \quad f6_{n6}^r \right], \tag{A19g}$$

$$[IC7] = \left[c7_0^{\Theta} \quad c7_{h7}^{\Theta} \quad d7_0^{\Theta} \quad d7_{h7}^{\Theta} \quad e7_{n7}^r \quad f7_{n7}^r \right]. \tag{A19h}$$

The structure of the electromagnetic sources vector $[ES]$ (of dimension $X_{\max} \times 1$), as well as the BCs matrix $[BC]$ (of dimension $X_{\max} \times X_{\max}$) is given in [1] (see Section 2.6). The novel corresponding elements in $[ES]$ and $[BC]$ are defined as follows for Region 1:

$$Q13c_{h1, h3} = -\frac{2 \cdot \beta3_{h3}}{\tau_{\Theta1}} \cdot \frac{\mu_1}{\mu_3} \cdot \frac{P_{\not{j}}(\beta3_{h3}, r_3, r_2)}{E_{\not{j}}(\beta3_{h3}, r_3, r_2)} \cdot F_3^{\Theta}(\beta3_{h3}, \beta1_{h1}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta3}), \tag{A20a}$$

$$Q13d_{h1,h3} = \frac{2 \cdot \beta_{3h3}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_3} \cdot \frac{r_3}{r_2} \cdot \frac{2}{E_{\neq}(\beta_{3h3}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{3h3}, \beta_{1h1}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A20b}$$

$$Q13f_{h1,h3} = \frac{2 \cdot \lambda_{3n3}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_3} \cdot \text{csch}(\lambda_{3n3} \cdot \tau_{\Theta 3}) \cdot F_5^{\Theta}(\lambda_{3n3}, \beta_{1h1}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A20c}$$

$$Q14c_{h1,h4} = -\frac{2 \cdot \beta_{4h4}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_4} \cdot \frac{P_{\neq}(\beta_{4h4}, r_3, r_2)}{E_{\neq}(\beta_{4h4}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{4h4}, \beta_{1h1}, \Theta_5, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A20d}$$

$$Q14d_{h1,h4} = \frac{2 \cdot \beta_{4h4}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_4} \cdot \frac{r_3}{r_2} \cdot \frac{2}{E_{\neq}(\beta_{4h4}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{4h4}, \beta_{1h1}, \Theta_5, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A20e}$$

$$Q14e_{h1,h4} = -\frac{2 \cdot \lambda_{4n4}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_4} \cdot \text{csch}(\lambda_{4n4} \cdot \tau_{\Theta 4}) \cdot F_5^{\Theta}(\lambda_{4n4}, \beta_{1h1}, \Theta_6, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A20f}$$

$$Q15c_{h1,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_5} \cdot \frac{P_{\neq}(\beta_{5h5}, r_3, r_2)}{E_{\neq}(\beta_{5h5}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{5h5}, \beta_{1h1}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A20g}$$

$$Q15d_{h1,h5} = \frac{2 \cdot \beta_{5h5}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_5} \cdot \frac{r_3}{r_2} \cdot \frac{2}{E_{\neq}(\beta_{5h5}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{5h5}, \beta_{1h1}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A20h}$$

$$Q15e_{h1,h5} = -\frac{2 \cdot \lambda_{5n5}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_5} \cdot \text{csch}(\lambda_{5n5} \cdot \tau_{\Theta 5}) \cdot F_5^{\Theta}(\lambda_{5n5}, \beta_{1h1}, \Theta_4, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A20i}$$

$$Q15f_{h1,h5} = \frac{2 \cdot \lambda_{5n5}}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_5} \cdot \text{csch}(\lambda_{5n5} \cdot \tau_{\Theta 5}) \cdot F_5^{\Theta}(\lambda_{5n5}, \beta_{1h1}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A20j}$$

$$Q16c_{h1,h6} = -\frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_6} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 = 0 \\ \beta_{6h6} \cdot \frac{P_{\neq}(\beta_{6h6}, r_3, r_2)}{E_{\neq}(\beta_{6h6}, r_3, r_2)} \cdot F_2^{\Theta}(\beta_{6h6}, \beta_{1h1}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 \neq 0 \end{cases} \tag{A20k}$$

$$Q16d_{h1,h6} = \frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_6} \cdot \frac{r_3}{r_2} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 = 0 \\ \frac{2 \cdot \beta_{6h6}}{E_{\neq}(\beta_{6h6}, r_3, r_2)} \cdot F_2^{\Theta}(\beta_{6h6}, \beta_{1h1}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 \neq 0 \end{cases} \tag{A20l}$$

$$Q16e_{h1,h6} = \frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_6} \cdot \text{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_4^{\Theta}(\lambda_{6n6}, \beta_{1h1}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}), \tag{A20m}$$

$$Q16f_{h1,h6} = -\frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_6} \cdot \text{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_4^{\Theta}(\lambda_{6n6}, \beta_{1h1}, \Theta_3, \Theta_1, \Theta_2, \tau_{\Theta 6}), \tag{A20n}$$

$$Q17c_{h1,h7} = -\frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_7} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 = 0 \\ \beta_{7h7} \cdot \frac{P_{\neq}(\beta_{7h7}, r_3, r_2)}{E_{\neq}(\beta_{7h7}, r_3, r_2)} \cdot F_2^{\Theta}(\beta_{7h7}, \beta_{1h1}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 \neq 0 \end{cases} \tag{A20o}$$

