

Article

New Concept of Smart UAS-GCP: A Tool for Precise Positioning in Remote-Sensing Applications

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Abstract: Today, ground control points (GCPs) represent indispensable tools for products' georeferencing in all the techniques concerning remote sensing (RS), particularly in monitoring activities from unmanned aircraft system (UAS) platforms. This work introduces an innovative tool, smart GCPs, which combines different georeferencing procedures, offering a range of advantages. It can serve three fundamental purposes concurrently: (1) as a drone takeoff platform; (2) as a base station, allowing the acquisition of raw global navigation satellite system (GNSS) data for post-processed kinematic (PPK) surveys or by providing real-time GNSS corrections for precision positioning; (3) as a rover in the network real-time kinematic (NRTK) mode, establishing its position in real time with centimetric precision. The prototype has undergone testing in a dedicated study area, yielding good results for all three geodetic correction techniques: PPK, RTK, and GCP, achieving centimeter-level accuracy. Nowadays, this versatile prototype represents a unique external instrument, which is also easily transportable and able to connect to the GNSS RING network, obtaining real-time positioning corrections for a wide range of applications that require precise positioning. This capability is essential for environmental applications that require a multitemporal UAS-based study. When the real-time RING data are accessible to the scientific community operating in RS surveying, this work could be a helpful guide for researchers approaching such investigations.

Keywords: GCP; GNSS; PPK; RTK; UAS; remote sensing



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1. Introduction

Today, unmanned aircraft systems (UASs) represent a common platform for mapping and performing the spatial analysis of territories [1–3]. Data collection through these technologies offers results in terms of quality and reliability comparable to those of conventional techniques (e.g., topographic campaigns, terrestrial laser scanning, and conventional aerial photogrammetry) [4–6], which require higher costs and very long times [7].

Over the last few years, various achievements and improvements in UASs have been made by numerous researchers from different disciplines. In fact, commercial societies, research institutes, and industries are interested in unmanned aerial vehicles (UAVs) as one of the simplest and cheapest pieces of equipment for data acquisition, which also depends on drones' payloads.

Data acquired using UASs offer useful information for archaeological investigations and cataloging [8,9], geological and geomorphological surveys and monitoring [10–15], earthquake surface-faulting analyses [16], urban mapping [17], emergency assessments [18–20], land cover classifications [21–23], multitemporal investigations [24–26], and engineering applications [27,28]. Nowadays, most UASs include an onboard, multifrequency GNSS

receiver, which is very useful for geomatic applications [29,30]. In fact, it is used to support navigation and for products' georeferencing and three-dimensional (3D) positioning. To achieve high precision in 3D space when using remote-sensing techniques, it is necessary to use GCPs (ground control points) [31], and the number, accuracy, and distribution of GCPs in the investigated area [32–34] affect the precision of the geometric correction in remotely sensed imagery.

A precise georeferencing technique known as indirect georeferencing (IG) [35,36] consists of using GCPs to support assisted aerotriangulation (AAT) and reaches accuracies of a few centimeters, as evaluated using independent checkpoints (ICPs) [37]. The utilization of GCPs is the most accurate solution as it allows for the comparison of UAS images with those of any other remote-sensing product [38–40]. Following the IG approach, initially, images are georeferenced with the drone's navigation coordinates and can be affected by metric errors, especially in the elevation component. Subsequently, point clouds are projected in an absolute coordinate system through a 3D linear similarity transformation taking into account the GCPs' coordinates acquired during the survey. Using these steps, it is possible to obtain point clouds with great accuracy. However, the acquisition of terrestrial GCPs can be the main obstacle in some important applications of UASs, such as forest inventories and mapping and surveys in areas with steep slopes and susceptible to landslides, avalanches, and other potential risks [41].

An alternative georeferencing method for UAV images has recently emerged, namely, direct georeferencing (DG) [42,43], whereby control is provided by measuring digital image positions at exposure times with centimeter-level accuracy [44]. This method uses a UAS-mounted GNSS receiver, which is capable for supporting dual frequency, multiconstellation phase observations [45]. The use of an inertial measurement unit (IMU) and a GNSS for DG can result in quick data collection and a significant improvement in work efficiency, rendering DG less time-consuming and costly. Different authors have evaluated the accuracy of UAV-based DG methods with GNSS RTK/PPK technology, and the experimental results highlighted that horizontal and vertical RMSE values (root mean square error) [46,47] are on the order from centimeters to decimeters [48–52].

When carrying out a flight mission for photogrammetric purposes, there is a need to bring a lot of instrumentation into the field to obtain GNSS measurements. From these difficulties arose the need to build a portable and manageable instrument that contains as much functionality and instrumentation as possible.

This work describes and presents a smart GCP (S-GCP), implemented by the authors, with the following features: a multi-constellation/multi-band (L1, L2, and L5) GNSS receiver, Wi-Fi and Bluetooth connections, a 4G LTE router, and a power system with solar energy charging and a cooling mechanism.

This new tool is able to work with various configurations as follows:

1. The S-GCP is used as takeoff and landing points for the drone;
2. The S-GCP is used as a GNSS base to acquire raw GNSS data for the post-processing analysis (PPK survey);
3. The S-GCP is used first to receive the real-time correction from CORS (specifically, RING networks, [53]) and then provide it to the drone (RTK survey);
4. The S-GCP is used as a GNSS base to provide corrections to the rover in GCP measurements (GCP surveys).

In particular, in Section 3, "Experiments and Results", the performance of the S-GCP set with configurations described in points 2, 3, and 4 are evaluated. The outcomes are examined separately and then compared to assess the accuracy of the instruments during a photogrammetric survey.

2. Materials and Methods

The tool proposed in this paper is assembled with equipment and materials already available at INGV. All the instrumentation is contained in a portable suitcase made up of

two resealable solar panels; their size is $675 \times 540 \times 35$ mm, and they work at a tension of 18 V and a maximum power of 50 Wp, as depicted in Figure 1.

