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Abstract: High-quality, reproducible tip coatings are essential for minimizing faradaic currents in electrochemical scanning tunneling microscopy (EC-STM), especially during in situ and operando measurements. The variability inherent in manual coating methods, influenced by the operator's skill and a lack of standardization, can lead to inconsistent results, increased research costs, and a greater workload. This study introduces an Automated Tip Coater (ATC) designed to automate and standardize the tip coating process. The ATC features a tip movement system using stepper motors, a rotation module with a DC motor, and a heating block based on a soldering iron. It is controlled by an Arduino development board, supported by motor drivers, and has a user-friendly interface with an OLED display and encoder. The ATC coating mechanism includes a redesigned plate with a reduced gap size and a milled tray to precisely control the amount of insulating material applied to the tip. A fast cyclic voltammetry test in a 0.1 M HClO₄ electrolyte demonstrated that over 75% of ATC-coated tips achieved excellent insulation with leakage currents below ±50 pA—and 30% below \pm 10 pA—suitable for highly sensitive experiments. Further measurements with EC-STM using the newly coated tips investigated the electrochemical behavior of highly oriented pyrolytic graphite (HOPG), revealing detailed atomic structures under dynamic electrochemical conditions. The ATC significantly enhances reproducibility, reduces dependency on operator skills, and lowers research costs while improving the accuracy and reliability of EC-STM measurements.

Keywords: electrochemical scanning tunneling microscopy (EC-STM); automated tip coater (ATC); tip insulation; cyclic voltammetry (CV); in situ measurements; operando conditions; electrocatalysis; high-resolution imaging; HOPG surface

1. Introduction

Electrochemical scanning tunneling microscopy (EC-STM) is a powerful technique that enables the study of various surface phenomena at the atomic level under electrochemical conditions [\[1–](#page-9-0)[3\]](#page-10-0). This capability is crucial for advancing our understanding of dynamic processes in various fields, including electrocatalysis [\[4–](#page-10-1)[6\]](#page-10-2), corrosion [\[7](#page-10-3)[,8\]](#page-10-4), energy storage [\[9](#page-10-5)[,10\]](#page-10-6), and nanotechnology [\[11,](#page-10-7)[12\]](#page-10-8). By enabling in situ and operando measurements, EC-STM allows researchers to observe real-time changes in the surface structure and composition during electrochemical reactions, providing insights that are essential for developing next-generation technologies in these areas [\[13](#page-10-9)[,14\]](#page-10-10).

Recent advancements in EC-STM have demonstrated the potential to identify electrocatalytically active sites with atomic precision by analyzing noise in the tunneling current [\[13,](#page-10-9)[15](#page-10-11)[–26\]](#page-10-12). By using this approach, it is possible to monitor catalytic sites during electrochemical reactions, offering insights into their stability and providing quantitative information related to the macroscopic onset potential, Tafel slope, and turnover frequency (TOF) with sub-nanometric spatial resolution, even for single-atom catalytic sites. This new method enables the determination of the nature, relative abundance, and specific activity of the sites where electrocatalytic processes occur, all at the atomic level. However, one of the

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major challenges in obtaining accurate and reliable EC-STM data is maintaining faradaic currents at negligible levels. These currents, which arise from electrochemical reactions at the tip due to the applied bias potential, can significantly interfere with the tunneling current, especially during in situ and operando measurements where dynamic changes in the electrochemical environment are prevalent.

Therefore, the EC-STM tips must be coated with a chemically and electrochemically inert insulating material, leaving only the apex exposed to the electrolyte [\[27\]](#page-10-13). Effective tip coatings markedly reduce unwanted faradaic leakage currents. Various insulating techniques have been developed, differing in the choice of coating materials and specialized equipment required. These methods include glass coating [\[28–](#page-10-14)[31\]](#page-11-0) followed by the sputter deposition of SiO [\[32\]](#page-11-1), the application of cataphoretic paint [\[33,](#page-11-2)[34\]](#page-11-3), the thermal evaporation of silicon or magnesium oxides [\[35\]](#page-11-4), and the use of waxes [\[36](#page-11-5)[,37\]](#page-11-6) or polymers such as nail varnish [\[38–](#page-11-7)[40\]](#page-11-8), epoxy resin [\[41–](#page-11-9)[43\]](#page-11-10), and silicon rubber [\[41](#page-11-9)[,44\]](#page-11-11). Molten polymers [\[29](#page-10-15)[,30](#page-10-16)[,45](#page-11-12)[,46\]](#page-11-13) or Apiezon wax [\[47–](#page-11-14)[51\]](#page-11-15) are commonly selected for their straightforward use and excellent insulating properties [\[33\]](#page-11-2). However, the quality of tip coatings obtained using these techniques is often highly dependent on the operator's manual skills, introducing variability that can range from well-insulated tips to those with inadequate or even complete insulation. Without the prior assessment of the tip coating quality, such irregularities can adversely impact the reliability of the EC-STM data, especially when an atomic-scale resolution is required but cannot be realized due to insufficient tip insulation.

