



Proceeding Paper

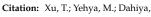
Dedicated Wearable Sensitive Strain Sensor, Based on Carbon Nanotubes, for Monitoring the Rat Respiration Rate [†]

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Abstract: This paper presents a highly sensitive and novel wearable strain sensor using one-dimensional material for monitoring the respiration rate of an anesthetized rat. The dedicated sensitive sensor, based on carbon nanotubes mixed with poly(3,4-ethylenedioxythiophene) polystyrene sulfonate, was attached above the rat chest. A Wheatstone bridge electrical circuit, associated with a multifunction portable device, was connected to the strain sensor. The change of the strain sensor's resistance value, induced by the mechanical deformability during the rat respiration, was detected and transformed into a voltage signal. The respiration information could be thus extracted and analyzed.

Keywords: wearable strain sensor; rat respiration rate monitoring; carbon nanotubes; poly(3,4-ethylenedioxythiophene) polystyrene sulfonate



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1. Introduction

Cardiovascular disease is a group of disorders of the heart and blood vessels, including coronary heart disease, cerebrovascular disease, and rheumatic heart disease, etc. [1]. It is one of the most common causes of death in the world. In 2013, cardiovascular disease claimed a total of 17.3 million lives (31% of total deaths), which is a significant increase from 12.3 million in 1990 (25.8% of total deaths). Since the 1970s, death rates from cardiovascular diseases have increased in developing countries regardless of age group, while it declines in most developed countries [2].

There is an increasing demand for a reliable heart monitoring system to capture intermittent abnormalities and detect serious heart behaviors, leading to sudden death in extreme cases. In addition to cardiac monitoring, there is a growing need to capture the respiratory function in several contexts, such as sleep apneas. For example, "Internet-of-Medical-Things (IoMT)" are now considered to be a good strategy for monitoring the abnormalities of breathing and cardiac rate. A wearable monitoring strain sensor detects accidents and sends the information immediately to the medical staff [3].

Therefore, there is a need to develop a highly sensitive, durable, and biocompatible strain sensor. In this paper, a new one-dimensional nanomaterial-based strain sensor is introduced for respiratory rate monitoring, followed by the fabrication process and the experimental platform. Then, we performed stretch tests on the strain sensor for the verification of the sensor's durability. Finally, the results of the respiration monitoring of the anesthetized rat are presented.

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2. Theory

Compared to other strain sensors such as capacitive, piezoelectric, and triboelectric sensors, piezoresistive sensors have gained interest as they provide high sensitivity with simple device design and readout circuits. The working principle of the piezoresistive sensor is based on the strain effect: when the conductor or semiconductor material is mechanically deformed under the action of external force, its electrical properties change accordingly. The sensitivity of the strain sensor could be characterized by the gauge factor (GF) [4]:

$$GF = \frac{\Delta r/r_0}{\Delta l/l_0},\tag{1}$$

where r_0 represents the initial resistance of the strain sensor, Δr represents the difference between its real-time resistance under stretching r and the original value r_0 ($\Delta r = r - r_0$). l_0 represents the initial length of the strain sensor, Δl represents the change in the length ($\Delta l = l - l_0$, l the real-time length).

In general, metallic materials have a significantly low GF (about 2), indicating a low sensitivity [5]. In addition, the appearance of the microcracking of the metallic thin films affects its stretch capability. Non-linear electromechanical behavior is the discrete deformation behavior of the conductive networks at different strain regimes. It impacts the long-term sensitivity and stretchability of the strain.

One-dimensional material was thus chosen to solve the problem of the metallic piezore-sistive strain sensor. In this paper, carbon nanotubes (CNTs) [6] were mixed with poly(3,4-ethylenedioxythiophene) polystyrene sulfonate (PEDOT:PSS) [7] to obtain more stable filler networks to avoid the resistance value shift caused by device aging and the repetitive tests. The CNT network formed a thin film less compact than the metallic layer, whereas the conductive polymer PEDOT:PSS filled the space in the network to ensure the tolerance of the stretch.

To encapsulate the wearable strain sensor, instead of the traditional polymers such as Polydimethylsiloxane (PDMS), Dragon skin (DS FX-Pro) was considered for its good elasticity, robustness, as well as biocompatibility.

3. Experimental

The conventional method of the strain sensor fabrication was realized by the deposition of gold evaporation on Polydimethylsiloxane (PDMS), and then covered all patterned surfaces with another PDMS layer. The obtained GF was very high (GF from 2.5×10^6 to 10×10^6); however, two of the major limitations were: (i) the response was linear up to 0.3% strain only followed by the sudden change in the resistance value and (ii) poor recoverability. The nominal resistance of the device significantly changed after releasing the applied strain; therefore, nanocomposite materials, such as carbon nanotubes, were chosen to have a GF high enough (from 3 to 6) to sense subtle movements but more robust and show a linear change in resistance up to a strain of 40%. In addition, the strain sensor is based on a mixture of CNTs; PEDOT:PSS has a more significant GF (about 50, 60). Moreover, instead of a linear shape, such 1D material was encapsulated in the polymer with 'U' shape, which was very useful to increase the sensitivity of the strain sensor.