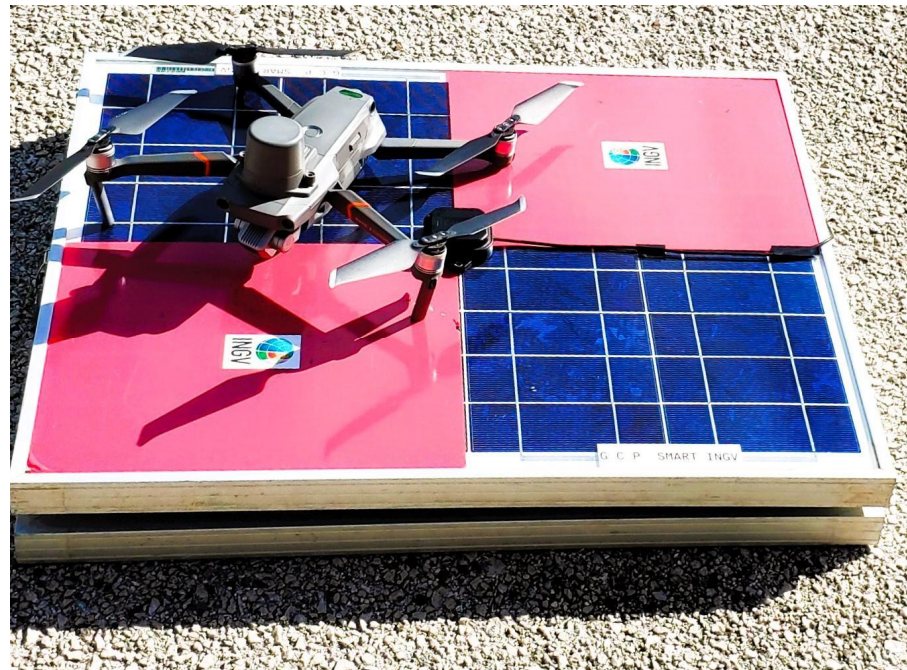


Figure 1. Suitcase of smart GCP. The small back box is the GNSS antenna.

On the suitcase is installed a u-blox ANN-MB multiband (L1, L2/E5b/B2I) active GNSS antenna. Inside the suitcase are installed the components described below and presented in Figure 2.

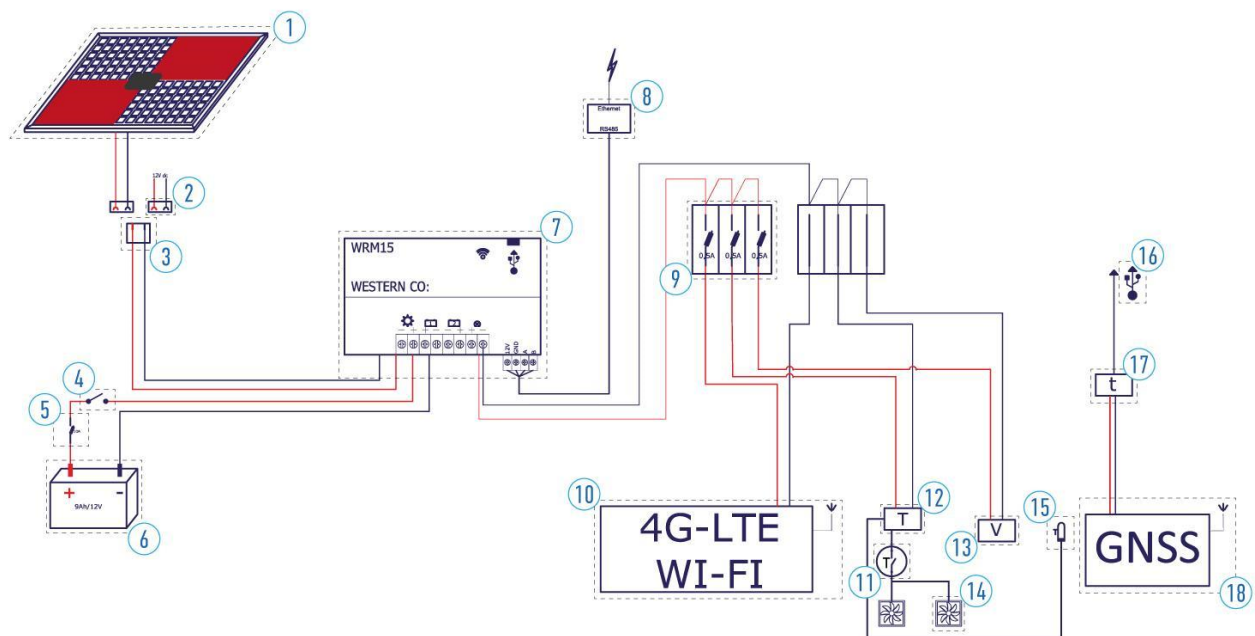


Figure 2. S-GCP components' connection: (1) solar panel; (2) power socket (DC max, 50 V); (3) power plug (DC max, 50 V); (4) unipolar switch; (5) disconnector with fuse holder; (6) solar battery (9 Ah, 12 V); (7) charge regulator; (8) RS485/ethernet interface; (9) disconnector with fuse holder; (10) Router-Board (Mikrotik); (11) NO contact; (12) temperature control module; (13) voltmeter; (14) cooling fan; (15) temperature probe; (16) USB connector; (17) delay switch (30 s); (18) GNSS receiver; red lines indicate positive electrical cables, black lines indicate negative.

2.1. Power System

The power supply system of the S-GCP is standalone, consisting of a polycrystalline silicon photovoltaic module, a WRM15 charge regulator produced by Western Co. (San Benedetto del Tronto, Italy), and a hermetic lead–acid accumulator. The charge regulator is equipped with an MPPT charging circuit that can optimize the charge of the accumulators with any photovoltaic module that has a maximum power Voltage (V_{mp}) greater than the battery voltage and that falls within the open circuit Voltage limits (V_{oc}) under 100 V. In addition, the system can also be recharged by means of a special 12 V DC power supply having a special power socket. The charge regulator is also equipped with an RS485 serial interface, thanks to which it is possible to set it and verify its operating status through the MODBUS communication protocol. The collected telemetry data can be consulted through the following:

- a web app interface, if the user is close to the S-GCP, through a Bluetooth connection (Figure 3a), ensuring the monitoring and the configuration of different parameters, including the produced power, load power, and battery charging;
- a web portal that can be accessed remotely, as illustrated in [54] (Figure 3b). Thanks to some Python queries that allow for storing, over time, information related to electrical parameters, such as the battery voltage, internal temperature, load current, photovoltaic current, photovoltaic voltage, and battery temperature.