Achieving the precision and consistency required in techniques such as EC-STM necessitates eliminating factors that compromise the integrity of results, particularly those associated with manual procedures like tip coating. In recent years, there has been a growing emphasis on automation and standardization in scientific research, driven by the need for reproducibility, efficiency, and a reduction in human errors [\[52\]](#page-11-16). The development of automated systems, such as the Automated Tip Coater (ATC) introduced in this study, represents a crucial step toward overcoming these challenges. By automating fundamental steps like tip coating, the ATC removes operator dependency and standardizes the process, aligning with the broader trend of enhancing experimental reproducibility and accuracy. The ATC uses molten polymers or Apiezon wax to provide a consistent insulating layer. Its key features include a precision tip movement system controlled by stepper motors, a rotational module driven by a DC motor, and a temperature-controlled heating block with a redesigned plate featuring a reduced gap size and a milled tray for the precise application of insulating material. The system is managed by an Arduino development board, with control software developed in C++ using PlatformIO for stand-alone operations. Furthermore, the ATC is user-friendly and requires minimal training, allowing users of all experience levels to achieve consistent results. Its modular design enables seamless adjustments to accommodate various EC-STM tip specifications—including tip diameter and length, as well as insulating material properties—ensuring the system can be tailored to the specific practices of any laboratory.

This study aims to address the challenges of achieving high-quality, reproducible tip coatings in EC-STM by developing the ATC. The primary objectives are to standardize the coating process, reduce operator-induced variability, and improve the reliability of EC-STM measurements under in situ and operando conditions. By achieving these goals, the study seeks to enhance the utility of EC-STM as a tool for investigating surface phenomena at the atomic scale, ultimately contributing to advancements in fields such as electrocatalysis, materials science, and energy storage.

2. Materials and Methods

2.1. Electrochemical Etching of W Tips

The STM tips were prepared by standard EC etching from a tungsten wire of 0.25 mm diameter in a 2 M KOH solution [\[53,](#page-11-17)[54\]](#page-11-18). Briefly, the etching process involves using a platinum wire loop with a diameter of 6 mm that serves as the counter electrode. The tungsten wire is placed in the center of the Pt loop so that 7 mm of the W wire is below the

horizontal plane of the Pt loop. The loop is then immersed in the electrolyte to suspend a thin lamella of electrolyte. A rectangular AC voltage of 8 Vpp and a frequency of 100 Hz is applied between the tungsten wire and the Pt wire loop. The etching process continues until the free end of the tungsten wire falls off into the Teflon container. The W tip is then rinsed with high-purity water and dried.

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The W wire is below that 7 mm of the W wire is below w

2.2. System Design and Architecture of the ATC 2.2. System Design and Architecture of the ATC

The ATC was developed with a focus on reliability, repeatability, and ease of use. A The ATC was developed with a focus on reliability, repeatability, and ease of use. A complete image of the working device is shown in Figure [1.](#page-2-0) The core design incorporates several key modules: a precise tip positioning system, a rotational module, and a temperature-controlled heating block with a redesign tray for melting insulating materials. The ATC is designed with a user-friendly interface, allowing researchers to configure all relevant parameters, including the immersion depth, coating duration, rotation speed, and horizontal and vertical movement speeds. horizontal and vertical movement speeds.