3.1. Fabrication

The strain sensor has a length of 3.5 cm, a width of 2 cm, and a thickness of 2 mm. The center groove of CNTs mixed with PEDOT:PSS has two branches in parallel (length = 2 cm, width = 2 mm, thickness = 0.4 mm). Both branches are connected at one side, and the distance between them equals 2 mm.

To fabricate the strain sensor by the unconventional method, here is the process to follow (See Figure 1):

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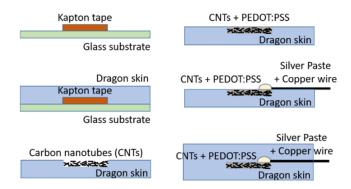


Figure 1. Fabrication process of the strain sensor based on carbon nanotubes (CNTs) mixed with poly(3,4-ethylenedioxythiophene) polystyrene sulfonate (PEDOT:PSS).

- In the first step, a Dragon Skin (DS) chip containing macro channels was realized by using a standard molding process. The Kapton tape was cut with a blade to define the dimensions of the macro channel.
- Then, carbon nanotubes (CNTs) suspension (5 or 6 times, approximately 30 μ L at a time) was dropped into the DS channel. The suspension, approximately 0.1–0.5 wt% in isopropanol (IPA), filled the channels of the DS mold through capillary forces. The conductive polymer poly(3,4-ethylenedioxythiophene) polystyrene sulfonate (PEDOT:PSS), which, similar to an elastic sheet, was deposited and mixed with CNTs. It enables CNTs to stay connected to each other although the strain sensor was under stretch force.
- Finally, copper (Cu) wires were attached using silver epoxy paste. A sandwichtype structure was realized by pouring another layer of DS, which flows into the CNT network and cross-linked with the bottom layer of DS. The top Dragon Skin layer encapsulated fully and firmly the CNT sensing material, thus improving the robustness of the device.

3.2. Experimental Set-Up

The wearable strain sensor was first tested using a linear stage controlled by E-861 PiezoWalk® NEXACT® Controller (See Figure 2a). Thanks to the monitoring with LabVIEW controlled by Keithley 2400 source meter, the strain sensor was stretched between 0.01 mm/s to 10 mm/s. When there was no stretch force, the strain sensor's resistance was equal to the other three resistances with a fixed value (22 k Ω).

The Wheatstone bridge consists of four resistors, three of them are fixed resistors R_{10} , R_{11} , and R_{12} (which have a value close to the resistivity of the strain sensor when it is at rest) and the fourth one is the strain sensor itself. The bridge is connected to a low-power operational amplifier with a gain of two that can be tuned with the feedback resistor R_{13} (47 k Ω). We chose the MCP6401 operational amplifier thanks to its characteristics: operating voltage from 1.8 V to 6 V, low quiescent current of 45 μ A, rail-to-rail input and output; these features make this operational amplifier well suited for battery-powered applications (See Figure 2b).

This allows the verification of the viability and durability of the CNTs/PEDOT:PSS-based strain sensor. The transformed current signal (or output DC voltage signal) was monitored by an oscilloscope (DSOX2024A-Keysight Technologies) (See Figure 2c) or multifunction hardware (Analog Discovery 2) and recorded for data processing. Thanks to Analog Discovery 2, the fast Fourier transform was obtained at the same time under the output DC voltage signal curve (See Figure 2d).

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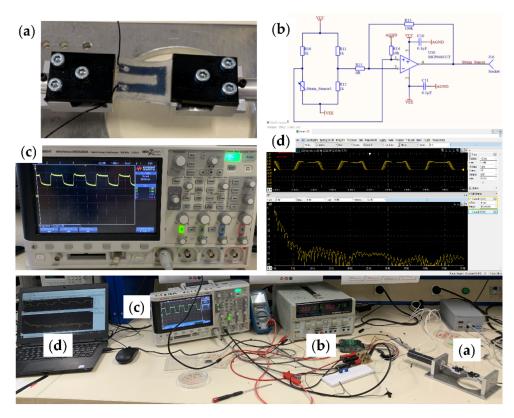


Figure 2. Experimental platform: (a) Strain sensor test by E-861 PiezoWalk[®] NEXACT[®] Controller; (b) Wheatstone bridge structure for the rat respiration monitoring; (c) output DC voltage signal verified by oscilloscope; (d) output DC voltage signal shown by the multifunction portable device (Analog Discovery) and its fast Fourier transform.

4. Results and Discussion

The relative resistance variation of the strain sensor $\Delta R/R_0$ was measured under repeated stretches by applying different stretch values (Figure 3b,c). When the stretch length of the strain sensor was equal to 0.36 mm, the ratio $\Delta R/R_0$ changed from 0.1 to 0.7 (Figure 3a). As the applied stretch force was cyclical, the signal curve was also repetitive. There are some peaks, which were observed at the beginning and the end of the square signal. Such "instantaneous stretch-relax" phenomenon might be related to the elasticity of the strain sensor. These measurements showed that the sensor resistance is stable and that the electrical characteristics of the sensor are maintained.