$$Q17d_{h1,h7} = \frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_7} \cdot \frac{r_3}{r_2} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 = 0 \\ \frac{2 \cdot \beta_{7h7}}{E_{\neq}(\beta_{7h7}, r_3, r_2)} \cdot F_2^{\Theta}(\beta_{7h7}, \beta_{1h1}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 \neq 0 \end{cases} \tag{A20p}$$

$$Q17e_{h1,h7} = \frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_7} \cdot \text{csch}(\lambda_{7n7} \cdot \tau_{\Theta 7}) \cdot F_4^{\Theta}(\lambda_{7n7}, \beta_{1h1}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}), \tag{A20q}$$

$$Q17f_{h1,h7} = -\frac{2}{\tau_{\Theta 1}} \cdot \frac{\mu_1}{\mu_7} \cdot \text{csch}(\lambda_{7n7} \cdot \tau_{\Theta 7}) \cdot F_4^{\Theta}(\lambda_{7n7}, \beta_{1h1}, \Theta_5, \Theta_1, \Theta_4, \tau_{\Theta 7}), \tag{A20r}$$

$$ES16_{h1} + ES17_{h1} = \mu_1 \cdot \frac{r_2}{\tau_{\Theta 1}} \cdot \left[J_{z6} \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_2, \tau_{\Theta 6}) + J_{z7} \cdot r_2 \cdot F_1^{\Theta}(\beta_{1h1}, \Theta_1, \Theta_4, \tau_{\Theta 7}) \right], \tag{A20s}$$

for Region 2:

$$Q23c_{h2,h3} = -\frac{2 \cdot \beta_{3h3}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_3} \cdot \frac{r_2}{r_3} \cdot \frac{2}{E_{\neq}(\beta_{3h3}, r_3, r_2)} \cdot F_3^{\Theta}(\beta_{3h3}, \beta_{2h2}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A21a}$$

$$Q23d_{h2,h3} = \frac{2 \cdot \beta_{3h3}}{\tau_{x2}} \cdot \frac{\mu_2}{\mu_3} \cdot \frac{P_{\neq}(\beta_{3h3}, r_3, r_2)}{E_{\neq}(\beta_{3h3}, r_3, r_2)} \cdot F_3^{\ominus}(\beta_{3h3}, \beta_{2h2}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A21b}$$

$$Q23f_{h2,n3} = \frac{2 \cdot \lambda_{3n3}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_3} \cdot \frac{r_2}{r_3} \cdot (-1)^{n3} \cdot \operatorname{csch}(\lambda_{3h3} \cdot \tau_{\Theta 3}) \cdot F_5^{\ominus}(\lambda_{3h3}, \beta_{2h2}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A21c}$$

$$Q24c_{h2,h4} = -\frac{2 \cdot \beta_{4h4}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_4} \cdot \frac{r_2}{r_3} \cdot \frac{2}{E_{\neq}(\beta_{4h4}, r_3, r_2)} \cdot F_3^{\ominus}(\beta_{4h4}, \beta_{2h2}, \Theta_5, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A21d}$$

$$Q24d_{h2,h4} = \frac{2 \cdot \beta_{4h4}}{\tau_{x2}} \cdot \frac{\mu_2}{\mu_4} \cdot \frac{P_{\neq}(\beta_{4h4}, r_3, r_2)}{E_{\neq}(\beta_{4h4}, r_3, r_2)} \cdot F_3^{\ominus}(\beta_{4h4}, \beta_{2h2}, \Theta_5, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A21e}$$

$$Q24e_{h2,n4} = -\frac{2 \cdot \lambda_{4n4}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_4} \cdot \frac{r_2}{r_3} \cdot (-1)^{n4} \cdot \operatorname{csch}(\lambda_{4h4} \cdot \tau_{\Theta 4}) \cdot F_5^{\ominus}(\lambda_{4h4}, \beta_{2h2}, \Theta_6, \Theta_1, \Theta_5, \tau_{\Theta 4}), \tag{A21f}$$

$$Q25c_{h2,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_5} \cdot \frac{r_2}{r_3} \cdot \frac{2}{E_{\neq}(\beta_{5h5}, r_3, r_2)} \cdot F_3^{\ominus}(\beta_{5h5}, \beta_{2h2}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A21g}$$

$$Q25d_{h2,h5} = \frac{2 \cdot \beta_{5h5}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_5} \cdot \frac{P_{\neq}(\beta_{5h5}, r_3, r_2)}{E_{\neq}(\beta_{5h5}, r_3, r_2)} \cdot F_3^{\ominus}(\beta_{5h5}, \beta_{2h2}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A21h}$$

$$Q25e_{h2,n5} = -\frac{2 \cdot \lambda_{5n5}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_5} \cdot \frac{r_2}{r_3} \cdot (-1)^{n5} \cdot \operatorname{csch}(\lambda_{5h5} \cdot \tau_{\Theta 5}) \cdot F_5^{\ominus}(\lambda_{5h5}, \beta_{2h2}, \Theta_4, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A21i}$$