Figure 1. Image of the Indian opponent with labeled components: (1) Horizontal module; (2) Horizontal mod (2) Vertical movement module; (3) Rotational module; (4) Tip holder; (5) Coating tray; (6) Heating $\sqrt{2}$ CO $\sqrt{2}$ CO ule; (7) OLED display; (8) Encoder for user input; (9) RGB status indicator. module; (7) OLED display; (8) Encoder for user input; (9) RGB status indicator. Figure 1. Image of the ATC system with labeled components: (1) Horizontal movement module;

components were made using 3D printing technology, providing flexibility in design iterations and rapid prototyping. The system includes vertical and horizontal movement modules, driven by precision stepper motors, that provide micron-level accuracy in tip positioning. The vertical motion is controlled by a Nema 17 stepper motor coupled with an 8 mm lead screw, enabling smooth and repeatable linear displacement. A smaller stepper motor, typically used in DVD drives, facilitates accurate lateral positioning. The The mechanical design focuses on precise and controlled movements. Most of the incorporation of linear bearings in both systems minimizes friction and enhances stability, allowing for highly controlled tip immersion and withdrawal during the coating process.

The key innovations that distinguish this device are the redesigned coating tray and the addition of a rotational module. The coating tray has been engineered with a narrow slit that is only 50 μ m wider than the tip diameter (see Figure [2\)](#page-3-0). Furthermore, the tray is milled to enhance the distribution and volume control of the insulating material within milled to enhance the distribution and volume control of the insulating material within the cavity, which ensures that the correct amount of insulating material adheres to the tip, the cavity, which ensures that the correct amount of insulating material adheres to the tip, minimizing excess and resulting in a consistent insulation layer. minimizing excess and resulting in a consistent insulation layer.

Figure 2. (a) A 3D model illustrating the tip passing through the slit in the tray (5) during the coating process, with red arrows indicating the direction of movement (upward) and rotation. (b) Photograph showing the coated tip emerging from the tray after the insulation process.

The rotational module, powered by a DC motor, is another feature designed to achieve uniform coatings. This module includes a holder that secures the tip during the coating
modes while allowing it to retate smoothly around its axis. The retation speed and process where the rotate smoothly around its axis and the rotation specifical episode in the duration are fully adjustable to match the properties of the insulating material, ensuring an even coverage across the entire tip surface. process while allowing it to rotate smoothly around its axis. The rotation speed and

The durability and performance of coated tips are greatly influenced by the choice of insulating material. The system is compatible with various materials, including molten polymers and Apiezon wax, which are widely used for their known insulating properties and Chemical Testsance. In this stady, we primally used function include their grac steks
(Henkel, Germany), an Ethylene Vinyl Acetate Copolymer (EVA) adhesive with a softening temperature of 85 ± 5 °C. The heating block is based on a modified TS100 soldering iron, capable of reaching temperatures up to 400 °C with minimal hysteresis. The material is heated to the desired viscosity within the tray cavity, which is monitored in real-time through a temperature sensor, allowing precise adjustments as needed. and chemical resistance. In this study, we primarily used Pattex PTK1 hot melt glue sticks

is heated to the desired viscosity within the tray cavity, which is monitored in real-time *2.3. Tip Coating Process*

The process of insulating the tips begins by depositing the insulating material into the at the lower end, opposite the tray, allowing for the safe and secure placement of the tip in the holder. Once the insulating material reaches its melting point, it is evenly distributed within the tray cavity. Excess material is removed using a flat tool (e.g., a utility knife)
within the tray cavity. Excess material is removed using a flat tool (e.g., a utility knife) insulating material. Any material leaking through the slit is also removed with the flat tool before the coating process begins. tray cavity (5) (Figures [1](#page-2-0) and [2\)](#page-3-0). During the heating phase, the tip holder (4) is positioned swept across the edges surrounding the tray cavity, ensuring a consistent volume of applied

Next, the tip holder is automatically moved beneath the tray containing the insulating material. By gradually passing through the slit from below, the tip is immersed in the insulating material (Figure [2\)](#page-3-0). Depending on the type of insulating material used, the the flat tool be flatted at one of three stages. (1) while passing through the site
(2) immediately after passing through the slit, or (3) during withdrawal from the slit. These parameters can be adjusted by the user based on experience to achieve optimal coating parameters can be adjusted by the user based on experience to achieve optimal coating ing material. By gradually passing through the slit from below, the tip is immersed in the tip rotation can be initiated at one of three stages: (1) while passing through the slit, coverage. After a few seconds, the platform returns to its initial position, allowing for the safe removal of the coated tip. This process is shown in videos 1 and 2, which are included in the online Supporting Information.