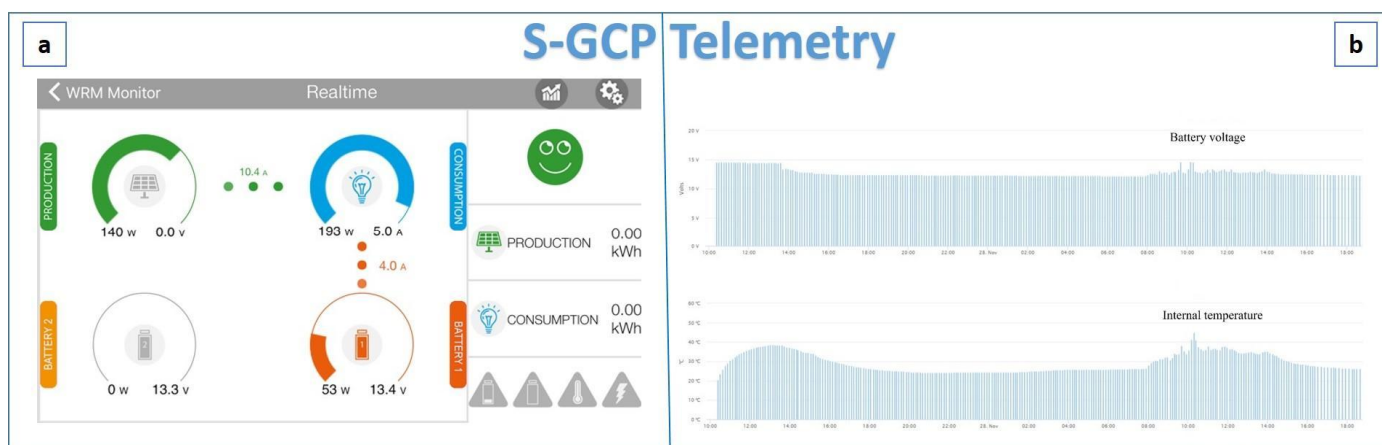


Figure 3. Real-time telemetry: (a) Bluetooth app for mobile devices where it is possible to visualize both the battery solar recharging and the S-GCP power consumption; (b) web portal that shows the battery voltage and the temperature inside the suitcase.

2.2. GNSS Data Acquisition

The GNSS antenna is connected to an Emlid Reach M2 (<https://emlid.com/reach/> accessed on 16 March 2024) GNSS receiver inside the S-GCP box. It is a multiband and multifrequency receiver that allows for precise UAS navigation and mapping. It provides robust performance and quick initialization, allowing for work on long baselines (e.g., a few tens of kilometers, [55]). The receiver has installed its web interface (Figure 4) to set different configurations and manage the collected data.

The user can visualize the interface by connecting via the Internet to the IP device address or via the ReachView smart app available for the Android and IOS operating systems.

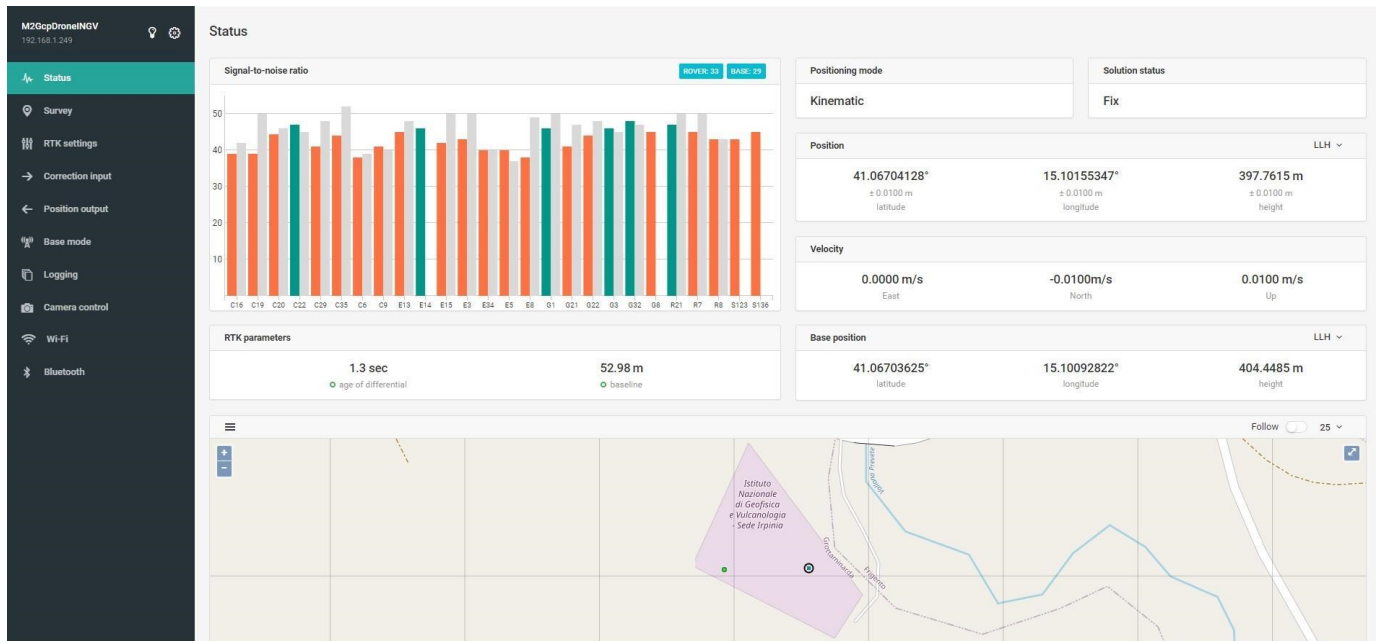


Figure 4. GNSS ReachView web interface. On the left, there are various tools for the system’s settings; the central part displays a comprehensive overview of the GNSS’s status, which includes the number and SNR of satellites, the positioning mode, the solution status, and the accuracy and coordinates of both the base and rover and their locations on a map.