$$Q25f_{h2,n5} = \frac{2 \cdot \lambda_{5n5}}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_5} \cdot \frac{r_2}{r_3} \cdot (-1)^{n5} \cdot \operatorname{csch}(\lambda_{5h5} \cdot \tau_{\Theta 5}) \cdot F_5^{\ominus}(\lambda_{5n5}, \beta_{2h2}, \Theta_3, \Theta_1, \Theta_3, \tau_{\Theta 5}), \tag{A21j}$$

$$Q26c_{h2,h6} = -\frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_6} \cdot \frac{r_2}{r_3} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 = 0 \\ \frac{2 \cdot \beta_{6h6}}{E_{\neq}(\beta_{6h6}, r_3, r_2)} \cdot F_2^{\ominus}(\beta_{6h6}, \beta_{2h2}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 \neq 0 \end{cases} \tag{A21k}$$

$$Q26d_{h2,h6} = \frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_6} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 = 0 \\ \beta_{6h6} \cdot \frac{P_{\neq}(\beta_{6h6}, r_3, r_2)}{E_{\neq}(\beta_{6h6}, r_3, r_2)} \cdot F_2^{\ominus}(\beta_{6h6}, \beta_{2h2}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}) & \text{for } h6 \neq 0 \end{cases} \tag{A21l}$$

$$Q26e_{h2,n6} = \frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_6} \cdot \frac{r_2}{r_3} \cdot (-1)^{n6} \cdot \operatorname{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_4^{\ominus}(\lambda_{6n6}, \beta_{2h2}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta 6}), \tag{A21m}$$

$$Q26f_{h2,n6} = -\frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_6} \cdot \frac{r_2}{r_3} \cdot (-1)^{n6} \cdot \operatorname{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_4^{\ominus}(\lambda_{6n6}, \beta_{2h2}, \Theta_3, \Theta_1, \Theta_2, \tau_{\Theta 6}), \tag{A21n}$$

$$Q27c_{h2,h7} = -\frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_7} \cdot \frac{r_2}{r_3} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 = 0 \\ \frac{2 \cdot \beta_{7h7}}{E_{\neq}(\beta_{7h7}, r_3, r_2)} \cdot F_2^{\ominus}(\beta_{7h7}, \beta_{2h2}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 \neq 0 \end{cases} \tag{A21o}$$

$$Q27d_{h2,h7} = \frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_7} \cdot \begin{cases} \frac{1}{\ln(r_3/r_2)} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_2, \tau_{\Theta 7}) & \text{for } h7 = 0 \\ \beta_{7h7} \cdot \frac{P_{\neq}(\beta_{7h7}, r_3, r_2)}{E_{\neq}(\beta_{7h7}, r_3, r_2)} \cdot F_2^{\ominus}(\beta_{7h7}, \beta_{2h2}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}) & \text{for } h7 \neq 0 \end{cases} \tag{A21p}$$

$$Q27e_{h2,n7} = \frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_7} \cdot \frac{r_2}{r_3} \cdot (-1)^{n7} \cdot \operatorname{csch}(\lambda_{n7} \cdot \tau_{\Theta 7}) \cdot F_4^{\ominus}(\lambda_{n7}, \beta_{2h2}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta 7}), \tag{A21q}$$

$$Q27f_{h2,n7} = -\frac{2}{\tau_{\Theta 2}} \cdot \frac{\mu_2}{\mu_7} \cdot \frac{r_2}{r_3} \cdot (-1)^{n7} \cdot \operatorname{csch}(\lambda_{n7} \cdot \tau_{\Theta 7}) \cdot F_4^{\ominus}(\lambda_{n7}, \beta_{2h2}, \Theta_5, \Theta_1, \Theta_4, \tau_{\Theta 7}), \tag{A21r}$$

$$ES26_{h2} + ES27_{h2} = \mu_2 \cdot \frac{r_3}{\tau_{\Theta 2}} \cdot [J_{z6} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_2, \tau_{\Theta 6}) + J_{z7} \cdot F_1^{\ominus}(\beta_{2h2}, \Theta_1, \Theta_4, \tau_{\Theta 7})], \tag{A21s}$$

for Region 3:

$$Q31d_{h3,h1} = \frac{2}{\tau_{\Theta 3}} \cdot \frac{1}{\beta_{1h1}} \cdot \frac{E_{\neq}(\beta_{1h1}, r_2, r_1)}{P_{\neq}(\beta_{1h1}, r_2, r_1)} \cdot F_3^{\ominus}(\beta_{1h1}, \beta_{3h3}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A22a}$$

$$Q32c_{h3,h2} = -\frac{2}{\tau_{\Theta 3}} \cdot \frac{1}{\beta_{2h2}} \cdot \frac{E_{\varphi}(\beta_{2h2}, r_4, r_3)}{P_{\varphi}(\beta_{2h2}, r_4, r_3)} \cdot F_3^{\Theta}(\beta_{2h2}, \beta_{3h3}, \Theta_1, \Theta_1, \Theta_1, \tau_{\Theta 3}), \tag{A22b}$$