2.4. Cyclic Voltammetry of Coated Tips

The CV measurements in 0.1 M HClO₄ electrolyte of the ATC-coated tips were carried out in a home-built three-electrode cell using a PocketPotentiostat developed by Matsubara [\[55\]](#page-11-19). Pt wires were used as counter and reference electrodes, placed less than 1 cm from the working electrode. The Pt quasi-reference electrode was calibrated with respect to RHE in argon-saturated 0.1 M HClO₄. All potentials thereafter are quoted with respect to RHE at pH = 1. The electrochemical cell was placed in a Faraday cage to minimize noise introduced by electromagnetic interference, which is essential for picoelectrochemical measurements.

2.5. EC-STM Measurements

The EC-STM measurements were carried out using a home-built EC-STM working in a constant-current mode, as described in detail by Wilms et al. [\[56\]](#page-11-20). This system is enhanced with a high-speed ADC acquisition card (Texas Instruments) that captures data at a rate up to 640 kSps. It features six channels simultaneously recording signals from the EC-STM, including lateral piezo displacement, working electrode potential, and sample current. Channels allocated for the recording of tunneling current and *z*-axis tip displacement during forward and backward scans enable the acquisition of both current and topographical STM images.

All electrolytes were prepared using deionized water from a Millipore-Pure system (Merck, Burlington, MA, USA) with a specific resistance of 18.2 M Ω ·cm and minimal organic impurities in the ppb range. Prior to use, the electrolytes were purged with argon gas for several hours. The chemicals used, obtained from Sigma-Aldrich (Saint Louis, MO, USA), were of the highest commercially available purity and were used without further purification.

The HOPG electrode (TipsNano, ZYB quality, mosaic spread: $0.8 \pm 0.2^{\circ}$) was prepared through mechanical exfoliation of the topmost layers by adhesive tape. To prevent recontamination of the surface, the HOPG was immediately mounted into the EC cell of the EC-STM and covered with a drop of degassed electrolyte.

All electrode potentials in the publication are referred to as an RHE reference electrode, while all tip bias potentials are reported with respect to the working electrode. Therefore, the bias voltage to the tip can be referred to as the RHE electrode in accordance with this equation:

$$
U_b \text{ vs. }_{ref} = E + U_b
$$

where U_b vs. $_{ref}$ represents the bias applied to the tip versus the reference electrode, E denotes the electrode potential, and U_b is the bias versus working electrode potential [\[53\]](#page-11-17).

3. Results and Discussion

3.1. Visual Assessment of Tip Coating Quality

The quality of the coated tips was evaluated using a two-step process involving both optical inspection and electrochemical testing. The first step focused on assessing insulation continuity, uniformity, and coating thickness under an optical microscope (Figure [3\)](#page-5-0). The results revealed that tips coated using the ATC displayed smooth and consistent insulation with minimal excess material. In contrast, manually coated tips often exhibited significant excess material, forming polymer tails that required mechanical trimming. These tails, resulting from the adhesive nature of the coating material, are a common issue in manual coating processes and can introduce variability in the insulation layer, particularly near the tip apex. This variability not only affects the reproducibility of EC-STM measurements but also increases the risk of damaging the insulation during the trimming process.

process.

Figure 3. Comparison of tip coatings produced by the ATC and manually. The ATC-coated tip (left) **Figure 3.** Comparison of tip coatings produced by the ATC and manually. The ATC-coated tip (left) shows smooth and consistent insulation without excess material or polymer tails. In contrast, the shows smooth and consistent insulation without excess material or polymer tails. In contrast, the manually coated tip (right) exhibits a significant excess of insulating material, forming a tail that manually coated tip (right) exhibits a significant excess of insulating material, forming a tail that
. requires mechanical trimming.

The ATC rotational module effectively addresses this issue by maintaining continuous rotation during the withdrawal phase of the coating process. By rotating the tip as it is withdrawn from the insulating material, the rotational module prevents the formation of polymer tails, ensuring a uniform and smooth coating without the need for further mechanical intervention (Figure [3\)](#page-5-0). This automation of the coating process reduces the pendence on operator skill and eliminates a significant source of variability. dependence on operator skill and eliminates a significant source of variability.

