



Communication Theoretical Comparison of Optothermal Absorption in Transmissive Metalenses Composed of Nanobricks and Nanoholes

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Abstract: Background: Optical components with high damage thresholds are very desirable in intense-light systems. Metalenses, being composed of phase-control nanostructures with peculiar properties, are one of the important component candidates in future optical systems. However, the optothermal mechanism in metalenses is still not investigated adequately. Methods: In this study, the optothermal absorption in transmissive metalenses made of silicon nanobricks and nanoholes is investigated comparatively to address this issue. Results: The geometrical dependencies of nanostructures' transmittance, phase difference, and field distribution are calculated numerically via simulations. To demonstrate the optothermal mechanism in metalenses, the mean absorption efficiencies of the selected unit-cells, which would constitute metalenses, are analyzed. The results show that the electric field in the silicon zone would lead to an obvious thermal effect, and the enhancement of the localized electric field also results in the strong absorption of optical energy. Then, two typical metalenses are designed based on these nanobricks and nanoholes. The optothermal simulations show that the nanobrick-based metalens can handle a power density of $0.15 \text{ W}/\mu\text{m}^2$, and the density of the nanohole-based design is $0.12 \text{ W}/\mu m^2$. Conclusions: The study analyzes and compares the optothermal absorption in nanobricks and nanoholes, which shows that the electricfield distribution in absorbent materials and the localized-field enhancement are the two key effects that lead to optothermal absorption. This study provides an approach to improve the anti-damage potentials of transmissive metalenses for intense-light systems.

Keywords: optothermal absorption; metasurfaces; complementary nanostructures; intense-light systems

1. Introduction

Intense-light systems increasingly impact laser fabrication [1], directed energy [2], renewable energy [3,4], etc. Transmissive phase components with high damage thresholds serve the crucial roles of beam shaping, steering, and focusing in these systems. Traditional refractive components mainly rely on geometrical shapes to bend rays, leading to the high complexity of intense-light systems. Flat optical components with anti-damage properties are the core to solving this problem. Particularly, metalenses, being composed of phase-control nanostructures with peculiar properties such as ultra-compact [5,6], large field of view [7,8], perfect absorption [9–11], etc., are one of the most important candidates for the future [12–14]. Many metasurfaces have been investigated to realize phase-control functions, such as imaging [15,16], steering [17–19], and holographic imaging [20,21]. However, the optothermal mechanism in metalenses is still not investigated adequately.

Due to the electromagnetic resonant effect, the electric field is usually localized in nanostructures [12], which would lead to optothermal absorption. This phenomenon is employed to induce deformation in laser fabrication of nanostructures [22]. The experiments



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). show that the heat power volume density in nanostructures stems from the imaginary part of permittivity and the in situ electric field [23]. This optothermal effect is also experimentally demonstrated in other plasmonic [24] and dielectric [25,26] nanostructures. Thus, to improve damage thresholds, an intuitional method is to tune the electric field out of absorbent constituent materials, avoiding direct optothermal absorption. This method has been experimentally verified in anti-reflection nanotextures on fused silica, in which the strong electric field is tuned from nanostructures into the air and anti-damage properties are obtained successfully [27,28]. According to the method, our previous works also demonstrated that reflective metasurfaces made of dielectric nanoholes could be realized with high damage thresholds via field manipulation, and the electromagnetic mechanism has been explained via the electromagnetic distribution of excitation states [29,30]. To further demonstrate the principles of anti-damage metasurfaces, the optothermal mechanism in transmissive phase-control metalenses still requires investigation.