$$Q36c_{n3,h6} = -\frac{2}{\tau_{r3}} \cdot \begin{cases} F_3^r(\lambda_{3n3}, r_2, r_3) & \text{for } h6 = 0 \\ F_5^r(\beta_{6h6}, \lambda_{3n3}, r_2, r_3) & \text{for } h6 \neq 0 \end{cases} \tag{A22c}$$

$$Q36d_{n3,h6} = -\frac{2}{\tau_{r3}} \cdot \frac{r_3}{r_2} \cdot \begin{cases} F_4^r(\lambda_{3n3}, r_2, r_3) & \text{for } h6 = 0 \\ F_6^r(\beta_{6h6}, \lambda_{3n3}, r_2, r_3) & \text{for } h6 \neq 0 \end{cases} \tag{A22d}$$

$$Q36e_{n3,n6} = -\frac{2}{\tau_{r3}} \cdot \frac{1}{\lambda_{6n6}} \cdot \operatorname{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_1^r(\lambda_{6n6}, \lambda_{3n3}, r_2, r_3), \tag{A22e}$$

$$Q36f_{n3,n6} = \frac{2}{\tau_{r3}} \cdot \frac{1}{\lambda_{6n6}} \cdot \operatorname{coth}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_1^r(\lambda_{6n6}, \lambda_{3n3}, r_2, r_3), \tag{A22f}$$

$$ES36_{n3} = -\mu_6 \cdot \frac{1}{2 \cdot \tau_{r3}} \cdot \frac{1}{r_2} \cdot J_{z6} \cdot F_2^r(\lambda_{3n3}, r_2, r_3), \tag{A22g}$$

for Region 4:

$$Q41d_{h4,h1} = \frac{2}{\tau_{\Theta 4}} \cdot \frac{1}{\beta_{1h1}} \cdot \frac{E_{\varphi}(\beta_{1h1}, r_2, r_1)}{P_{\varphi}(\beta_{1h1}, r_2, r_1)} \cdot F_3^{\Theta}(\beta_{1h1}, \beta_{4h4}, \Theta_1, \Theta_5, \Theta_5, \tau_{\Theta 4}), \tag{A23a}$$

$$Q42c_{h4,h2} = -\frac{2}{\tau_{\Theta 4}} \cdot \frac{1}{\beta_{2h2}} \cdot \frac{E_{\varphi}(\beta_{2h2}, r_4, r_3)}{P_{\varphi}(\beta_{2h2}, r_4, r_3)} \cdot F_3^{\Theta}(\beta_{2h2}, \beta_{4h4}, \Theta_1, \Theta_5, \Theta_5, \tau_{\Theta 4}), \tag{A23b}$$

$$Q47c_{n4,h7} = -\frac{2}{\tau_{r4}} \cdot \begin{cases} F_3^r(\lambda_{4n4}, r_2, r_3) & \text{for } h7 = 0 \\ (-1)^{h7} \cdot F_5^r(\beta_{7h7}, \lambda_{4n4}, r_2, r_3) & \text{for } h7 \neq 0 \end{cases} \tag{A23c}$$

$$Q47d_{n4,h7} = -\frac{2}{\tau_{r4}} \cdot \frac{r_3}{r_2} \cdot \begin{cases} F_4^r(\lambda_{4n4}, r_2, r_3) & \text{for } h7 = 0 \\ (-1)^{h7} \cdot F_6^r(\beta_{7h7}, \lambda_{4n4}, r_2, r_3) & \text{for } h7 \neq 0 \end{cases} \tag{A23d}$$

$$Q47e_{n4,n7} = -\frac{2}{\tau_{r4}} \cdot \frac{1}{\lambda_{7n7}} \cdot \operatorname{coth}(\lambda_{7n7} \cdot \tau_{\Theta 7}) \cdot F_1^r(\lambda_{7n7}, \lambda_{4n4}, r_2, r_3), \tag{A23e}$$

$$Q47f_{n4,n7} = \frac{2}{\tau_{r4}} \cdot \frac{1}{\lambda_{7n7}} \cdot \operatorname{csch}(\lambda_{7n7} \cdot \tau_{\Theta 7}) \cdot F_1^r(\lambda_{7n7}, \lambda_{4n4}, r_2, r_3), \tag{A23f}$$

$$ES47_{n4} = -\mu_7 \cdot \frac{1}{2 \cdot \tau_{r4}} \cdot \frac{1}{r_2} \cdot J_{z7} \cdot F_2^r(\lambda_{4n4}, r_2, r_3), \tag{A23g}$$

for Region 5:

$$Q51d_{h5,h1} = \frac{2}{\tau_{\Theta 5}} \cdot \frac{1}{\beta_{1h1}} \cdot \frac{E_{\varphi}(\beta_{1h1}, r_2, r_1)}{P_{\varphi}(\beta_{1h1}, r_2, r_1)} \cdot F_3^{\Theta}(\beta_{1h1}, \beta_{5h5}, \Theta_1, \Theta_3, \Theta_3, \tau_{\Theta 5}). \tag{A24a}$$

$$Q52c_{h5,h2} = -\frac{2}{\tau_{\Theta 5}} \cdot \frac{1}{\beta_{2h2}} \cdot \frac{E_{\varphi}(\beta_{2h2}, r_4, r_3)}{P_{\varphi}(\beta_{2h2}, r_4, r_3)} \cdot F_3^{\Theta}(\beta_{2h2}, \beta_{5h5}, \Theta_1, \Theta_3, \Theta_3, \tau_{\Theta 5}). \tag{A24b}$$