3.2. Electrochemical Testing of Coated Tips 3.2. Electrochemical Testing of Coated Tips

The second and most crucial phase of quality assessment involved conducting fast The second and most crucial phase of quality assessment involved conducting fast cyclic voltammetry (CV) tests to evaluate the electrochemical stability and insulation performance of the coated tips. In these tests, tungsten tips coated using the ATC were assessed in 0.1 M HClO₄ at a scan rate of 50 mV/s within an electrode potential window of −500 mV to 500 mV. The relatively high scan rate was chosen to expedite the evaluation −500 mV to 500 mV. The relatively high scan rate was chosen to expedite the evaluation process, allowing multiple tips to be tested in a shorter timeframe. process, allowing multiple tips to be tested in a shorter timeframe.

Figur[e 4](#page-6-0) presents two key outcomes: on the left, the CV curve of a coated tip, and on Figure 4 presents two key outcomes: on the left, the CV curve of a coated tip, and on the right, the statistical analysis of the insulation performance across a total of 60 tips sourced from five independent batches (batch 1: 15 tips, batch 2: 12 tips, batch 3: 6 tips, batch 4: 9 tips, batch 5: 18 tips). The CV curve illustrates that the ATC-coated tip maintained a low leakage current within the range of ± 10 pA, signifying effective insulation. The statistical analysis revealed that 30% of the tips exhibited leakage currents below ± 10 pA, with an additional 30% maintaining leakage below ± 50 pA. Furthermore, 17% of the tips showed leakage currents below ± 20 pA, while only 10% exhibited currents exceeding ± 100 pA, ±100 pA, indicating minor defects. A small percentage (2%) were fully isolated, showing indicating minor defects. A small percentage (2%) were fully isolated, showing negligible current leakage. A contrasting trend emerges in the analysis of manually coated tips, as illustrated in Figure S2 of the Supporting Information. Among the 74 tips examined, 28% were fully isolated, while a significant 43% displayed leakage current exceeding ± 100 pA. Notably, only 6% of tips recorded leakage current below ± 10 pA, with an additional 2% maintaining leakage levels below ± 20 pA. These results further highlight the effectiveness of the automated approach to tip coating employed by the ATC.

effectiveness of the automated approach to tip coating employed by the ATC.

(**b**) Pie chart showing the percentage of coated tips with leakage currents below specific thresholds. Figure 4. (a) Typical CV curve recorded in 0.1 M HClO₄ electrolyte for a W tip coated using the ATC.

tips for diverse EC-STM experiments. The distribution shown in Figure 4b demonstrates that the ATC can produce tips suitable for a wide range of experimental needs, from general imaging to highly sensitive EC-STM measurements, especially with the bias tip potential
leads on that power seconds networks Understanding the role of insulation quality is key to determining the suitability of kept constant versus sample potential.

Experiment versitive stample potentials.
The required level of tip insulation depends significantly on the specific type of EC-STM experiment being conducted. While high-resolution imaging of atomic structures can often be achieved with tips exhibiting leakage currents exceeding ± 100 pA—by adjusting the bias voltage to match the open circuit potential of the tip and increasing the tunneling current setpoint—certain advanced measurements demand higher insulation quality.

For instance, experiments involving step or cyclic voltammetry (CV) potentiodynamic measurements and quasi-spectroscopy are particularly sensitive to leakage currents. In these techniques, the tip potential is varied over a range, and any leakage current can
the formatik the comment of the measurement between the integral distance design and or disturbing the electrochemical equilibrium at the tip-sample interface. Therefore, tips with leakage currents below ± 50 pA, ± 20 pA, or even ± 10 pA are preferred for such sensitive experiments. interfere with the accuracy of the measurements by introducing additional faradaic currents

By producing a significant proportion of tips with leakage currents below ± 10 pA and ± 20 pA, the ATC provides researchers with the ability to select tips based on the specific insulation quality required for their experiments, enhancing the versatility and reliability of EC-STM studies. This improvement not only elevates the quality of imaging and measurements but also reduces the frequency of tip replacement, thereby lowering operational costs.