2.3. Data Transmission

The S-GCP Internet connection is ensured by an LTE router consisting of a Mikrotik RouterBoard (RB912R-2nD-LTm) and a Mikrotik R11e-LTE modem.

The router, thanks to a secure SSTP VPN tunnel with the INGV Irpinia headquarters (<http://www.irp.ingv.it> accessed on 16 March 2024), allows the remote and real-time checking of the operating status of the instrumentation (i.e., the S-GCP and charge controller) and interaction with the relative configurations. Moreover, thanks to the VPN connection, if the smart GCP works in the NRTK (network real-time kinematic) mode, it can receive corrections via NTRIP (the networked transport of the RTCM via the internet protocol) from the stations of the National Integrated Network GNSS (RING—<http://ring.gm.ingv.it> accessed on 16 March 2024) collected by an NTRIP caster server (Figure 5). The implemented tool is the only platform capable for connecting and communicating (i.e., receiving corrections) with the GNSS RING network at the national level, even outside the INGV intranet systems. However, in the case of a lack of Internet connections, the acquired data can be collected and then corrected following the post-processing approach.

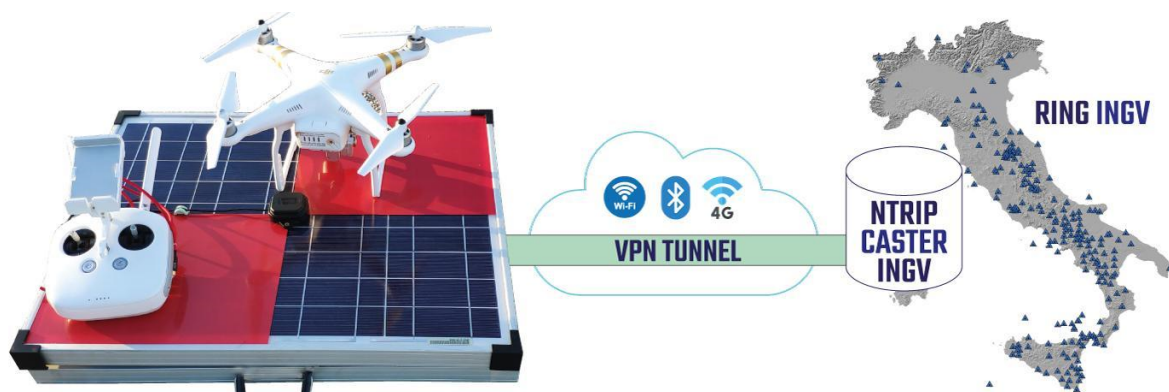


Figure 5. Data transmission system illustrating the various types of connections between the RING network and the S-GCP prototype through the VPN tunnel.

3. Experiments and Results

3.1. Test Site, Reference Points, Ground Control Points, and Mission Planning

The test site corresponds to the parking lot of the INGV Irpinia headquarters. The area is mostly flat and paved and all around, small trees and light fixtures are distributed throughout. On the top of the building, the permanent station (GRO1) of the RING network is installed.

Initially, 15 reference points (RPs) were measured in the NRTK mode, as shown in Table 1. The antenna was set at 2.134 m on the ground. The acquisitions were performed using a rover (Emlid Reach RS2) connected through Wi-Fi to the S-GCP to receive corrections (RTCM3) from the mountpoint (GRO1) (with a very short baseline) of the NTRIP caster INGV.

Table 1. Reference point (RP) measurements.

RP	Longitude	Latitude	Ellipsoidal Height (m)	RMS Longitude (m)	RMS Latitude (m)	RMS Height (m)	Antenna Height (m)	Solution
RP1	15.10173960	41.06693724	398.501	0.010	0.011	0.010	2.134	FIX
RP2	15.10158153	41.06699612	397.791	0.010	0.010	0.010	2.134	FIX
RP3	15.10142833	41.06692386	397.548	0.030	0.039	0.036	2.134	FIX
RP4	15.10150068	41.06700504	397.582	0.011	0.010	0.011	2.134	FIX
RP5	15.10151433	41.06711872	397.596	0.010	0.011	0.013	2.134	FIX
RP6	15.10135649	41.06734742	397.703	0.014	0.011	0.015	2.134	FIX
RP7	15.10156138	41.06665081	402.284	0.012	0.013	0.011	2.134	FIX
RP8	15.10097971	41.06684580	400.009	0.010	0.012	0.014	2.134	FIX
RP9	15.10067424	41.06725649	398.734	0.011	0.013	0.011	2.134	FIX
RP10	15.10092421	41.06762236	397.260	0.019	0.011	0.025	2.134	FIX
RP11	15.10166062	41.06729281	396.962	0.010	0.014	0.013	2.134	FIX
RP12	15.10195685	41.06701512	397.679	0.012	0.014	0.011	2.134	FIX
RP13	15.10195654	41.06681348	399.632	0.014	0.011	0.018	2.134	FIX
RP14	15.10055287	41.06697345	401.143	0.011	0.010	0.011	2.134	FIX
RP15	15.10109080	41.06782385	396.144	0.010	0.012	0.011	2.134	FIX

In addition, the positions of the other 30 ground control points (GCPs) were acquired to be used as control points during photogrammetric data processing (UAS-GCP survey, Section 3.3) and are summarized in Table 2.

Table 2. Ground control point (GCP) measurements.

GCP	Longitude	Latitude	Ellipsoidal Height (m)	RMS Longitude (m)	RMS Latitude (m)	RMS Height (m)	Antenna Height (m)	Solution
GCP1	15.10163383	41.06694796	398.115	0.010	0.010	0.011	2.134	FIX
GCP2	15.10140970	41.06686684	397.570	0.013	0.011	0.011	2.134	FIX
GCP3	15.10143691	41.06697751	397.603	0.010	0.011	0.013	2.134	FIX
GCP4	15.10148248	41.06706010	397.642	0.013	0.011	0.032	2.134	FIX
GCP5	15.10158908	41.06714598	397.599	0.013	0.014	0.010	2.134	FIX
GCP6	15.10147918	41.06726008	397.729	0.011	0.011	0.013	2.134	FIX

Table 2. Cont.