In this study, the optothermal absorption in transmissive phase-control metalenses made of silicon nanobricks and nanoholes are investigated comparatively. The optothermal absorption of the nanobricks and nanoholes with the $0-2\pi$ phase coverage is analyzed numerically. The results show that the electric field in the silicon zone would lead to an obvious thermal effect, and the enhancement of the localized electric field also results in strong absorption of optical energy. Then, two typical metalenses are constructed based on these nanostructures. The optothermal simulations show that the nanobrick-based metalens can handle a stronger laser of $0.15 \text{ W/}\mu\text{m}^2$ than that ($0.12 \text{ W/}\mu\text{m}^2$) of nanoholes. The study demonstrates that the electric-field distribution in absorbent materials and the localized-field enhancement are the two key effects that lead to optothermal absorption, which improves the principles of designing anti-damage metalenses.

2. Materials and Methods

The studied transmissive metalenses are composed of periodic silicon (Si) nanobricks or nanoholes on SiO₂ substrates with the same height H = 200 nm and the same lattice period P = 600 nm, as shown in Figure 1. Each unit-cell has a nanostructure with a rectangular shape described by length L_b or L_h , and width W_b or W_h . p-Si is chosen in the study due to its higher melting point and thermal stability than amorphous Si. The coating material is air, and the absorptivity could be ignorable. The incident light is continuous and polarized along the *x*-axis direction and injected from the bottom of the unit-cells. The wavelength is set as $\lambda = 1064$ nm, which is usually used in intense-light systems. The length and width are the control parameters used to manipulate the electric field distribution, phase difference, and transmittance.



Figure 1. Schematics of two unit-cells: (a) Nanobricks; (b) Nanoholes. The nanostructures have the same parameters as height H = 200 nm and lattice period P = 600 nm. The rectangular shapes are described by length L_b and L_h , and width W_b and W_h , respectively.

For absorbent materials, the analytical model of the optothermal effect can be defined by the imaginary part of the complex permittivity ε of silicon and the in-situ electric field |E|, which can be described as [23]:

$$P_{abs}\left(\vec{r},\omega\right) = \frac{0.5\varepsilon_0\omega \left| E\left(\vec{r},\omega\right) \right|^2 imag\left(\varepsilon\left(\vec{r},\omega\right)\right)}{sourcepower(\omega)}$$

where $P_{abs}(\vec{r}, \omega)$ is the spatial distribution of the fraction of absorbed power per cubic meter, normalized to the source power (unit: m⁻³). The absorption would transfer to heat, leading to the thermal effect. However, in metalenses made of nanostructures, the electric field distributes nonuniformly due to the localized-field effect. Subsequently, the simulation methods have to be exploited to calculate the electric field distribution in our study.

All the optical simulations in this study are implemented by the three-dimensional finite-difference time-domain (3D-FDTD) algorithm, and the optothermal simulations are based on the finite element method (FEM). The simulation region of nanostructures is surrounded by periodic boundaries in the *x*-axis and *y*-axis directions and perfectly matched layers in the *z*-axis direction. The simulation region of metalenses was surrounded by periodic boundaries in the *y*-axis direction and perfectly matched layers in the *x*-axis and *z*-axis directions. All the optical and thermal constants of materials were taken directly from the database [31].

3. Results and Discussion

To construct transmissive metalenses, a group of unit-cells should be designed with high transmittance and phase differences covering the $0-2\pi$ range. By sweeping the parameters (length L_b and L_h , and width W_b and W_h) of the nanostructures, the geometrical dependencies of the transmittance and phase difference are obtained via calculating the S-matrix parameter of the unit-cells, as shown in Figure 2. When changing the width W_b and length L_b of nanobricks, the transmittance can be tuned as shown in Figure 2a, and the phase difference of a transmitted light changes as shown in Figure 2b. The transmittance and phase difference of the hole unit-cells are also the functions of L_h and W_h . The strips of high transmittance come from the coupling between the electric/magnetic dipoles in the nanostructures. With suitable geometrical parameters, high transmittance of more than 90% can be obtained. When tuning the nanostructures geometrically to obtain the $0-2\pi$ phase coverage, the transmittance of unit-cells will decrease. Except for the transmittance and phase coverage, the electric field distribution in the unit-cells is also important for the intense-light applications. Thus, the electric field distributions of these nanostructures are also obtained via simulations.