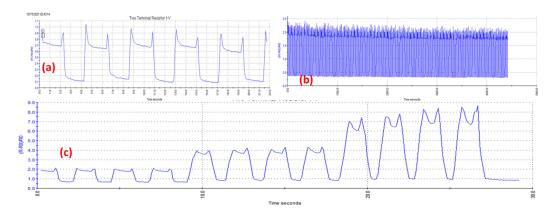


Figure 3. (a) Variation of the resistance $\Delta R/R_0$ of the sensor at a stretch of 2% (0.36 mm), (b) relative resistance variation of the strain sensor under repeated tensions for a strain of 2% during more than 400 cycles, (c) $\Delta R/R_0$ measurement for different stretch (2%, 5%, 10%).

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After the validation, such CNTs/PEDOT:PSS-based strain sensor was reversibly attached above the rat chest for its respiration monitoring during anesthesia. Isoflurane (2.5%) was used to make the rat sleep during the experiment [8]. The regular respiration curve for 60 s is shown in Figure 4a. The output voltage evolution is between 0.6 and 0.7 V. For 1 min, the rat respiration rate during the rest equals 62 times/min, which corresponds with the theory value [9]. The electrical monitoring result is very reliable and repetitive. The experiments were carried out by using three different rats, and stable electrical sensing curves were obtained (Figure 4b–d). The rat's state was also monitored by the cardiogram, which detected the cardiac frequency during the rat anesthesia (See Figure 5). The actual measurement was obtained from conventional electrocardiogram (ECG) recording obtained by surface-needles two-lead electrodes, using Powerlab and Chart system (ADinstrument).

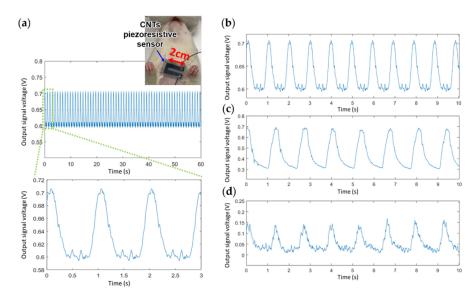


Figure 4. (a) Voltage signal for the rat respiration rate monitoring during its rest. Reproductive electrical monitoring curves of rat respiration rate (for three different anesthetized rats); (b) for first rat; (c) for second rat; (d) for third rat.

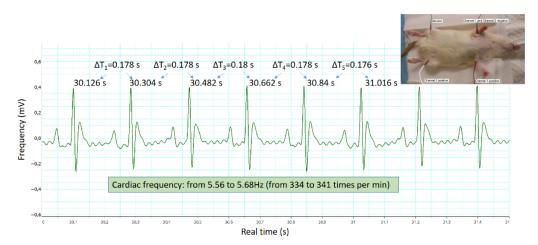


Figure 5. Cardiogram for the rat respiration rate monitoring during its anesthesia.

One major drawback we found with this type of sensor is the drifting of the nominal resistance that occurs after intensive stretching of the sensor. We experimented with the aging of the sensor by measuring its nominal resistance over several weeks and by stretching at different times. We found that the nominal resistance increases slightly with time but mainly after testing experiences, as shown in Figure 6. The mechanism behind this shift in resistance is not well known and we think that permanent changes in the CNTs

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network can occur with time but also when the sensor is used for large (>10%) elongations. Carbon nanotubes may move within the polymer composite and contacts between CNTs may break during large elongations.

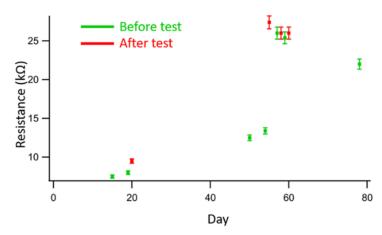


Figure 6. Resistance value evolution of the strain sensor before and after test.

Finally, in order to build the sensor with common shape and functionalities, a filament mold printed by 3D printing was realized to create the repetitive polymer substrate to insert the CNTs.

5. Conclusions

We developed a new wearable strain sensor based on one-dimensional material (CNTs) mixed with conductive polymer (PEDOT:PSS) and reported that the sensitivity and the durability of the wearable strain sensor were improved compared to other CNT based strain sensors. The respiration of the anesthetized rat was successfully monitored using CNTs/PEDOT:PSS-based strain sensor.

In addition to many advantages such as low-cost fabrication, simple fabrication process, ease of testing as well as biocompatibility, stretchable strain sensors will play a crucial role in monitoring patients with cardiovascular disease as well as their breathing and heart rate. Such sensors will enable the new technological drive called "Internet-of-Medical-Things (IoMT)", which links wearable devices/sensors into a communication network for real-time or periodic patient-doctor communications. The patient information could be immediately recorded and transformed to healthcare service providers, and that might reduce the death rate of cardiovascular disease.

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