GCP	Longitude	Latitude	Ellipsoidal Height (m)	RMS Longitude (m)	RMS Latitude (m)	RMS Height (m)	Antenna Height (m)	Solution
GCP7	15.10119349	41.06744444	397.649	0.010	0.018	0.010	2.134	FIX
GCP8	15.10112709	41.06759876	397.453	0.013	0.014	0.015	2.134	FIX
GCP9	15.10095407	41.06737923	397.395	0.011	0.010	0.011	2.134	FIX
GCP10	15.10082529	41.06718486	397.188	0.010	0.011	0.014	2.134	FIX
GCP11	15.1007533	41.0670634	396.985	0.015	0.016	0.010	2.134	FIX
GCP12	15.1009648	41.0669831	397.176	0.013	0.015	0.013	2.134	FIX
GCP13	15.10114986	41.06691	397.276	0.020	0.025	0.020	2.134	FIX
GCP14	15.10156166	41.06683385	397.955	0.011	0.010	0.011	2.134	FIX
GCP15	15.10169574	41.06678654	398.666	0.010	0.011	0.010	2.134	FIX
GCP16	15.10142539	41.06668525	401.606	0.016	0.013	0.013	2.134	FIX
GCP17	15.10077957	41.06694036	399.848	0.013	0.014	0.014	2.134	FIX
GCP18	15.10060978	41.06712069	399.680	0.013	0.018	0.011	2.134	FIX
GCP19	15.10084447	41.06737075	397.923	0.011	0.010	0.011	2.134	FIX
GCP20	15.10089415	41.06773107	396.964	0.013	0.015	0.020	2.134	FIX
GCP21	15.10124942	41.0677565	396.232	0.011	0.013	0.010	2.134	FIX
GCP22	15.10141916	41.06755329	396.566	0.019	0.018	0.017	2.134	FIX
GCP23	15.10162296	41.06737292	396.664	0.010	0.010	0.011	2.134	FIX
GCP24	15.1018342	41.06712677	397.262	0.015	0.016	0.017	2.134	FIX
GCP25	15.10201904	41.06691067	398.621	0.014	0.014	0.013	2.134	FIX
GCP26	15.10182229	41.06675068	399.040	0.020	0.013	0.025	2.134	FIX
GCP27	15.10187161	41.06688077	399.112	0.013	0.014	0.015	2.134	FIX
GCP28	15.10076534	41.0675224	397.567	0.011	0.010	0.011	2.134	FIX
GCP29	15.10117618	41.06681989	399.863	0.010	0.011	0.010	2.134	FIX
GCP30	15.10173165	41.06659000	404.059	0.015	0.017	0.016	2.134	FIX

All the positions of the RPs and GCPs were acquired by fixing the carrier phase ambiguities [56] and RMS values within a few centimeters.

The aerial surveys were performed on 3 May 2023, using a DJI Phantom 4 RTK equipped with the RTK/PPK system. For each mission (i.e., PPK, RTK, and GCP surveys) the same flight plan was used (see Figure 6). The software employed for the mission planning is UgCS Enterprise version 4.16 (<https://shop.ugcs.com/en-it> accessed on 16 March 2024). With this software, the terrain-following module allows for the creation of missions by keeping the drone's height from the ground constant. In particular, the tool Photogrammetry was used, and the parameters were set as follows: the flight altitude was 50 m above the ground for collecting nadiral images with a forward overlap of 80% and a side overlap of 70%, achieving an average ground sample distance (GSD) of 1 cm. The flight speed was 3.5 m/s, and the drone flew for 5.34 min, capturing 131 images and covering an area of 14,725 m².



Figure 6. UgCS Enterprise v. 4.20 software interface for UAS mission planning. In the left panel are shown the set parameters for the flight plan; the right panel shows the UAS telemetry, and the bottom window displays the survey's altimetry and number of waypoints.

3.2. UAS-PPK Survey

In this approach, the UAS is set to acquire GNSS raw data at 10 Hz, and at the same time, for each photo, the corresponding triggers are recorded. These data will subsequently be used for image geotagging. Simultaneously, the GRO1 station was set for GNSS raw data acquisition at 10 Hz.

Photo geotagging is performed using RedToolbox v. 3.1 software (Figure 7—<https://www.redcatch.at/redtoolbox/> accessed on 16 March 2024). First, you need to choose the GNSS data format and trigger used by the drone (DJI Phantom 4 RTK L1/L2) and then the format of the correct data output from the software (in this case, Agisoft project .psx, TextFile .txt, and Pdf Report .pdf files). Moreover, the choice of the output coordinate system is required, and in this case, the ellipsoidal model WGS84 was selected.



Figure 7. RedToolbox interface: (a) device and output setting interface; (b) data loading and processing.

Successively, (i) the acquired photos, (ii) GNSS IMU and triggers and UAS data, and (iii) GNSS data of the base station (Figure 8b) were imported and processed with the RedToolbox environment. Regarding the position of the base station (GRO1), it was estimated, considering the information in the header of the RINEX file, to employ the same position in the RTK and GCP surveys. After the geotagging step, the corrected photos were processed following the SfM workflow [57,58] implemented in Agisoft Metashape Professional software (Version 2.03, Agisoft LLC, St. Petersburg, Russia), including image alignment, sparse point cloud generation, dense point cloud refinements, and DEM generation.