Interefore, the performance of the ATC-coated tips at such a high scan rate is par-
Therefore, the performance of the ATC-coated tips at such a high scan rate is particularly notable, as EC-STM measurements are typically conducted at lower scan rates to minimize Faradaic current. Maintaining low leakage currents at 50 mV/s highlights bustness under more demanding conditions than are typically encountered in standard EC-STM experiments. Furthermore, the ability to perform such fast checks significantly enhances workflow efficiency, allowing researchers to quickly assess the insulation quality δ multiple ups. the high-quality insulation provided by the ATC. It also demonstrates the system's roof multiple tips.

3.3. In Situ and Operando EC-STM Performance

To further evaluate the performance of the ATC-coated tips, they were tested under in situ and operando conditions on an HOPG surface in 0.1 M $\overline{HClO_4}$ electrolyte. These experiments aimed to determine the stability and resolution of the tips in a dynamic electrochemical environment.

Figure 5 displays a typical CV curve recorded during these experiments, along with large-scale and high-resolution STM images. The CV curve reflects the expected electrochemical behavior of the HOPG surface, with the electrode potential window limited by
the hydrogen synkties gentian (LIEP), or the exthedise ideased parablemate ion integer the hydrogen evolution reaction (HER) on the cathodic side and perchlorate ion interca-the hydrogen evolution reaction (TED) on the called the and perchabilities on interest
lation followed by the oxygen evolution reaction (OER) on the anodic side [\[57–](#page-11-21)[59\]](#page-12-0). The large-scale STM image (Figure 5b), captured at an electrode potential of 270 mV, reveals terraces separated by monoatomic steps approximately 3.3 A in height, consistent with the known interlayer spacing of graphite [\[60\]](#page-12-1). At atomic resolution, Figure 5c shows the hexagonal lattice structure of the HOPG surface, with a lattice spacing of approximately hexagonal lattice structure of the FIOT G surface, which lattice spacing of approximately
2.46 Å. This spacing corresponds to the periodicity of every second carbon atom in the hexagonal lattice, a result of the ABAB stacking of graphene layers in HOPG [\[61\]](#page-12-2).

E vs RHE (mV)

scale topography STM image of the HOPG surface, recorded at an electrode potential of 270 mV; inset shows the cross-section corresponding to the red line in (b). (c) High-resolution current STM image of the HOPG surface under the same conditions, demonstrating the tip's ability to maintain precise imaging at the atomic scale. Tunneling conditions: (**b**) I_t = 1.6 nA, U_b = −235 mV; (**c**) I_t = 0.5 nA, $U_{\rm b} = -104 \text{ mV};$ **Figure 5.** (a) CV curve of a HOPG surface recorded in Ar-saturated 0.1 M HClO₄ electrolyte. (**b**) Large- $U_b = -104$ mV.

and continuous cha[ng](#page-8-0)es in electrode potential. Figure 6 illustrates two critical scenarios where the electrode potential was dynamically varied while capturing STM images. The ATC-coated tips were further subjected to rigorous testing under potentiodynamic conditions to evaluate their performance in maintaining atomic resolution during rapid

In Figure [6a](#page-8-0), an STM image of the HOPG surface with atomic resolution is shown. but in a might generally variable potential was tapidly changed at a specific point as indicated by the corresponding time-aligned plots in Figure [6b](#page-8-0),c. The *y*-axis of the STM image in Figure [6a](#page-8-0) is directly correlated with the time axis in Figure $6b$,c, providing a clear visualization of how the STM image changes as the electrode potential is abruptly altered. Despite the rapid potential change, the ATC-coated tip maintained its resolution, successfully capturing the atomic structure of the HOPG surface without any significant
loss of imaging quality During the imaging process, the electrode potential was rapidly changed at a specific point, loss of imaging quality.