$$Q56c_{n5,h6} = -\frac{2}{\tau_{r5}} \cdot \begin{cases} F_3^r(\lambda_{5n5}, r_2, r_3) & \text{for } h6 = 0 \\ (-1)^{h6} \cdot F_5^r(\beta_{6h6}, \lambda_{5n5}, r_2, r_3) & \text{for } h6 \neq 0 \end{cases} \tag{A24c}$$

$$Q56d_{n5,h6} = -\frac{2}{\tau_{r5}} \cdot \frac{r_3}{r_2} \cdot \begin{cases} F_4^r(\lambda_{5n5}, r_2, r_3) & \text{for } h6 = 0 \\ (-1)^{h6} \cdot F_6^r(\beta_{6h6}, \lambda_{5n5}, r_2, r_3) & \text{for } h6 \neq 0 \end{cases} \tag{A24d}$$

$$Q56e_{n5,n6} = -\frac{2}{\tau_{r5}} \cdot \frac{1}{\lambda_{6n6}} \cdot \operatorname{coth}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_1^r(\lambda_{6n6}, \lambda_{5n5}, r_2, r_3), \tag{A24e}$$

$$Q56f_{n5,n6} = \frac{2}{\tau_{r5}} \cdot \frac{1}{\lambda_{6n6}} \cdot \operatorname{csch}(\lambda_{6n6} \cdot \tau_{\Theta 6}) \cdot F_1^r(\lambda_{6n6}, \lambda_{5n5}, r_2, r_3), \tag{A24f}$$

$$Q57c_{n5,h7} = -\frac{2}{\tau_{r5}} \cdot \begin{cases} F_3^r(\lambda_{5n5}, r_2, r_3) & \text{for } h7 = 0 \\ F_5^r(\beta_{7h7}, \lambda_{5n5}, r_2, r_3) & \text{for } h7 \neq 0 \end{cases} \quad (A24g)$$

$$Q57d_{n5,h7} = -\frac{2}{\tau_{r5}} \cdot \frac{r_3}{r_2} \cdot \begin{cases} F_4^r(\lambda_{5n5}, r_2, r_3) & \text{for } h7 = 0 \\ F_6^r(\beta_{7h7}, \lambda_{5n5}, r_2, r_3) & \text{for } h7 \neq 0 \end{cases} \quad (A24h)$$

$$Q57e_{n5,n7} = -\frac{2}{\tau_{r5}} \cdot \frac{1}{\lambda_{7n7}} \cdot \operatorname{csch}(\lambda_{7n7} \cdot \tau_{\Theta7}) \cdot F_1^r(\lambda_{7n7}, \lambda_{5n5}, r_2, r_3), \quad (A24i)$$

$$Q57f_{n5,n7} = \frac{2}{\tau_{r5}} \cdot \frac{1}{\lambda_{7n7}} \cdot \operatorname{coth}(\lambda_{7n7} \cdot \tau_{\Theta7}) \cdot F_1^r(\lambda_{7n7}, \lambda_{5n5}, r_2, r_3), \quad (A24j)$$

$$ES56_{n5} = -\mu_6 \cdot \frac{1}{2 \cdot \tau_{r5}} \cdot \frac{1}{r_2} \cdot J_{z6} \cdot F_2^r(\lambda_{5n5}, r_2, r_3). \quad (A24k)$$

$$ES57_{n5} = -\mu_7 \cdot \frac{1}{2 \cdot \tau_{r5}} \cdot \frac{1}{r_2} \cdot J_{z7} \cdot F_2^r(\lambda_{5n5}, r_2, r_3). \quad (A24l)$$

for Region 6:

$$Q61d_{h6,h1} = \frac{1}{\tau_{\Theta6}} \cdot \frac{1}{\beta_{1h1}} \cdot \frac{E_f(\beta_{1h1}, r_2, r_1)}{P_f(\beta_{1h1}, r_2, r_1)} \cdot \begin{cases} F_1^\Theta(\beta_{1h1}, \Theta_1, \Theta_2, \tau_{\Theta6}) & \text{for } h6 = 0 \\ 2 \cdot F_2^\Theta(\beta_{6h6}, \beta_{1h1}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta6}) & \text{for } h6 \neq 0 \end{cases} \quad (A25a)$$

$$Q62c_{h6,h1} = -\frac{1}{\tau_{\Theta6}} \cdot \frac{1}{\beta_{2h2}} \cdot \frac{E_f(\beta_{2h2}, r_4, r_3)}{P_f(\beta_{2h2}, r_4, r_3)} \cdot \begin{cases} F_1^\Theta(\beta_{2h2}, \Theta_1, \Theta_2, \tau_{\Theta6}) & \text{for } h6 = 0 \\ 2 \cdot F_2^\Theta(\beta_{6h6}, \beta_{2h2}, \Theta_2, \Theta_1, \Theta_2, \tau_{\Theta6}) & \text{for } h6 \neq 0 \end{cases} \quad (A25b)$$