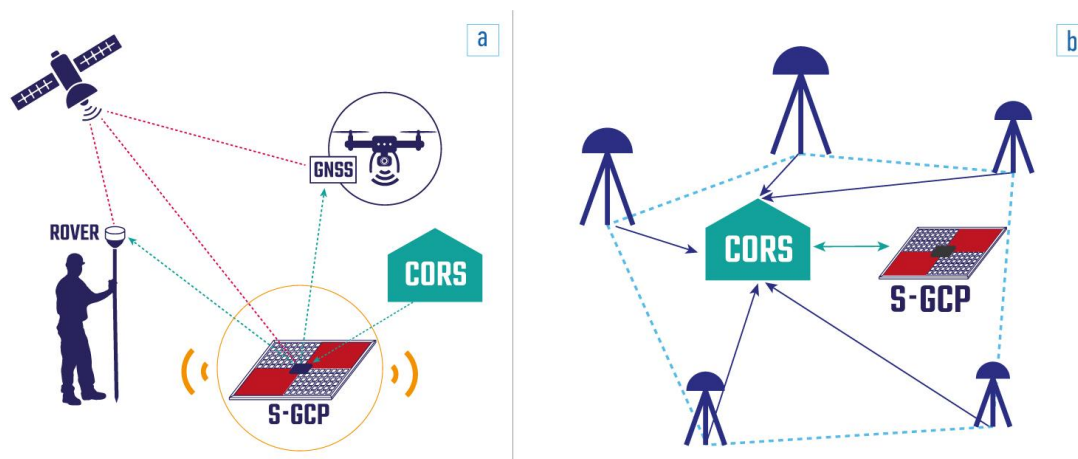


Figure 8. (a) S-GCP in base/NTRIP configuration to provide real-time GNSS correction to rover and UAS; (b) S-GCP in rover/base configuration to receive real-time GNSS corrections from the CORS and save the raw data locally, using them later in PPK.

3.3. UAS-RTK Survey

In the second test, the UAS was connected to the S-GCP, gaining real-time RTCM3 correction (sampling at 1 Hz) from the GRO1 mountpoint via the NTRIP caster. With this configuration, the S-GCP plays a key role in ensuring the correct navigation to the drone in RTK, and, then, the geotagged images obtained the precise position in the adopted reference system (Figure 8a). Successively, the obtained imagery was processed with the same approach as that in the UAS-PPK survey.

3.4. UAS-GCP Survey

With this configuration, the UAS flight was performed without any position corrections, and, consequently, the geotags of the acquired images were affected by metric errors (The average errors for 'X', 'Y', and 'Z' were 2.19, 2.32, and 2.95 m, respectively.).

In the second step, during photogrammetric processing, the measured GCPs (Figure 8a) were recognized in each image and adopted for the point cloud optimization. In this way, we tried to refine the positions of the captured images by reducing the geotag metric errors to the centimeter scale.

3.5. Survey Results

In this section, the three digital elevation models (DEMs) obtained in various acquisition modes are introduced and subsequently compared. The 3 DEMs were obtained considering the same flight mission and the same number of images but with different geodetic correction approaches. So, the models are perfectly overlapping considering the planar coordinates.

In the GIS environment (Figure 9), the ellipsoidal elevation value was measured for each DEM at the same X and Y coordinates of the 15 RPs.

Table 3 indicates the RPs' elevations in meters a.s.l. (column 4), as measured with Emlid Reach RS2, and the projections of the elevations measured in the GIS environment onto the three obtained DEMs (columns 5, 7, and 9) corresponding to the same RP coordinates.

Columns 6, 8, and 10 show the height differences (in meters) between the RPs and the 3 DEMs. It is interesting to note that for the DEM obtained through PPK processing, the elevation difference with respect to all the RPs never exceeds 3 cm.

Considering the DEM obtained with the RTK survey, the differences in the RPs range from 0.8 cm to 9.7 cm. Therefore, this DEM shows an error larger than that of the PPK-survey DEM. Lastly, the DEM produced with the use of GCPs seems to have the highest error rate. In fact, corresponding to RP4, the elevation difference is 13.6 cm, representing

the highest value among the three DEMs. However, for the other RPs, the error is similar to that measured in the RTK survey.

Despite looking at the absolute value of the average difference, PPK processing produced the best result (1.7 cm), while the other two processing methods had errors similar to 3–4 cm.

The information in columns 6, 8, and 10 of Table 3 is depicted in Figure 10. As shown, only for some points, there are substantial differences, and they are located very close to the building and parking area.