Metalenses are composed of nanostructures that have digitized phase-control values covering the $0-2\pi$ range. In this study, the $0-2\pi$ range is digitized by 8 phase points with an interval of $\pi/4$; thus eight unit-cells are selected. When selecting unit-cells, ± 0.1 rad phase deviation is accepted to obtain better field confinement and higher transmittance, meaning that the unit-cells with phase differences of $n\pi/4 \pm 0.1$ rad (n = 0, 1, ..., 8) are chosen first. Then, the unit-cells with in-air field confinement and high transmittance are selected, which are marked by the white stars in Figure 2. The details of the selected unit-cells are shown in Figure 3. The transmittance-phase relationship of nanobricks and nanoholes are shown in Figure 3a,b, while the others describe the widths and lengths of the selected nanostructures. It is noted that at the phase point of $3\pi/4$, the transmittance is only 50%. The most energy is reflected by the nanostructure, not absorbed.



Figure 2. Optical properties of the unit-cells with nanobricks and nanoholes: (**a**) Transmittance and (**b**) Phase difference of the brick unit-cells as a function of L_b and W_b ; (**c**) Transmittance and (**d**) Phase difference of the hole unit-cells as a function of L_h and W_h .



Figure 3. The eight unit-cells with nanobricks or nanoholes selected for constructing metalenses: The transmittance and phase difference of (**a**) Nanobricks and (**b**) Nanoholes. The widths and lengths of (**c**) Nanobricks and (**d**) Nanoholes.

The responding electric field distributions of the selected unit-cells are shown in Figures 4 and 5 for nanobricks and nanoholes, respectively. The electric field of the selected unit-cells is normalized with the source. The x–y–plane distributions of field |E| are obtained with z = 100 nm, while the x–z–plane distributions are obtained with y = 0 nm. Because the phase control of transmitted light relies on the electromagnetic resonances, the field-enhancement effect in some unit-cells is inevitable to obtain the $0-2\pi$ phase coverage. To demonstrate the influence of the field distribution on the optothermal absorption, the optothermal absorption efficiencies of the selected unit-cells are simulated, and the mean values are shown in Figure 6. Under the illumination of the continuous incident light, the partial heat would spread rapidly to the whole nanostructure by thermal transmission due to the subwavelength size. Thus, the mean absorption is considered here. In Figures 4 and 5, for both nanobricks and nanoholes, the absorption efficiencies at the phase points $(0, \pi/4,$ $\pi/2$, $3\pi/4$) are smaller than the others. In Figure 4, we can see that at the phase points (π , $5\pi/4$, $3\pi/2$, $7\pi/4$), these unit-cells have stronger electric resonances and localized field intensities in the silicon bricks than that in the air zone. It means that the electric field in absorbent materials would lead to strong optothermal, and tuning the field into the air zone with ignorable absorption can reduce the heat effect. For example, in Figure 4b,c, the very strong field appears in the air zone, leading to a low absorption in Figure 6. These electric fields do not interact with the silicon directly, avoiding the optothermal effect. On the other hand, in Figure 5e-h, although most fields of nanoholes distribute in the air holes, some points with strong field intensities enhanced by the nanostructures appear on the Si-SiO₂ interfaces, resulting in strong absorption. Absorption is related to the square of the electric field amplitude $|E^2|$; thus, the field enhancement in absorbent materials will result in a strong absorption.



Figure 4. Electric field distributions of the eight selected unit-cells with nanobricks: (a-1-h-1) Normalized electric field distribution on the x-y plane with z = 100 nm; (a-2-h-2) Normalized electric field distribution on the x-z plane with y = 0 nm.



Figure 5. Electric field distributions of the eight selected unit-cells with nanoholes: (a-1-h-1) Normalized electric field distribution on the x-y plane with z = 100 nm; (a-2-h-2) Normalized electric field distribution on the x-z plane with y = 0 nm.