$$Q63c_{n6,h3} = -\frac{2 \cdot \beta_{3h3}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_3} \cdot (-1)^{h3} \cdot F_5^r(\beta_{3h3}, \lambda_{6n6}, r_2, r_3), \quad (A25c)$$

$$Q63d_{n6,h3} = -\frac{2 \cdot \beta_{3h3}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_3} \cdot \frac{r_3}{r_2} \cdot (-1)^{h3} \cdot F_6^r(\beta_{3h3}, \lambda_{6n6}, r_2, r_3), \quad (A25d)$$

$$Q63f_{n6,n3} = -\frac{2 \cdot \lambda_{3n3}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_3} \cdot \operatorname{coth}(\lambda_{3n3} \cdot \tau_{\Theta3}) \cdot F_1^r(\lambda_{3n3}, \lambda_{6n6}, r_2, r_3), \quad (A25e)$$

$$Q65c_{n6,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_5} \cdot F_5^\Theta(\beta_{5h5}, \lambda_{6n6}, r_2, r_3), \quad (A25f)$$

$$Q65d_{n6,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_5} \cdot \frac{r_3}{r_2} \cdot F_6^\Theta(\beta_{5h5}, \lambda_{6n6}, r_2, r_3), \quad (A25g)$$

$$Q65e_{n6,n5} = \frac{2 \cdot \lambda_{5n5}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_5} \cdot \operatorname{coth}(\lambda_{5n5} \cdot \tau_{\Theta5}) \cdot F_1^r(\lambda_{5n5}, \lambda_{6n6}, r_2, r_3), \quad (A25h)$$

$$Q65f_{n6,n5} = -\frac{2 \cdot \lambda_{5n5}}{\tau_{r6}} \cdot \frac{\mu_6}{\mu_5} \cdot \operatorname{csch}(\lambda_{5n5} \cdot \tau_{\Theta5}) \cdot F_1^r(\lambda_{5n5}, \lambda_{6n6}, r_2, r_3), \quad (A25i)$$

$$ES61_0 = \frac{1}{4} \cdot \mu_6 \cdot J_{z6} \cdot r_2, \quad (A25j)$$

$$ES62_0 = \frac{1}{4} \cdot \mu_6 \cdot J_{z6} \cdot r_3, \quad (A25k)$$

for Region 7:

$$Q71d_{h7,h1} = \frac{1}{\tau_{\Theta7}} \cdot \frac{1}{\beta_{1h1}} \cdot \frac{E_f(\beta_{1h1}, r_2, r_1)}{P_f(\beta_{1h1}, r_2, r_1)} \cdot \begin{cases} F_1^\Theta(\beta_{1h1}, \Theta_1, \Theta_4, \tau_{\Theta7}) & \text{for } h7 = 0 \\ 2 \cdot F_2^\Theta(\beta_{7h7}, \beta_{1h1}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta7}) & \text{for } h7 \neq 0 \end{cases} \quad (A26a)$$

$$Q72c_{h7,h2} = -\frac{1}{\tau_{\Theta7}} \cdot \frac{1}{\beta_{2h2}} \cdot \frac{E_f(\beta_{2h2}, r_4, r_3)}{P_f(\beta_{2h2}, r_4, r_3)} \cdot \begin{cases} F_1^\Theta(\beta_{2h2}, \Theta_1, \Theta_4, \tau_{\Theta7}) & \text{for } h7 = 0 \\ 2 \cdot F_2^\Theta(\beta_{7h7}, \beta_{2h2}, \Theta_4, \Theta_1, \Theta_4, \tau_{\Theta7}) & \text{for } h7 \neq 0 \end{cases} \quad (A26b)$$

$$Q74c_{n7,h4} = -\frac{2 \cdot \beta_{4h4}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_4} \cdot F_5^r(\beta_{4h4}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26c})$$

$$Q74d_{n7,h4} = -\frac{2 \cdot \beta_{4h4}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_4} \cdot \frac{r_3}{r_2} \cdot F_6^r(\beta_{4h4}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26d})$$

$$Q74e_{n7,h4} = \frac{2 \cdot \lambda_{4n4}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_4} \cdot \coth(\lambda_{4n4} \cdot \tau_{\Theta 4}) \cdot F_1^r(\lambda_{4n4}, \lambda_{7n7}, r_2, r_3). \quad (\text{A26e})$$

$$Q75c_{n7,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_5} \cdot (-1)^{h5} \cdot F_5^r(\beta_{5h5}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26f})$$

$$Q75d_{n7,h5} = -\frac{2 \cdot \beta_{5h5}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_5} \cdot \frac{r_3}{r_2} \cdot (-1)^{h5} \cdot F_6^r(\beta_{5h5}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26g})$$

$$Q75e_{n7,h5} = \frac{2 \cdot \lambda_{5n5}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_5} \cdot \operatorname{csch}(\lambda_{5n5} \cdot \tau_{\Theta 5}) \cdot F_1^\ominus(\lambda_{5n5}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26h})$$

$$Q75f_{n7,h5} = -\frac{2 \cdot \lambda_{5n5}}{\tau_{r7}} \cdot \frac{\mu_7}{\mu_5} \cdot \coth(\lambda_{5n5} \cdot \tau_{\Theta 5}) \cdot F_1^\ominus(\lambda_{5n5}, \lambda_{7n7}, r_2, r_3), \quad (\text{A26i})$$