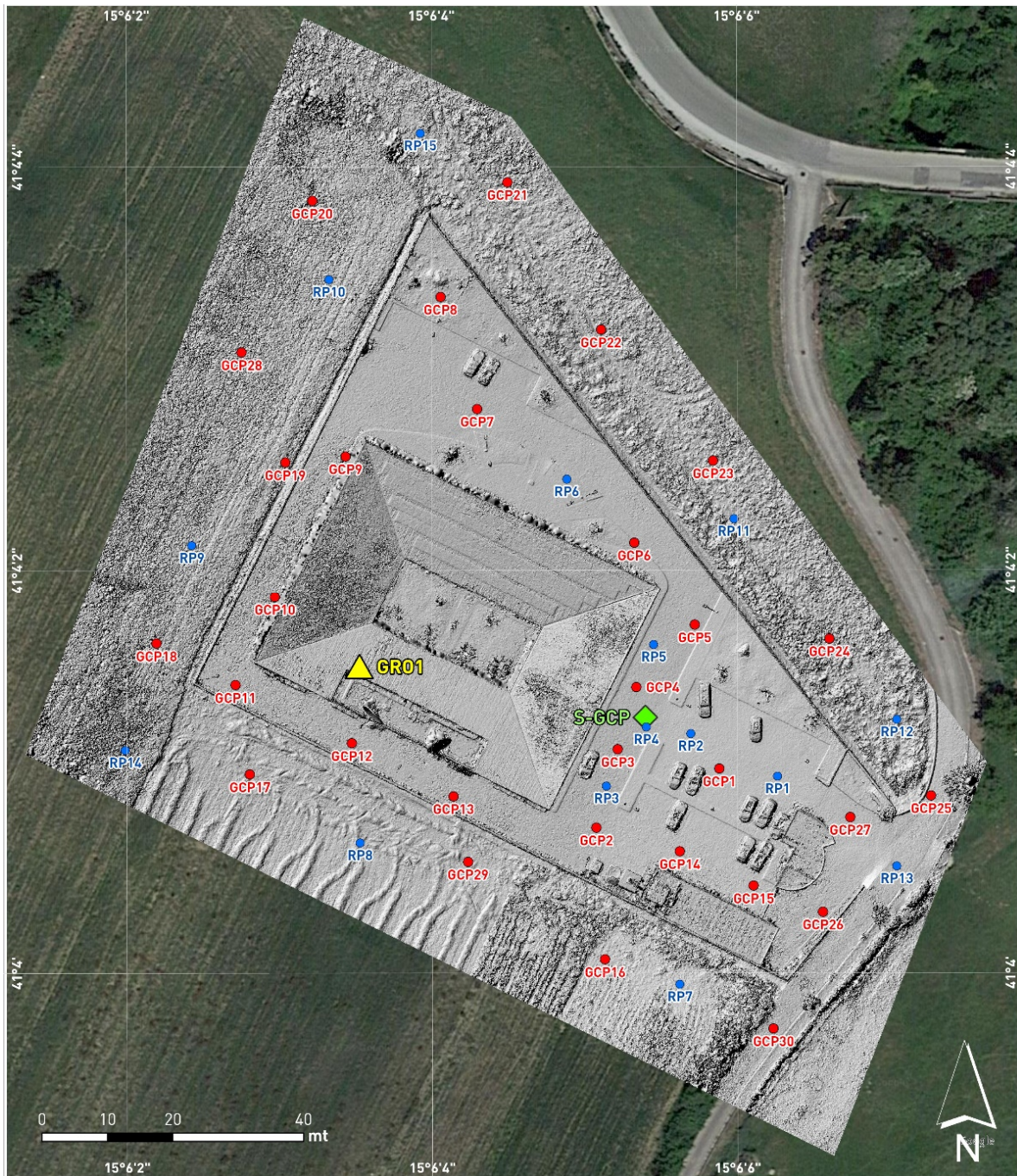


Figure 9. PPK-survey DEM derived from the positions of the GCPs (red circles), RPs (blue circles), GRO1 RING station (yellow triangle), and S-GCP (green diamond).

Table 3. Survey result comparison.

RP	Longitude	Latitude	RP Height (m)	PPK Height (m)	Diff. RP PPK (m)	RTK Height (m)	Diff. RP RTK (m)	GCP Height (m)	Diff. RP GCP (m)
RP1	15.1017396	41.06693724	398.501	398.522	0.021	398.586	-0.085	398.475	0.026
RP2	15.10158153	41.06699612	397.791	397.81	0.019	397.78	0.011	397.701	0.09
RP3	15.10142833	41.06692386	397.548	397.563	0.015	397.601	-0.053	397.601	-0.053
RP4	15.10150068	41.06700504	397.582	397.598	0.016	397.63	-0.048	397.446	0.136
RP5	15.10151433	41.06711872	397.596	397.621	0.025	397.499	0.097	397.567	0.029
RP6	15.10135649	41.06734742	397.703	397.732	-0.029	397.722	-0.019	397.753	-0.05
RP7	15.10156138	41.06665081	402.284	402.271	0.013	402.26	0.024	402.254	0.03
RP8	15.10097971	41.0668458	400.009	400.029	-0.02	400.019	-0.01	400.03	-0.021
RP9	15.10067424	41.06725649	398.734	398.743	-0.009	398.715	0.019	398.745	-0.011
RP10	15.10092421	41.06762236	397.26	397.278	-0.018	397.233	0.027	397.281	-0.021
RP11	15.10166062	41.06729281	396.962	396.95	0.012	396.94	0.022	396.952	0.01
RP12	15.10195685	41.06701512	397.679	397.67	0.009	397.658	0.021	397.661	0.018
RP13	15.10195654	41.06681348	399.632	399.652	-0.02	399.64	-0.008	399.601	0.031
RP14	15.10055287	41.06697345	401.143	401.13	0.013	401.121	0.022	401.155	-0.012
RP15	15.1010908	41.06782385	396.144	396.16	-0.016	396.128	0.016	396.184	-0.04
Average Difference							0.017	0.032	0.038

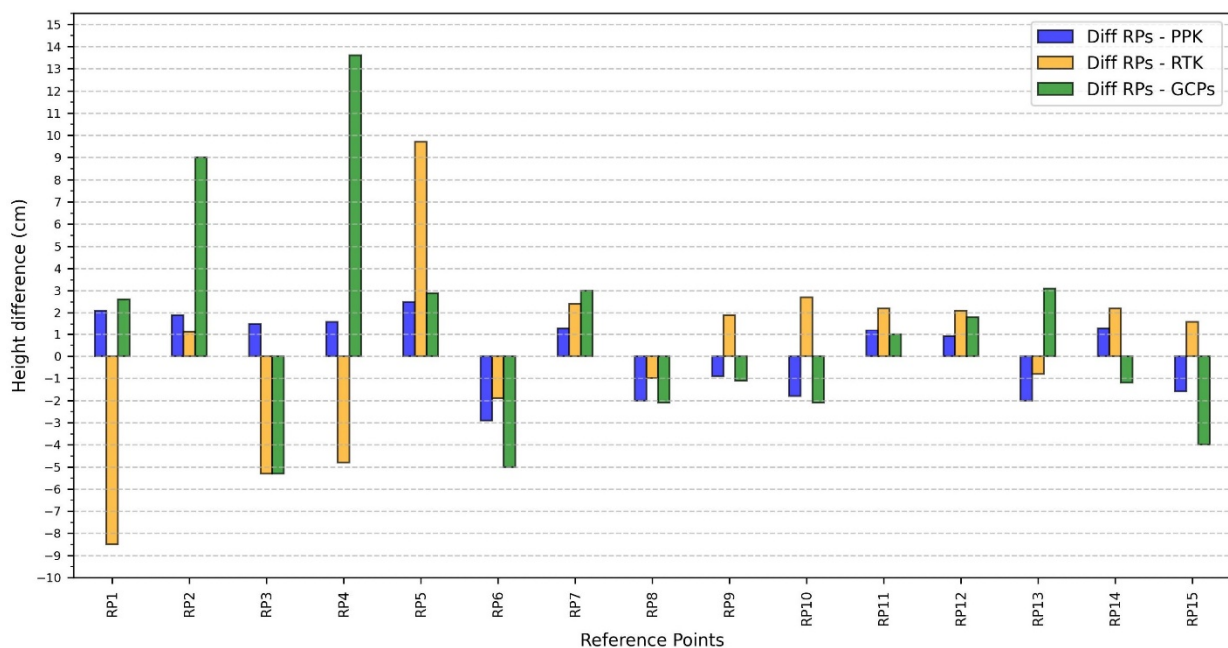


Figure 10. Graphical comparison among the height differences (cm) of the three DEMs measured for the 15 RPs that were considered.