Figure [6d](#page-8-0)–f presents a second scenario where the electrode potential was continuously varied during the STM imaging process. In this experiment, the potential was systematically ramped up and down at a rate up to 100 mV/s, as shown in the corresponding plots. The *y*-axis in the STM image (Figure [6d](#page-8-0)) again corresponds to the time axis in the electrochemical Λ edula proto (Figure 6d). Even under these dynamically enarging conditions, the FITE coated tip consistently resolved the atomic lattice of the HOPG surface, demonstrating its robustness and stability under potentiodynamic conditions. data plots (Figure [6e](#page-8-0),f). Even under these dynamically changing conditions, the ATC-

face, demonstrating its robustness and stability under potentiodynamic conditions.

resolution STM image captured during rapid changes in electrode potential. (**b**) Corresponding current density vs. time plot, illustrating the current response to the dynamic potential changes. rent density vs. time plot, illustrating the current response to the dynamic potential changes. (**c**) (**c**) Electrode potential vs. time plot, showing the timing of the rapid potential changes during the STM ϵ the STM scan. (**d**) STM image of the HOPG surface obtained during continuous potentiodynamic imaging, with the electrode potential modulated at a rate of up to 100 mV/s, maintaining atomic resolution throughout. (**e**) Current density vs. time plot corresponding to the continuous potential modulation. (f) Electrode potential vs. time plot, demonstrating the continuous modulation of the electrode potential during imaging. Tunneling conditions: (a) $I_t = 0.5$ nA, $U_b = -104$ mV; (b) $I_t = 1$ nA, **Figure 6.** Potentiodynamic STM imaging of the HOPG surface using an ATC-coated tip. (**a**) Atomic $U_b = 234$ mV.

These results underscore the capability of the ATC-coated tips to operate reliably under challenging electrochemical environments. The ability to maintain atomic resolution during rapid and continuous changes in electrode potential is a crucial requirement for in situ and operando EC-STM studies, where capturing real-time structural dynamics at the atomic level is essential. The ATC's consistent performance under these conditions validates its effectiveness in producing high-quality, insulated tips that can withstand the rigorous demands of advanced EC-STM research.

4. Conclusions 4. Conclusions

This study presents the development and application of an Automatic Tip Coater (ATC) designed to a designed to a challenge of an automatic tip coater (ATC) designed to address the challenges of achieving high-quality, reproducible tip coatings for
EC-STM, The ATC leads of a line of a lin EC-STM. The ATC key features, including a precision tip movement system, a rotational module, and a temperature-controlled iteating block, enable the consistent and uniform
application of insulating materials, significantly reducing the variability often associated apprecisent of instituting materials, significantly This study presents the development and application of an Automatic Tip Coater (ATC) module, and a temperature-controlled heating block, enable the consistent and uniform

The ATC-coated tips demonstrated a superior insulation performance, as evidenced by cyclic voltammetry (CV) tests conducted at a scan rate of 50 mV/s in a 0.1 M HClO₄

electrolyte. The results showed that over 75% of the tips maintained leakage currents below 50 pA, with a substantial subset (30%) achieving currents as low as \pm 10 pA, indicating the high quality of the coatings. The ability to perform reliably at such a high scan rate is particularly noteworthy as it allows for the rapid screening and evaluation of multiple tips, an important factor in EC-STM research. In contrast, manually coated tips often struggle to achieve such a consistent performance due to issues with excess material and uneven coatings. This can result in significant variability in tip performance, leading to inconsistencies in data quality and reliability. By standardizing the coating process and reducing dependence on operator skills, the ATC ensures a consistent coating quality across batches, making the process more accessible to new users while significantly reducing the variability associated with manual methods.

Further validation under in situ and operando conditions using the HOPG surface confirmed the stability of the ATC-coated tips. The tips maintained an atomic resolution even under dynamic electrochemical conditions, demonstrating their robustness and reliability in capturing detailed surface phenomena.

In summary, the introduction of the ATC offers a reproducible solution for tip coating that enhances the accuracy and reliability of the EC-STM studies. By automating a process that traditionally relies heavily on operator skill, the ATC reduces experimental variability, lowers research costs, and contributes to the standardization of EC-STM methodologies. This innovation aids the exploration of surface phenomena at the atomic level, particularly in fields such as electrocatalysis, energy storage, and materials science, where precise and reliable measurements are paramount.

5. Patents

Patent application PL448634 has been submitted to the Polish Patent Office for the ATC described in this paper.

Supplementary Materials: The following supporting information can be downloaded at [https://www.mdpi.com/article/10.3390/surfaces7040065/s1,](https://www.mdpi.com/article/10.3390/surfaces7040065/s1) Videos S1 and S2: Movies demonstrating the tip coating process. Figure S1 shows images of manual tip coater, and Figure S2 presents CV curves and statistical analysis of insulation performance for 74 manually coated tips.

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