$$ES71_0 = \frac{1}{4} \cdot \mu_7 \cdot J_{z7} \cdot r_2, \quad (\text{A26j})$$

$$ES72_0 = \frac{1}{4} \cdot \mu_7 \cdot J_{z7} \cdot r_3. \quad (\text{A26k})$$

References

- Dubas, F.; Boughrara, K. New scientific contribution on the 2-D subdomain technique in Cartesian coordinates: Taking into account of iron parts. *Math. Comput. Appl.* **2017**, *22*, doi: 10.3390/mca22010017.
- Lehmann, T. Méthode graphique pour déterminer le trajet des lignes de force dans l'air. *Revue d'Électricité: La Lumière Électrique* **1909**, 43–45, 103–110, 137–142, 163–168.
- Jin, J. *The Finite Element Method in Electromagnetic*, 2nd ed.; John Wiley and Sons, Inc.: New York, NY, USA, 2002.
- Smith, G.D. *Numerical Solution of Partial Differential Equations: Finite Difference Methods*, 3rd ed.; Clarendon Press: Oxford, UK, 1985.
- Wrobel, L.C.; Aliabadi, M.H. *The Boundary Element Method*; John Wiley and Sons, Inc.: New York, NY, USA, 2002.
- Kron, G. *Equivalent Circuits of Electric Machinery*; John Wiley and Sons, Inc.: New York, NY, USA; Chapman and Hall, Ltd.: London, UK, 1951.
- Holman, J.P. *Heat Transfer*, 6th ed.; McGraw-Hill Book Compagny: New York, NY, USA, 1986.
- Roters, H.C. *Electromagnetic Devices*; John Wiley and Sons, Inc.: New York, NY, USA, 1941.
- Driscoll, T.A.; Trefethen, L.N. *Schwarz-Christoffel Mapping*; Cambridge University Press: Cambridge, UK, 2002.
- Hague, B. *Electromagnetic Problems in Electrical Engineering*; Oxford University Press: London, UK, 1929.
- Sylvester, P. *Modern Electromagnetic Fields*; Prentice-Hall: London, UK, 1968.
- Stoll, R.L. *The Analysis of Eddy Currents*; Clarendon Press: Oxford, UK, 1974.
- Binns, K.J.; Lawrenson, P.J.; Trowbridge, C.W. *The Analytical and Numerical Solution of Electric and Magnetic Fields*; John Wiley and Sons, Inc.: New York, NY, USA, 1992.
- Melcher, J.R. *Continuum Electromechanics*; MIT Press: Cambridge, MA, USA, 1981.
- Farlow, S.J. *Partial Differential Equations for Scientists and Engineers*; Dover, Inc.: New York, NY, USA, 1993.
- Dubas, F.; Espanet, C. Analytical solution of the magnetic field in permanent-magnet motors taking into account slotting effect: No-load vector potential and flux density calculation. *IEEE Trans. Magn.* **2009**, *45*, 2097–2109.
- Tiegna, H.; Amara, Y.; Barakat, G. Overview of analytical models of permanent magnet electrical machines for analysis and design purposes. *Math. Comput. Simul.* **2013**, *90*, 162–177.