4. Discussion

New technological platforms for quick land surveying and measurements, such as UASs, are widespread in different fields, and the precise georeferencing of acquired data plays a key role in obtaining robust products. This study concerns the use of the S-GCP prototype by describing its application potential in high-precision georeferencing drone surveys. For this purpose, three DEM outcomes were compared, in terms of accuracy and error estimation, taking into account different survey approaches. Specifically, for the

traditional UAS photogrammetric application, where the point cloud and all the resulting products are processed by georeferencing, the use of GCPs has been compared with that in the other two image orthorectification modes: PPK and RTK.

As shown in Section 3.4, the three different geodetic correction techniques constitute valid approaches for proximal remote sensing. Among them, PPK processing proved to be the most accurate as it showed the lowest average error, less than 2 cm, according to previous studies by Cirillo et al. (2022) and Martínez-Carricondo et al. (2023). This result was predictable because in PPK, the correction of the GNSS data can be refined in retrospect, adding more correct information, and because by working in RTK, the sample frequencies are lower. In fact, if the UAV in our test flew at 3.5 m/s and corrected its position at a frequency of 1 Hz, it obtained a correct position at every 3.5 m. From the drill, in PPK, we worked with a sampling frequency at 10 Hz, obtaining a new position at every 35 cm. The PPK method for georeferencing provides consistent accuracy and can take the place of the GCP-based method when it is challenging [59].

In the other two tests that were mentioned, the performance of the S-GCP proved to be highly promising also in scenarios where a nearby CORS system was unavailable. The vertical RMSE values achieved through RTK and GCP surveys may suffice for a broad range of medium-coarse mapping tasks, where extremely high-accuracy height models are not imperative. Specifically, in the RTK survey outlined in this study, the short baseline between the drone and the mountpoint (GRO1) significantly contributes to minimizing the RMSE. At the same time, when faced with the absence of a nearby and stable GNSS station, the S-GCP, leveraging its VPN connection to the RING network, has the potential to reduce the RMSE thanks to its capability to function as a station for obtaining position corrections.

The prototype presented herein is the only one that can work with the real-time data of the national GNSS INGV network, providing corrections to any connected device (terrestrial rover or drone). RING-INGV's GNSS data are currently available a few hours after acquisition (<ftp://gpsfree.gm.ingv.it> accessed on 16 March 2024), with 30 s sampling. In the near future, INGV also plans to provide a real-time GNSS data distribution service with 1 Hz sampling.

GCP-derived DEMs are affected by higher diffuse errors that can be explained by the RMSE values in Table 2. In fact, despite the solution in the FIX mode, there are GCP positions acquired by Emlid Reach RS2 with different RMSEs, which may be because of problems in the ambiguity resolution processes. This survey was conducted on a flat surface without significant elevation gradients but with the presence of disturbing elements (buildings, walls, cars, and light poles). The higher errors corresponding to RPs were recorded in the crowded area, while for the other points (RP6-RP15), thanks to the absence of obstacles, the GCP-derived model could also be compared with the other two. From RP1 to RP5, the model derived from RTK also had the same behavior, while the model derived from PPK also demonstrated its effectiveness in the parking lot. S-GCP-based methods improve speed and allow photogrammetry to be used for a wider range of tasks in both industry and science by ensuring the required accuracy. Another strong point of S-GCP concerns its easy portability. In fact, in addition to the environmental conditions necessary for successful flights and scanning, such as the temperature, sun exposure, and humidity, the transportation of instrumentation to the field to have precise GNSS measurements may be an additional problem to be solved. Therefore, having a handy, easily transportable, and, at the same time, very reliable tool in terms of GNSS data management represents a further step forward for smart data acquisition surveys.

5. Conclusions

In this study, the potentialities of S-GCPs were evaluated during photogrammetric surveys, and, in particular, the contribution of S-GCPs to the correct geopositioning of acquired images has been assessed. The obtained DEMs have been compared, highlighting differences in terms of elevation errors corresponding to known reference points. In three distinct tests, the utilization of S-GCPs highlighted their potential across all the adopted

photogrammetric approaches. Although the PPK method yielded the most precise DEM, both the GCP and RTK methods produced acceptable elevation models, demonstrating the effectiveness of S-GCPs in enhancing accuracy thanks to their capability to obtain corrections from private and public GNSS CORS stations (specifically, in the RING network).

In conclusion, the use of S-GCPs allows for connecting drones to different stations in the RING network, and, therefore, their use can be a replicable added value throughout the Italian national territory. Furthermore, there are RING stations located in other areas of the Mediterranean Basin (e.g., Malta and Greece), allowing for the use of S-GCPs outside of Italy.

The RING network represents a scientifically driven permanent GNSS infrastructure, and the capability of S-GCPs to connect to it constitutes an added value of this tool, especially in the reconstruction of differential DEMs along a certain time span: for this application, having a stable station within a CORS plays a key role.

With regard to the encouraging results that were achieved, the S-GCP prototype can be used for several data acquisition campaigns involving the use of drones and where high precision in the georeferencing of the acquired data is required, such as lidar, echo-sounding, and ground-penetrating radar.

In addition, the S-GCP prototype can be used in other geodesy applications: for example, it can be used as a GNSS mobile station for “noise tests” that are carried out at sites where the GNSS station of a permanent network is to be installed. S-GCPs would significantly reduce the amount of equipment to be transported and installed, making both telemetry and GNSS data usable in real time and allowing for instant “quality checks” of the same.

The authors, in the next few months, will start the procedure to obtain the patent of the prototype, and in the future, substantial changes can be made to the tool presented in this article by optimizing the size and components.

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