Figure 6. The mean absorption efficiencies of the selected unit-cells, which are defined as absorbed power per cubic meter, normalized to the source power.

Based on the selected unit-cells with the $0-2\pi$ coverage in Figure 3, two 1D metalenses are constructed and investigated. The phase profiles of the metalenses are $\varphi(x) = -k_0 \left(\sqrt{x^2 + f^2} - f\right)$, where k_0 is the wavenumber in a vacuum, x is the x-axis coordinate, and f is the focal length. The simulated metalenses have the size of 30 µm (x-axis) × 0.6 µm (y-axis). The focusing performances of the two metalenses are shown in Figure 7a,c. In optical absorption simulations, the x-axis and y-axis boundaries of the metalenses are set as "closed", and the z-axis boundaries are set as "shell". The absorption density distributions P_{abs} are shown in Figure 7c,d. It is seen that the absorption mainly concentrates in the nanobricks or at the corners of the nanoholes. Due to the heat conduction, the temperature distribution is different from the absorption density distribution. Thermal damage would appear once the maximum temperature in metalens is higher than the melting point 1683 K of silicon. Under the illumination of different incident power,

the maximum temperature values in the metalenses are simulated via the finite element method, as shown in Figure 8. To remove the influence of the environment, the ambient temperature of the SiO₂ substrate and air is set as a constant value of 300 K. In the heat simulations, all boundaries of the metalenses are set as "closed". When the illumination power changes, the corresponding heat energy will vary according to the absorption efficiencies in Figure 7. After calculating the thermal conduction and convection of the heat energy, it will stay at a steady-state. Then, the temperature distributions of the metalenses with varying illumination power are obtained. With the assumption that the optothermal property of silicon remains unchanged before the thermal damage happens, the maximum temperature has a linear relationship with the incident power. Although the stronger field distributes in the air zone, some weaker field still stays in the silicon and would be absorbed via the optothermal conversion, as shown in Figure 7b,d. Under the illumination of continuous light with a high power-density, the highest temperatures of metalenses can reach the metaling point due to heat accumulation. The metalens made of nanobricks starts to be damaged with an indent power of 2.70 W, while the nanohole one can handle the highest power of 2.18 W. The corresponding maximum power-density values are $0.15 \text{ W}/\mu\text{m}^2$ and $0.12 \text{ W}/\mu m^{2}$, respectively.



Figure 7. Focusing and absorption of the metalenses: (**a**) Intensity distribution at the focal point of the brick metalens; (**b**) The absorption density distribution in the brick metalens; (**c**) Intensity distribution at the focal point of the hole metalens; (**d**) The absorption density distribution in the hole metalens.



Figure 8. The maximum temperature in the metalenses with a nanobrick (blue) or nanohole (red) configuration under the illumination of different incident power. The black line marks the melting point of 1683 K of silicon.

4. Conclusions

In this study, the optothermal absorption in transmissive metalenses made of silicon nanobricks and nanoholes was investigated comparatively. The transmittance, phase difference, and field distribution of nanobricks and nanoholes were numerically analyzed. The optothermal results show that the electric field in the silicon zone would lead to an obvious thermal effect. The in-air electric field would not be absorbed by absorbent materials, avoiding the optothermal conversion. Meanwhile, the field enhancement also results in strong absorption of optical energy. Thus, the key to designing anti-damage metalens is manipulating the field distribution out of absorbent materials and restraining the field enhancement in nanostructures. Two presentative metalenses were designed based on these nanobricks and nanoholes. The optothermal simulations show that they can handle a maximum laser density of $0.15 \text{ W/}\mu\text{m}^2$ and $0.12 \text{ W/}\mu\text{m}^2$. The study compared the optothermal factors of electric-field distribution and enhancement. This provided an approach to improving high damage thresholds in transmissive metalenses for intense-light systems.

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