18. Devillers, E.; Le Besnerais, J.; Lubin, T.; Hecquet, M.; Lecointe, J.P. A review of subdomain modeling techniques in electrical machines: Performances and applications. In Proceedings of the XXII International Conference on Electrical Machines (ICEM), Lausanne, Switzerland, 4–7 September 2016.
19. Kumar, P.; Bauer, P. Improved analytical model of a permanent-magnet brushless DC motor. *IEEE Trans. Magn.* **2008**, *44*, 2299–2309.
20. Dalal, A.; Kumar, P. Analytical model for permanent magnet motor with slotting effect, armature reaction, and ferromagnetic material property. *IEEE Trans. Magn.* **2015**, *51*, doi:10.1109/TMAG.2015.2459036.
21. Boules, N. Two-dimensional field analysis of cylindrical machines with permanent magnet excitation. *IEEE Trans. Ind. Appl.* **1984**, *IA-20*, 1267–1277.
22. Berkani, M.S.; Sough, M.L.; Giurgea, S.; Dubas, F.; Boualem, B.; Espanet, C. A simple analytical approach to model saturation in surface mounted permanent magnet synchronous motors. In Proceedings of the 2015 IEEE Energy Conversion Congress and Exposition (ECCE), Montreal, QC, Canada, 20–24 September 2015.
23. Mishkin, E. Theory of the squirrel-cage induction machine derived directly from Maxwell's field equations. *Q. J. Mech. Appl. Math.* **1954**, *7*, 472–487.
24. Panaitescu, A.; Panaitescu, I. A field model for induction machines. In Proceedings of the International Conference on Electrical Machines (ICEM), Vigo, Spain, 10–12 September 1996.
25. Madescu, G.; Boldea, I.; Miller, T.J.E. An analytical iterative model (AIM) for induction motor design. In Proceedings of the Conference Record of the 1996 IEEE Industry Applications Conference Thirty-First IAS Annual Meeting, San Diego, CA, USA, 6–10 October 1996.
26. Sprangers, R.L.J.; Motoasca, T.E.; Lomonova, E.A. Extended anisotropic layer theory for electrical machines. *IEEE Trans. Magn.* **2013**, *49*, 2217–2220.
27. Sprangers, R.L.J.; Paulides, J.J.H.; Gysen, B.L.J.; Lomonova, E.A. Magnetic saturation in semi-analytical harmonic modeling for electric machine analysis. *IEEE Trans. Magn.* **2016**, *52*, doi:10.1109/TMAG.2015.2480708.
28. Sprangers, R.L.J.; Paulides, J.J.H.; Gysen, B.L.J.; Waarma, J.; Lomonova, E.A. Semi-analytical framework for synchronous reluctance motor analysis including finite soft-magnetic material permeability. *IEEE Trans. Magn.* **2015**, *51*, doi:10.1109/TMAG.2015.2442419.
29. Djelloul, K.Z.; Boughrara, K.; Ibtouen, R.; Dubas, F. Nonlinear analytical calculation of magnetic field and torque of switched reluctance machines. In Proceedings of the CISTEM, Marrakech-Benguérir, Maroc, 26–28 October 2016.
30. Djelloul, K.Z.; Boughrara, K.; Dubas, F.; Ibtouen, R. Nonlinear analytical prediction of magnetic field and electromagnetic performances in switched reluctance machines. *IEEE Trans. Magn.* **2017**, *53*, doi:10.1109/TMAG.2017.2679686.
31. Theodoulidis, T.P. Model of ferrite-cored probes for eddy current nondestructive evaluation. *J. Appl. Phys.* **2003**, *93*, 3071–3078.
32. Theodoulidis, T.P.; Bowler, J. Eddy-current interaction of a long coil with a slot in a conductive plate. *IEEE Trans. Magn.* **2005**, *41*, 1238–1247.
33. Roubache, L.; Boughrara, K.; Dubas, F.; Ibtouen, R. Semi-Analytical modeling of spoke-type permanent-magnet machines considering the iron core relative permeability: Subdomain technique and Taylor polynomial. *Prog. Electromagn. Res. B* **2017**, *77*, 85–101.
34. Roubache, L.; Boughrara, K.; Dubas, F.; Ibtouen, R. Semi-analytical modeling of spoke-type permanent-magnet machines considering nonlinear magnetic saturation: Subdomain Technique and Taylor polynomial. *Math. Comput. Simul.* **2017**, Under review.
35. Abdel-Razek, A.A.; Coulomb, J.L.; Feliachi, M.; Sabonnadière, J.C. The calculation of electromagnetic torque in saturated electric machines within combined numerical and analytical solutions of the field equations. *IEEE Trans. Magn.* **1981**, *17*, 3250–3252.
36. Liu, Z.J.; Bi, C.; Tan, H.C.; Low, T.S. A combined numerical and analytical approach for magnetic field analysis of permanent magnet machines. *IEEE Trans. Magn.* **1995**, *31*, 1372–1375.
37. Mirzayee, M.; Mehrjerdi, H.; Tsurkerman, I. Analysis of a high-speed solid rotor induction motor using coupled analytical method and reluctance networks. In Proceedings of the 2005 IEEE/ACES International Conference on Wireless Communications and Applied Computational Electromagnetics (ACES), Honolulu, HI, USA, 3–7 April 2005.
38. Hemeida, A.; Sergeant, P. Analytical modeling of surface PMSM using a combined solution of Maxwell's equations and magnetic equivalent circuit. *IEEE Trans. Magn.* **2014**, *50*, doi:10.1109/TMAG.2014.2330801.

39. Pluk, K.J.W.; Jansen, J.W.; Lomonova, E.A. 3-D hybrid analytical modeling: 3-D Fourier modeling combined with mesh-based 3-D magnetic equivalent circuits. *IEEE Trans. Magn.* **2015**, *51*, doi:10.1109/TMAG.2015.2455951.
40. Flux2D. *General Operating Instructions*, Version 10.2.1; Cedrat S.A. Electrical Engineering: Grenoble, France, 2008.
41. Lee, S.W.; Jones, W.; Campbell, J. Convergence of numerical solution of iris-type discontinuity problems. *IEEE Trans. Microw. Theory Tech.* **1971**, *19*, 528–536.
42. Mittra, R.; Itoh, T.; Li, T.-S. Analytical and numerical studies of the relative convergence phenomenon arising in the solution of an integral equation by the moment method. *IEEE Trans. Microw. Theory Tech.* **1972**, *20*, 96–104.
43. Rahideh, A.; Korakianitis, T. Analytical calculation of open-circuit magnetic field distribution of slotless brushless PM machines. *Electr. Power Energy Syst.* **2012**, *44*, 99–114.
44. Dubas, F.; Rahideh, A. Two-dimensional analytical PM eddy-current loss calculations in slotless PMSM equipped with surface-inset magnets. *IEEE Trans. Magn.* **2014**, *50*, doi:10.1109/TMAG.2013.2285525.
45. Gysen, B.L.J.; Meessen, K.J.; Paulides, J.J.H.; Lomonova, E.A. General formulation of the electromagnetic field distribution in machines and devices using Fourier analysis. *IEEE Trans. Magn.* **2010**, *46*, 39–52.



© 2017 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).